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A TABLE OF LANCHESTER-CLIFFORD-SCHLAEFLI FUNCTIONS.(U)
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NAVAL POSTGRADUATE SCHOOL

Monterey, California

A TABLE OF

LANCHESTER-CLIFFORD-SCHLÄFLI FUNCTIONS

by

James G. Taylor

and

Gerald G. Brown

October 1977

NAVAL POSTGRADUATE SCHOOL
Monterey, California

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This report contains the most extensive set of tables currently available of Lanchester-Clifford-Schläfli (LCS) functions. These functions may be used to analyze Lanchester-type combat between two homogeneous forces modelled by power attrition-rate coefficients with "no offset." Theoretical background for the LCS functions is given, as well as a narrative description of the physical circumstances under which the associated Lanchester-type combat model may be expected to be applicable. Numerical examples are given

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to illustrate the use of the LCS functions for analyzing "aimed-fire" combat modelled by the power attrition-rate coefficients with "no offset." Our results and these tabulations allow one to study this particular variable-coefficient combat model almost as easily and thoroughly as Lanchester's classic constant-coefficient model.

A TABLE OF LANCHESTER-CLIFFORD-SCHLÄFLI FUNCTIONS

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1. Introduction

Lanchester-type* differential-equation combat models are an important tool for analyzing many important problems of military operations research. In such a combat model, a so-called attrition-rate coefficient represents the fire effectiveness of a particular weapon-system type against a particular target type, i.e. the weapon-system type's effective firepower against such a target. Time-dependent attrition-rate coefficients are used to model temporal variations in firepower on the battlefield. Thus, we see that time-dependent attrition-rate coefficients are important (and, in fact, essential [4-6]) for the quantitative analysis of hypothetical combat.

Militarily realistic computer-based Lanchester-type models of quite complex military systems have been developed for almost the entire spectrum of combat operations, from combat between battalion-sized units to theater-level operations. Nevertheless, a simple combat model may yield a clearer understanding of significant interrelationships that are difficult to perceive in a more complex model, and such insights can subsequently provide valuable guidance for more detailed computerized investigations. In this report we consider such a simplified variable-coefficient Lanchester-type model of combat between two homogeneous forces.

For this variable-coefficient Lanchester-type model of combat between two homogeneous forces, different functional forms for the attrition-rate coefficients lead to different mathematical functions being involved in representing and computing the force-level trajectories. In a previous paper [5] we have discussed the plausibility of the hypothesis that except for the special case of a constant ratio of attrition-rate coefficients,

---

*So-called after pioneering work of F. W. Lanchester [3].

the solutions to such differential equations cannot be represented in terms of "elementary" functions of analysis. Thus, new transcendental functions arise in the study of combat modelled with time-dependent attrition-rate coefficients. In particular, we have previously introduced [5-6] so-called Lanchester-Clifford-Schläfli (LCS) functions for analyzing combat modelled with power attrition-rate coefficients with "no offset" (see Section 3 below).

In the Appendix to this report is contained the most extensive set of tables currently available for the LCS functions: it contains tables of five-decimal-place values of the hyperbolic-like LCS functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ (see Section 4 below) for 25 fractional values of α (see Section 6 below). The main body of this report provides the theoretical and modelling background for the use of these tables. In particular, we *examine a model of a constant-speed attack* on a static defensive position and show how associated range-dependent kill rates give rise to time-dependent attrition-rate coefficients with "no offset." Numerical computations are presented to illustrate the use of the LCS functions for analyzing such "aimed-fire" combat. As a consequence of the availability of these tables, one can now study this variable-coefficient combat model almost as easily and thoroughly as Lanchester's classic constant-coefficient model.

2. Variable-Coefficient Lanchester-Type Equations of Modern Warfare.

We consider combat between two homogeneous forces modelled by the following variable-coefficient Lanchester-type [3] (see [4,5]) equations of modern warfare

$$\begin{cases} \dfrac{dx}{dt} = -a(t)y & \text{with } x(0) = x_0 , \\ \dfrac{dy}{dt} = -b(t)x & \text{with } y(0) = y_0 , \end{cases} \tag{2.1}$$

where $t = 0$ denotes the time at which the battle begins, $x(t)$ and $y(t)$ denote the numbers of X and Y at time t, and $a(t)$ and $b(t)$ denote time-dependent Lanchester attrition-rate coefficients, which represent the effectiveness of each side's fire. These coefficients depend on variables such as force separation, tactical posture of targets, rate of target acquisition, firing rate, etc. (see [4-7] for further details). Variable attrition-rate coefficients are used to model temporal variations in firepower on the battlefield. In any analysis of combat, moreover, we should use the above equations (2.1) only for x and $y \geq 0$ and, for example, set $dx/dt = 0$ when $x = 0$, since negative force levels have no physical meaning.

Mathematically, we assume that the attrition-rate coefficients $a(t)$ and $b(t)$ are defined, positive, and continuous for $t_0 < t < +\infty$ with $t_0 \leq 0$. We also assume that $a(t)$ and $b(t) \in L(t_0,T)$ for any finite $T \geq t_0$. We further take $a(t)$ and $b(t)$ to be given in the form

$$a(t) = k_a g(t) , \qquad \text{and} \qquad b(t) = k_b h(t) , \tag{2.2}$$

where k_a and k_b are positive constants chosen so that $a(t)/b(t) = k_a/k_b$ when $g(t) \equiv h(t)$. We introduce the combat-intensity parameter λ_I and the relative-fire-effectiveness parameter λ_R defined by

$$\lambda_I = \sqrt{k_a k_b}\ , \qquad \text{and} \qquad \lambda_R = k_a/k_b\ . \tag{2.3}$$

From our assumptions about $a(t)$ and $b(t)$, it follows that, for example, $a(t) \notin L(t_0,T)$ implies $\int_{t_0}^{T} a(t)dt = +\infty$.

The X force level as a function of time may be represented as [5,6]

$$x(t) = x_0\{C_Y(0)C_X(t) - S_Y(0)S_X(t)\} - y_0\sqrt{\lambda_R}\ \{C_X(0)S_X(t) - S_X(0)C_X(t)\}, \tag{2.4}$$

where the hyperbolic-like <u>general Lanchester functions</u> (GLF) $C_X(t)$ and $S_X(t)$ are linearly-independent solutions to the X <u>force-level equation</u>

$$\frac{d^2x}{dt^2} - \left\{\frac{1}{a(t)}\frac{da}{dt}\right\}\frac{dx}{dt} - a(t)b(t)x = 0\ , \tag{2.5}$$

with initial conditions

$$C_X(t_0) = 1\ , \qquad S_X(t_0) = 0\ ,$$
$$\{1/a(t_0)\}\ dC_X/dt(t_0) = 0\ , \qquad \{1/a(t_0)\}\ dS_X/dt(t_0) = 1/\sqrt{\lambda_R}\ . \tag{2.6}$$

Here t_0 denotes the largest finite time at which $a(t)$ or $b(t)$ ceases to be defined, positive, or continuous. The Y force level as a function of time is given by a similar expression, with $C_Y(t)$ and $S_Y(t)$ being analogously defined for the corresponding Y force-level equation.

It is sometimes convenient to introduce the new independent variable τ defined by

$$\tau = \int_{t_0}^{t} \sqrt{a(s)b(s)}\, ds\ . \qquad (2.7)$$

It is readily seen that the transformation $\tau = \tau(t)$ is well defined and invertible. Let us denote $\tau(0)$ as τ_0. We observe that $t_0 \leq 0$ implies that $\tau_0 \geq 0$. If we denote the "average intensity of combat" as $\overline{\sqrt{a(t)b(t)}}$, then

$$\overline{\sqrt{a(t)b(t)}}\ t = \{(1/t) \int_{0}^{t} \sqrt{a(s)b(s)}\, ds\}t = \tau - \tau_0\ . \qquad (2.8)$$

The substitution (2.7) transforms (2.5) into

$$\frac{d^2x}{d\tau^2} - \left(\frac{1}{2}\right)\left\{\frac{d}{d\tau}\ \ln R(\tau)\right\}\frac{dx}{d\tau} - x = 0\ , \qquad (2.9)$$

with initial conditions

$$x(\tau_0) = x_0\ , \qquad \text{and} \qquad \{1/\sqrt{R(\tau_0)}\}\ dx/d\tau(\tau_0) = -y_0\ ,$$

where $R(\tau) = a(t)/b(t)$.

3. Combat Modelled with Power Attrition-Rate Coefficients.

The above equations (2.1) basically apply to "aimed-fire" combat when target-acquisition times do not depend on the numbers of targets available (see [5,6] for further details). A large class of tactical situations of interest can be modelled with the following general power attrition-rate coefficients [5-7]

$$a(t) = k_a(t + C)^{\mu}, \qquad \text{and} \qquad b(t) = k_b(t + C + A)^{\nu}, \tag{3.1}$$

where A and $C \geq 0$. We will call A the <u>offset parameter</u>, since it allows us to model (with μ and $\nu \geq 0$) battles between opposing weapon systems with different maximum effective ranges (see [5,6]). We will call C the <u>starting parameter</u>, since it allows us to model (again, with μ and $\nu \geq 0$) battles that begin within the maximum effective ranges of the two opposing systems. We observe that for the general power attrition-rate coefficients (3.1) we have $t_0 = -C$, and μ and ν must be > -1 in order that $a(t)$ and $b(t) \in L(t_0,T)$.

The above nomenclature is motivated and possible applications of our work are indicated by considering S. Bonder's model of the constant-speed attack on a static defensive position (see [4-7] for further details)

$$\frac{dx}{dt} = -\alpha(r)y, \qquad \text{and} \qquad \frac{dy}{dt} = -\beta(r)x , \tag{3.2}$$

where r denotes the range between opposing forces, and $\alpha(r)$ and $\beta(r)$ denote range-dependent attrition-rate coefficients. Range is related to time by

$$r(t) = R_0 - vt , \tag{3.3}$$

where R_0 denotes the opening range of battle and $v > 0$ denotes the constant attack speed. For example, let us consider the constant-speed attack of a homogeneous Y force against the static defensive position of a homogeneous X force. Figure 1 diagrammatically portrays this situation.

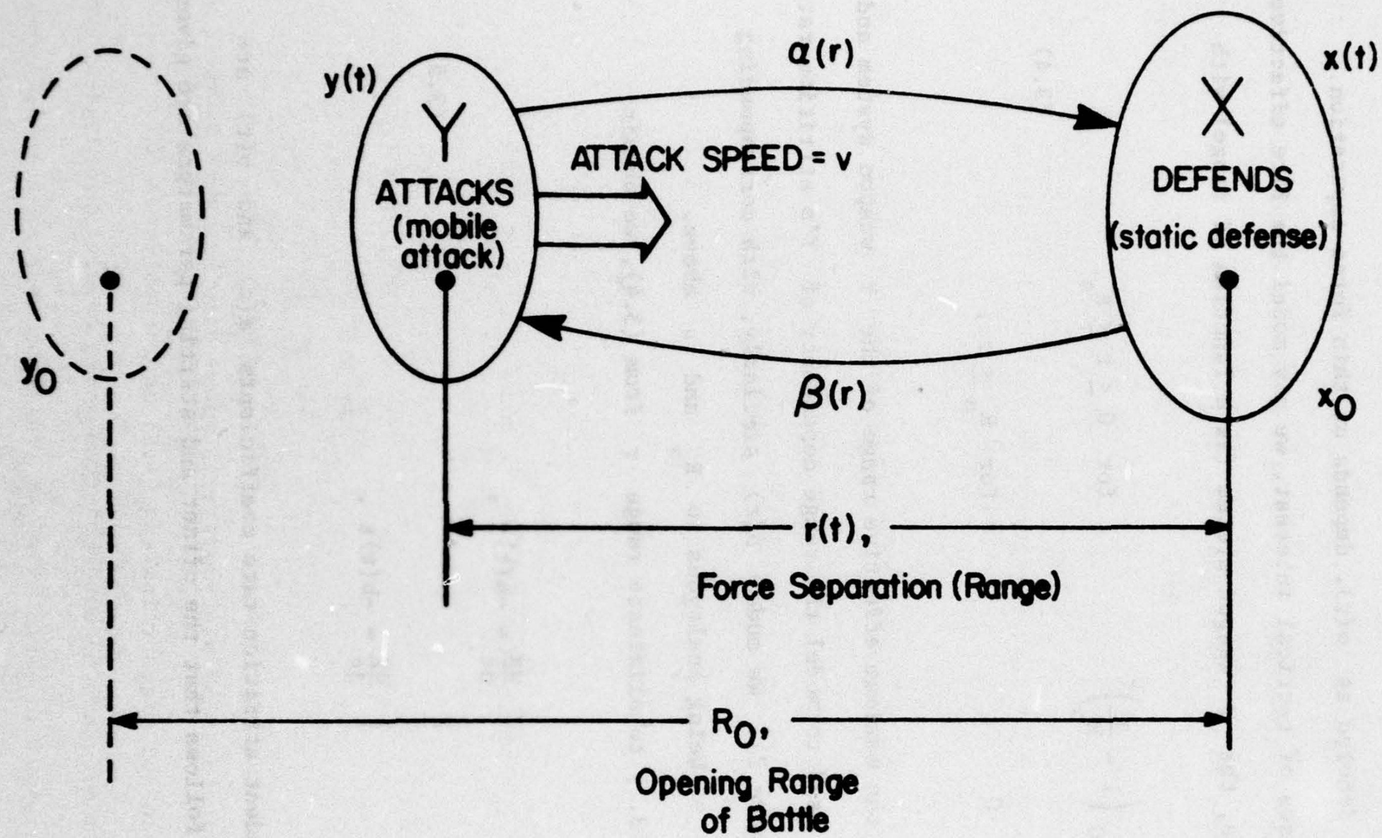

Figure 1. Diagram of Bonder's constant-speed attack model. Force separation, $r(t)$, is given by $r(t) = R_0 - vt$.

The basic idea is that force separation, i.e. range between the opposing forces, changes over time, and the fire effectiveness of, for example, a single Y firer, denoted as $\alpha(r)$, depends on this force separation.

In many cases of tactical interest, we may model the fire effectiveness of, for example, the Y weapon system (as a function of range) with

$$\alpha(r) = \begin{cases} \alpha_0 \left(1 - \frac{r}{R_\alpha}\right)^\mu & \text{for } 0 \leq r \leq R_\alpha, \\ 0 & \text{for } R_\alpha \leq r , \end{cases} \tag{3.4}$$

where R_α denotes the maximum effective range of the Y weapon system and $\mu \geq 0$. Here μ is used to model the range dependency of Y's attrition-rate coefficient (see Figure 2). We model $\beta(r)$ similarly, with corresponding quantities R_β and ν being analogous to R_α and μ above.

If we use (3.3) to eliminate range r from (3.4), we obtain

$$\begin{cases} \frac{dx}{dt} = -a(t)y , \\ \frac{dy}{dt} = -b(t)x , \end{cases} \tag{3.5}$$

where the time-dependent attrition-rate coefficients $a(t)$ and $b(t)$ are given by (3.1). It follows that the offset and starting parameters are given by

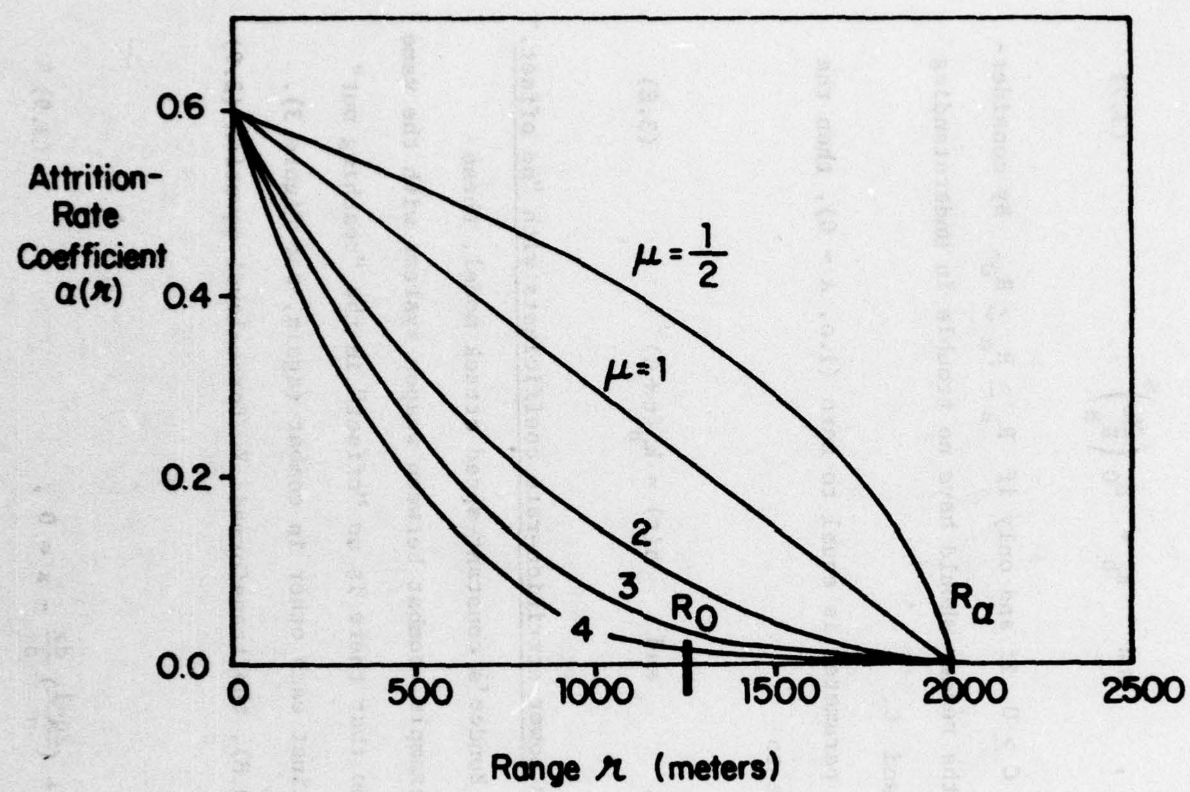

Figure 2. Dependence of Y's attrition-rate coefficient $\alpha(r)$ on the exponent μ with the maximum effective range of the weapon system and kill rate at zero range held constant. [NOTES: 1. The maximum effective range of the system is denoted as R_α = 2000 meters. 2. $\alpha(0) = \alpha_0 = 0.6X$ casualties/(unit time × number of Y firers) denotes the weapon-system kill rate for Y at zero force separation (range). 3. The opening range of battle is denoted as R_0 = 1250 meters and (as shown) $R_0 < R_\alpha$.]

$$A = \left(\frac{R_\beta - R_\alpha}{v}\right), \qquad \text{and} \qquad C = \left(\frac{R_\alpha - R_0}{v}\right), \tag{3.6}$$

and that

$$k_a = \alpha_0 \left(\frac{v}{R_\alpha}\right)^\mu \quad , \qquad \text{and} \qquad k_b = \beta_0 \left(\frac{v}{R_\beta}\right)^\nu . \tag{3.7}$$

We observe that A and $C \geq 0$ if and only if $R_\beta \geq R_\alpha \geq R_0$. By considering (3.6) and Figure 3, the reader should have no trouble in understanding our terminology for A and C.

When the offset parameter is equal to zero (i.e. $A = 0$), then the coefficients (3.1) reduce to

$$a(t) = k_a (t + C)^\mu, \qquad \text{and} \qquad b(t) = k_b (t + C)^\nu . \tag{3.8}$$

We will refer to (3.8) as power attrition-rate coefficients with "no offset." As we have seen above in Bonder's constant-speed attack model, these coefficients model, for example, combat between weapon systems with the same maximum effective range so that there is no "offset" in the "reaching out" of the weapon systems against each other in combat (again, see Figure 3). For these coefficients (3.8), the transformed X force-level equation (2.9) becomes

$$\frac{d^2x}{d\tau^2} + \left(\frac{2q-1}{\tau}\right) \frac{dx}{d\tau} - x = 0 , \tag{3.9}$$

with initial conditions

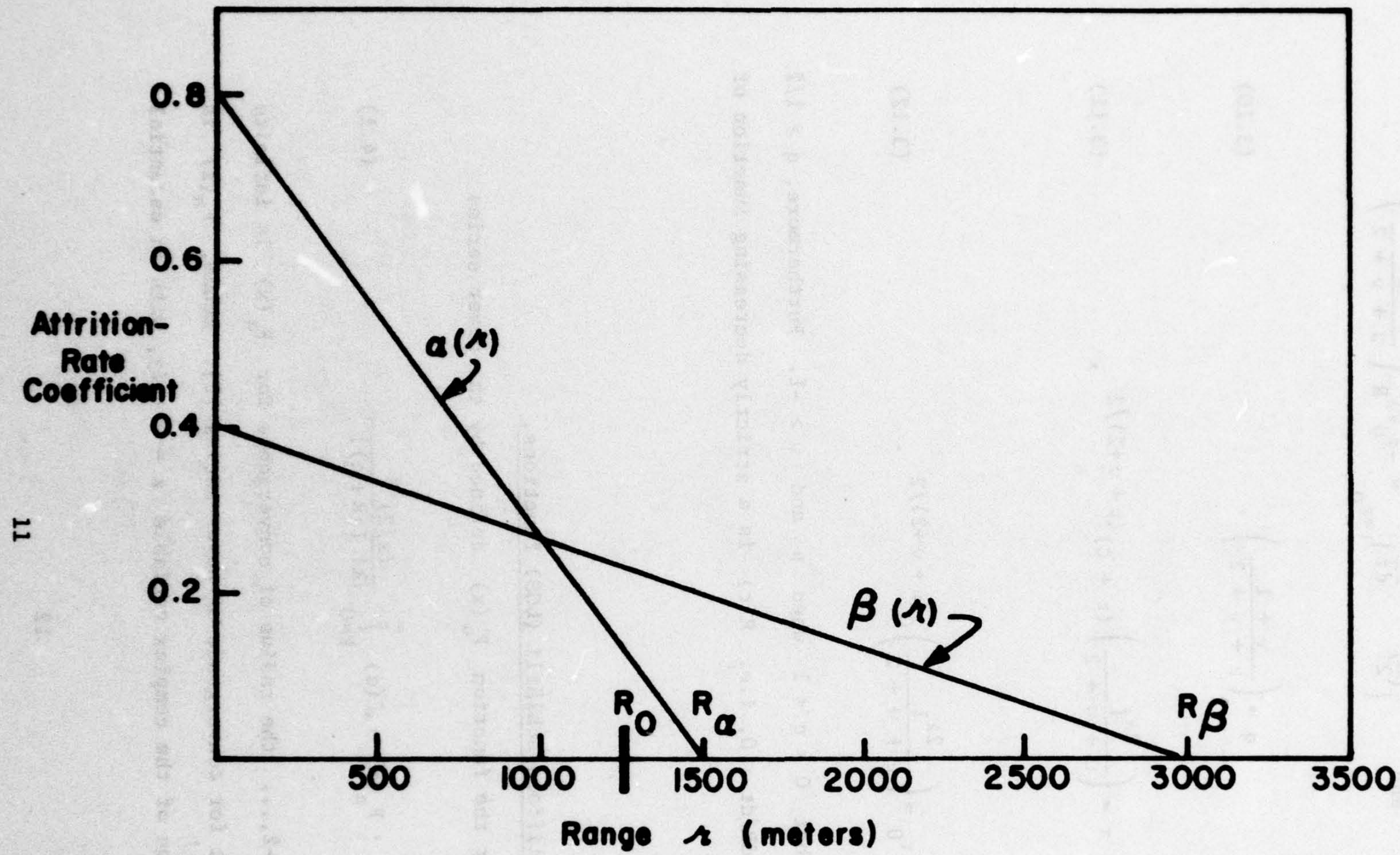

Figure 3. Explanation of the offset parameter A and the starting parameter C for power attrition-rate coefficients modelling constant-speed attack. [NOTES: 1. The maximum effective ranges of the X and Y weapon systems are denoted as R_α and R_β, respectively. 2. The opening range of battle is denoted as R_0 and (as shown) $R_0 < \text{minimum}(R_\alpha, R_\beta)$. 3. The offset parameter is given by $A = (R_\beta - R_\alpha)/v$. 4. The starting parameter is given by $C = (R_\alpha - R_0)/v$.]

$$x(\tau_0) = x_0 \,, \qquad \text{and} \qquad \left\{ \left(\frac{\tau}{2}\right)^{2q-1} \frac{dx}{d\tau} \right\}_{\tau=\tau_0} = -y_0\sqrt{\lambda_R} \left(\frac{\lambda_I}{\mu + \nu + 2} \right)^{2q-1} .$$

Here

$$q = \left(\frac{\nu + 1}{\mu + \nu + 2} \right) , \tag{3.10}$$

$$\tau = \left(\frac{2\lambda_I}{\mu + \nu + 2} \right) (t + C)^{(\mu+\nu+2)/2} , \tag{3.11}$$

and

$$\tau_0 = \left(\frac{2\lambda_I}{\mu + \nu + 2} \right) C^{(\mu+\nu+2)/2} . \tag{3.12}$$

Let us observe that $0 < q < 1$ when μ and $\nu > -1$. Furthermore, $q > 1/2$ if and only if $dR/dt < 0$, i.e. $R(t)$ is a strictly decreasing function of time.

4. Lanchester-Clifford-Schläfli (LCS) Functions.

Consider the function $F_\alpha(x)$ defined by the power series

$$F_\alpha(x) = \Gamma(\alpha) \sum_{k=0}^{\infty} \frac{(x/2)^{2k}}{\{k!\ \Gamma(k+\alpha)\}} . \tag{4.1}$$

For $\alpha \neq 0, -1, -2, \ldots$ the radius of convergence for $F_\alpha(x)$ is infinite by the ratio test for convergence of power series [2]. Hence, $F_\alpha(z)$ is an entire function of the complex variable $z = x + iy$, with an essential

singularity at the point at infinity. Now consider the function $H_\alpha(x)$ defined by the infinite series

$$H_\alpha(x) = \Gamma(\alpha) \sum_{k=0}^{\infty} \frac{(x/2)^{2(k+\alpha)}}{\{k!\ \Gamma(k+\alpha+1)\}} . \tag{4.2}$$

Observing that

$$H_\alpha(x) = (1/\alpha)(x/2)^{2\alpha} F_{\alpha+1}(x) , \tag{4.3}$$

we see that for $\alpha > 0$ the infinite series (4.2) is uniformly convergent on compact subsets of the complex plane. From (4.3) one can readily deduce the recursive relation

$$F_\alpha(x) = F_{\alpha+1}(x) + \left\{\frac{(x/2)^2}{\alpha(\alpha+1)}\right\} F_{\alpha+2}(x) . \tag{4.4}$$

We will call the functions $F_\alpha(x)$ and $H_\alpha(x)$ <u>Lanchester-Clifford-Schläfli</u> (LCS) functions (see Note 10 on pp. 66-67 of [5]). Other properties are readily deduced and are given in Table I.

The function $F_\alpha(x)$ satisfies the linear second-order ordinary differential equation

$$\frac{d^2F_\alpha}{dx^2} + \left(\frac{2\alpha-1}{x}\right)\frac{dF_\alpha}{dx} - F_\alpha = 0 , \tag{4.5}$$

with initial conditions

Table I. Properties of the LCS Functions $F_\alpha(x)$ and $H_\alpha(x)$.

1. $dF_\alpha/dx = (x/2)^{1-2\alpha}H_\alpha(x)$

2. $dH_\alpha/dx = (x/2)^{2\alpha-1}F_\alpha(x)$

3. $F_\alpha(x)F_{1-\alpha}(x) - H_\alpha(x)H_{1-\alpha}(x) = 1 \quad \forall x$

   where α is not an integer (including zero)

4. $F_\alpha(x=0) = 1$

5. $H_\alpha(x=0) = 0$ for $\alpha > 0$

6. $dF_\alpha/dx(x=0) = 0$

7. $\{(x/2)^{1-2\alpha}dH_\alpha/dx\}_{x=0} = 1$

8. $F_{1/2}(x) = \cosh x$

9. $H_{1/2}(x) = \sinh x$

$$F_\alpha(0) = 1, \qquad \text{and} \qquad \frac{dF_\alpha}{dx}(0) = 0 ,$$

while $H_\alpha(x)$ satisfies

$$\frac{d^2H_\alpha}{dx^2} - \left(\frac{2\alpha-1}{x}\right)\frac{dH_\alpha}{dx} - H_\alpha = 0 , \tag{4.6}$$

with initial conditions

$$H_\alpha(0) = 0 , \qquad \text{and} \qquad \left\{\left(\frac{x}{2}\right)^{1-2\alpha}\frac{dH_\alpha}{dx}\right\}_{x=0} = 1 .$$

Thus, $\{F_\alpha, H_{1-\alpha}\}$ is a fundamental system of solutions to

$$\frac{d^2F}{dx^2} + \left(\frac{2\alpha-1}{x}\right)\frac{dF}{dx} - F = 0 , \tag{4.7}$$

with Wronskian $W(F_\alpha, H_{1-\alpha}) = (x/2)^{1-2\alpha}$. It follows that the GLF for the X and Y force-level equations for combat modelled with the attrition-rate coefficients (3.8) are given by

$$C_X(t) = F_q(\tau(t)), \qquad S_X(t) = \left(\frac{\lambda_I}{\mu+\nu+2}\right)^{2q-1} H_p(\tau(t)) , \tag{4.8}$$

$$C_Y(t) = F_p(\tau(t)), \qquad S_Y(t) = \left(\frac{\lambda_I}{\mu+\nu+2}\right)^{1-2q} H_q(\tau(t)) , \tag{4.9}$$

where $p = 1-q$. If we define

$$T_\alpha(x) = H_{1-\alpha}(x)/F_\alpha(x) \ , \tag{4.10}$$

then

$$T_X(t) = \frac{S_X(t)}{C_X(t)} = \left(\frac{\lambda_I}{\mu+\nu+2}\right)^{2q-1} \frac{H_p(\tau(t))}{F_q(\tau(t))} \ , \tag{4.11}$$

or

$$T_X(t) = \left(\frac{\lambda_I}{\mu+\nu+2}\right)^{2q-1} T_q(\tau(t)) \ , \tag{4.12}$$

where $T_X(t)$ denotes a hyperbolic-like GLF, which corresponds to the hyperbolic tangent. Observing that for $\mu, \nu > -1$, $\lim_{\tau \to +\infty} \tau(t) = +\infty$, we see that $T_\alpha(x)$ is a strictly increasing function of x on the interval $[0, +\infty)$ and

$$0 \le T_\alpha(x) < \frac{\Gamma(1-\alpha)}{\Gamma(\alpha)} \qquad \text{for} \quad 0 \le x < +\infty \ , \tag{4.13}$$

with

$$\lim_{x \to +\infty} T_\alpha(x) = \frac{\Gamma(1-\alpha)}{\Gamma(\alpha)} \ , \tag{4.14}$$

since by the results of Taylor and Comstock [7] the parity-condition parameter $Q^* = Q^*(\mu, \nu, C = 0)$ is given by

$$\lim_{t \to +\infty} T_X(t) = \frac{1}{Q^*(\mu, \nu, 0)} = \left(\frac{\lambda_I}{\mu+\nu+2}\right)^{2q-1} \frac{\Gamma(p)}{\Gamma(q)} \ . \tag{4.15}$$

We recall that Taylor and Comstock [7] have introduced the so-called parity-condition parameter Q^* as the value (or range of such values) for the initial condition Q to the initial-value problem

$$\begin{cases} \dfrac{dE_X^-}{dt} = -\dfrac{1}{\sqrt{\lambda_R}} a(t)E_Y^- & \text{with } E_X^-(t_0) = 1 , \\ \dfrac{dE_Y^-}{dt} = -\sqrt{\lambda_R}\, b(t)E_X^- & \text{with } E_Y^-(t_0) = Q , \end{cases} \tag{4.16}$$

such that $E_X^-(t;Q^*)$ and $E_Y^-(t;Q^*) > 0$ for all $t \geq t_0$. In other words, Q^* is the value of Q in (4.16) above such that neither E_X^- nor E_Y^- ever become zero. In this case, both $E_X^-(t;Q^*)$ and $E_Y^-(t;Q^*)$ are positive, strictly decreasing functions, similar to decreasing exponentials. Thus, we may call Q^* "the Y equivalent of an X force of unit strength," since the forces are "at parity," with neither force being annihilated in finite time. Taylor and Comstock have shown that for either $a(t) \notin L(0,+\infty)$ or $b(t) \notin L(0,+\infty)$, then Q^* is unique and given by

$$\lim_{t\to+\infty} \frac{S_X(t)}{C_X(t)} = \frac{1}{Q^*} . \tag{4.17}$$

The significance of the parity-condition parameter Q^* is that it allows us to predict force annihilation as the following theorem shows.

THEOREM 1 (Taylor and Comstock [7]): Assume that either $a(t) \notin L(0,+\infty)$ or $b(t) \notin L(0,+\infty)$. Then the X force will be annihilated in finite time if and only if

$$\frac{x_0}{y_0} < \sqrt{\lambda_R} \left\{ \frac{C_X(0) - Q^*S_X(0)}{Q^*C_Y(0) - S_Y(0)} \right\} . \tag{4.18}$$

5. <u>Use of LCS Functions for Analyzing Combat</u>.

The Lanchester-Clifford-Schläfli (LCS) functions $F_\alpha(x)$ and $H_\alpha(x)$ are useful for analyzing "aimed-fire" combat (see Section 3 above) modelled with the power attrition-rate coefficients with "no offset" (3.8), which we rewrite here as

$$a(t) = k_a(t + C)^\mu, \qquad \text{and} \qquad b(t) = k_b(t + C)^\nu . \tag{5.1}$$

In other words, the LCS functions arise in solving the differential combat model (2.1) with attrition-rate coefficients (5.1). In order that both $a(t)$ and $b(t) \in L(t_0,T)$, we must have μ and $\nu > -1$. Military situations modelled by these equations have been discussed in Section 3 above, e.g. combat between two weapon *systems with the same maximum effective range.* For such combat, the LCS functions may be used to

(1) compute force-level declines,

(2) predict force annihilation,

and (3) predict the time of force annihilation.

Let us now see how the LCS functions may be used to obtain the above information about force-level declines and force-annihilation prediction. According to (2.4), (4.8), and (4.9) above, the X force level is given by

$$x(t) = x_0\{F_p(\tau_0)\, F_q(\tau(t)) - H_q(\tau_0)\, H_p(\tau(t))\}$$

$$- y_0 \sqrt{\lambda_R} \left(\frac{\lambda_I}{\mu + \nu + 2} \right)^{2q-1} \{F_q(\tau_0)H_p(\tau(t)) - H_p(\tau_0)F_q(\tau(t))\}, \tag{5.2}$$

where q is given by (3.10), $p = 1-q$, and $\tau(t)$ is given by (3.11), which we rewrite as

$$\tau(t) = \left(\frac{2\lambda_I}{\mu + \nu + 2} \right) (t + C)^{(\mu+\nu+2)/2} . \tag{5.3}$$

The time to annihilate the X force* is determined by $x(t_a^X) = 0$, and it follows that

$$T_q(\tau(t_a^X)) = \frac{x_0 F_p(\tau_0) + y_0 \sqrt{\lambda_R} \left(\frac{\lambda_I}{\mu + \nu + 2} \right)^{q-p} H_p(\tau_0)}{x_0 H_q(\tau_0) + y_0 \sqrt{\lambda_R} \left(\frac{\lambda_I}{\mu + \nu + 2} \right)^{q-p} F_q(\tau_0)} , \tag{5.4}$$

where from (4.10)

$$T_q(\tau(t)) = H_p(\tau(t))/F_q(\tau(t)) , \tag{5.5}$$

and we recall that $p + q = 1$. It follows that the time to annihilate X, t_a^X, is given by

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*If we multiply the first equation of (2.1) by y, the second by x, add, and integrate, we obtain

$$x(t)\, y(t) = x_0 y_0 - \int_0^t \{a(s)\, y^2(s) + b(s)\, x^2(s)\} ds ,$$

which shows that $x(t)$ and $y(t)$ can have at most one finite zero. Hence, if $x(t_a^X) = 0$, then we know that $y(t) > 0$ for all $t \geq 0$.

$$t_a^X = \tau^{-1}\left\{ T_q^{-1}\left[\frac{x_0 F_p(\tau_0) + y_0\sqrt{\lambda_R}\left(\dfrac{\lambda_I}{\mu+\nu+2}\right)^{q-p} H_p(\tau_0)}{x_0 H_q(\tau_0) + y_0\sqrt{\lambda_R}\left(\dfrac{\lambda_I}{\mu+\nu+2}\right)^{q-p} F_q(\tau_0)} \right] \right\} . \tag{5.6}$$

Taylor and Comstock [7] have shown that $T_q(\tau)$ is strictly increasing and satisfies (see also (4.12) above)

$$0 \leq T_q(\tau) < \Gamma(p)/\Gamma(q) , \tag{5.7}$$

where $p = 1-q$. It follows that in order for X to be annihilated in finite time, the right-hand side of (5.4) must be less than $\Gamma(p)/\Gamma(q)$. Let us observe that for $t_0 = -C = 0$, (5.4) simplifies to

$$T_q(\tau(t_a^X)) = \frac{x_0}{y_0\sqrt{\lambda_R}}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{p-q} . \tag{5.8}$$

Thus, we have proved the following theorem concerning force-annihilation prediction.

THEOREM 2: Consider combat between two homogeneous forces modelled by (2.1) with power attrition-rate coefficients (5.1). Assume that μ and $\nu > -1$ and that the above equations hold for all time. Then the X force will be annihilated in finite time if and only if

$$\Gamma(q)\left\{x_0F_p(\tau_0) + y_0\sqrt{\lambda_R}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{q-p}H_p(\tau_0)\right\}$$

$$< \Gamma(p)\left\{x_0H_q(\tau_0) + y_0\sqrt{\lambda_R}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{q-p}F_q(\tau_0)\right\}, \tag{5.9}$$

where $q = (\nu + 1)/(\mu + \nu + 2)$ and $p = 1-q$. For $t_0 = 0$ (i.e. $C = 0$ so that $\tau_0 = 0$), X will be annihilated in finite time if and only if

$$\frac{x_0}{y_0} < \frac{\Gamma(p)}{\Gamma(q)}\sqrt{\lambda_R}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{q-p}. \tag{5.10}$$

6. Tabulation of LCS Functions.

This report contains the most extensive set of tables of the Lanchester-Clifford-Schläfli functions currently available. The Appendix contains tables of five-decimal-place values of the hyperbolic-like LCS functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for various values of the argument x, namely $x = 0.00\ (0.01)\ 2.00\ (0.1)\ 10.0$, and $\alpha = 1/2, 1/3, 2/3, 1/4, 3/4, 1/5, 2/5, 3/5, 4/5, 2/7, 3/7, 4/7, 5/7, 4/9, 5/9, 3/11, 5/11, 6/11, 8/11, 5/13, 8/13, 5/17, 12/17, 5/21$, and $16/21$. These values of the index α correspond to $\mu, \nu = 0, 1/4, 1/2, 1, 1\frac{1}{2}, 2$, and 3 in (3.8) and allow one to analyze, for example, a fairly wide variety of range capabilities for weapon systems in the constant-speed-attack model of Section 3. These

tables have been calculated by the recursive means given in Section 8 of [5]. A less extensive tabulation (namely, for $\alpha = 1/2, 1/3, 2/3, 1/4, 3/4, 1/5, 2/5, 3/5, 4/5, 3/7$, and $4/7$ corresponding to $\mu, \nu = 0, 1, 2, 3$) is to be found in a companion report [8].

A representative tabulation of the hyperbolic-like LCS functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ is given in, for example, Tables 8A and 8B of the Appendix for $\alpha = 3/5$. The values of the argument x are the same as those used for the tabulation of the hyperbolic functions by Abramowitz and Stegun [1]. We observe from Table 8B and (4.13) that the limiting value of $T_\alpha(x)$ as $x \to +\infty$ (here $\alpha = 3/5$) is quickly reached, with three-decimal-place accuracy already attained for $x = 4.5$. Moreover, the use of these tables (specifically, Tables 8A and 8B of the Appendix) for combat analysis is illustrated in the next section.

7. Numerical Examples

In this section we examine a couple of numerical examples to show some of the insights that may be gained into the dynamics of combat between two homogeneous forces from our results (see also [6]). These examples illustrate the use of the LCS functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for analyzing "aimed-fire" combat modelled with the power attrition-rate coefficients with "no offset" (5.1). As in [4-7], we consider S. Bonder's model (3.2) for the constant-speed attack against a static defensive position. We will focus on the use of the LCS functions for predicting force annihilation, since the computing of force-level trajectories with Lanchester functions is adequately handled elsewhere (see [4-5]).

Let us accordingly consider the constant-speed attack of a homogeneous Y force against the static defensive position of a homogeneous X force (see Section 3 above for further modelling details, especially Figure 1). For our numerical computations, we assume that the fire effectiveness of the Y weapon system varies linearly with range, i.e.

$$\alpha(r) = \begin{cases} \alpha_0 \left(1 - \frac{r}{R_\alpha}\right) & \text{for } 0 \leq r \leq R_\alpha, \\ 0 & \text{for } R_\alpha \leq r, \end{cases} \tag{7.1}$$

and that the fire effectiveness of the X weapon system varies quadratically with range, i.e.

$$\beta(r) = \begin{cases} \beta_0 \left(1 - \frac{r}{R_\beta}\right)^2 & \text{for } 0 \leq r \leq R_\beta, \\ 0 & \text{for } R_\beta \leq r, \end{cases} \tag{7.2}$$

with $R_\alpha = R_\beta$, i.e. both weapon systems have the same maximum effective range. In other words, $\mu = 1$ in (3.4) and $\nu = 2$ for $\beta(r)$. We consider a battle modelled by the input data given in Table II. In terms of time as the independent variable, the attrition-rate coefficients (7.1) and (7.2) become via (3.3)

$$a(t) = k_a(t + C) \quad \text{and} \quad b(t) = k_b(t + C)^2, \tag{7.3}$$

Table II. Input Data for Numerical Examples

$\mu = 1, \quad \nu = 2$

$\alpha_0 = 0.06$ X casualties/minute/Y firer

$\beta_0 = 0.6$ Y casualties/minute/X firer

$R_\alpha = R_\beta = 2000$ meters

$v = 5$ miles/hour

where $R_\alpha = R_\beta$,

$$C = \frac{R_\alpha - R_0}{v}, \quad k_a = \frac{\alpha_0 v}{R_\alpha}, \quad \text{and} \quad k_b = \beta_0 \left(\frac{v}{R_\beta} \right)^2 . \tag{7.4}$$

From the input data given in Table II, we compute the parameter values shown in Table III, since the transformed X force-level equation is given by (3.9) with $q = (\nu + 1)/(\mu + \nu + 2)$, $p = 1-q$, $\mu = 1$, and $\nu = 2$. Thus, the X force level may be computed with $F_\alpha(\tau)$ and $H_{1-\alpha}(\tau)$ with $\alpha = q = 3/5$. Force-annihilation prediction involves the limiting value of $T_\alpha(\tau) = H_{1-\alpha}(\tau)/F_\alpha(\tau)$ as $\tau \to +\infty$. From Table 8B of the Appendix and Table III, we note the predicted agreement between $\Gamma(1-\alpha)/\Gamma(\alpha)$ and the limiting value of $T_\alpha(x)$ as $x \to +\infty$ [recall (4.13)] for $\alpha = q = 3/5$. We now consider two cases: (I) $R_0 = 2000$ meters, and (II) $R_0 = 1250$ meters.

When $R_0 = 2000$ meters (see Figure 3 of [4]), we have $C = 0$ and $\tau_0 = 0$. The maximum time that the battle can last is $t_{max} = R_0/v = 14.91$ minutes, since at this time the attackers reach their final objective, i.e. the defender's position (again, see Figure 1). We now consider the qualitative behavior of the $\mu = 1$, $\nu = 2$ force-level trajectory shown in Figure 3 of [4]. Theorem 2 tells us that the X force can be annihilated in finite time if and only if

$$\frac{x_0}{y_0} < \frac{\Gamma(p)}{\Gamma(q)} \sqrt{\lambda_R} \left(\frac{\lambda_I}{\mu + \nu + 2} \right)^{q-p} , \tag{7.3}$$

where $q = 3/5$ and $p = 1-q$. Using the numerical values in Table III, we compute from (7.3) that the X force can be annihilated in finite time if and only if

Table III. Parameter Values for Numerical Examples

$k_a = 4.0233 \times 10^{-3}$ X casualties/(minute)$^{\mu}$/Y firer

$k_b = 2.6979 \times 10^{-3}$ Y casualties/(minute)$^{\nu}$/X firer

$p = 2/5, \quad q = 3/5$

$\Gamma(p)/\Gamma(q) = 1.48951$

$A = 0$

$$\frac{x_0}{y_0} < 0.420 \ . \tag{7.4}$$

When the X force can be annihilated, its annihilation time is given by (5.8), which we rewrite here as

$$T_q(\tau(t_a^X)) = \frac{x_0}{y_0 \sqrt{\lambda_R}} \left(\frac{\lambda_I}{\mu + \nu + 2} \right)^{p-q} , \tag{7.5}$$

where

$$\tau(t) = \left(\frac{2\lambda_I}{\mu + \nu + 2} \right) t^{(\mu+\nu+2)/2} \ . \tag{7.6}$$

Thus, for the numerical values given in Table III, the time of annihilation of the X force is given by

$$T_q(\tau(t_a^X)) = 3.544 \ \frac{x_0}{y_0} , \tag{7.7}$$

with $q = 3/5$. We will now illustrate further computations for $x_0 = 10$ and $y_0 = 30$. From (7.4) we see that the X force can be annihilated in finite time (but we must verify that $t_a^X \leq t_{max}$). In this case (7.7) becomes

$$T_q(\tau(t_a^X)) = 1.18122 \ . \tag{7.8}$$

We must now determine $\tau(t_a^X)$ such that $\tau(t_a^X) = T_q^{-1}(1.18122)$ by using interpolation methods and Tables 8A and 8B. From Table 8A, we find

$T_q(\tau) = 1.18172$ for $= 1.01$

$T_q(\tau) = 1.17630$ for $= 1.00$

so that using linear interpolation, we obtain

$$\tau(t_a^X) = 1.009 \, , \tag{7.9}$$

whence use of (7.6) yields

$$t_a^X = 14.24 \text{ minutes}, \tag{7.10}$$

which is less than $t_{max} = 14.91$ minutes so that the defending X force is indeed annihilated before the attacking Y force reaches its final objective. Since $r(t) = R_0 - vt$, we find that force separation at the instant of annihilation of the X force is

$$r_a^X = 89.8 \text{ meters} \, . \tag{7.11}$$

Further results may be computed in a similar fashion and are given in Table IV.

When $R_0 = 1250$ meters (see Figure 3 of [5]), we have $C = 5.5923$ minutes, $\tau_0 = 0.0975$, and $t_{max} = R_0/v = 9.32$ minutes. In this case Theorem 2 tells us that the X force can be annihilated in finite time if and only if

Table IV. Annihilation of the X Force as a Function of the Initial Force Ratio for R_0 = 2000 meters

(x_0/y_0)	t_a^X (minutes)	r_a^X (meters)
0.333	14.24	89.8
0.250	11.61	443.2
0.200	10.19	633.2

$$\frac{x_0}{y_0} < \sqrt{\lambda_R}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{q-p}\frac{\Gamma(p)}{\Gamma(q)}\;\frac{\left\{F_q(\tau_0)-\frac{\Gamma(q)}{\Gamma(p)}H_p(\tau_0)\right\}}{\left\{F_p(\tau_0)-\frac{\Gamma(p)}{\Gamma(q)}H_q(\tau_0)\right\}}\quad, \tag{7.12}$$

with $q = 3/5$ and $p = 1-q$. Using linear interpolation, we obtain from Tables 7A and 8A of the Appendix that for the numerical values of Table III

$$\begin{aligned} F_p(\tau_0) &= 1.006\ , & H_q(\tau_0) &= 0.044\ , \\ F_q(\tau_0) &= 1.004\ , & H_p(\tau_0) &= 0.223\ , \end{aligned} \tag{7.13}$$

so that (7.12) says that the X force can be annihilated if and only if

$$\frac{x_0}{y_0} < 0.382\ . \tag{7.14}$$

When the X force can be annihilated, its annihilation time is given by (5.4), which we rewrite here as

$$T_q(\tau(t_a^X)) = \frac{\left\{\frac{x_0}{y_0\sqrt{\lambda_R}}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{p-q}F_p(\tau_0)+H_p(\tau_0)\right\}}{\left\{F_q(\tau_0)+\frac{x_0}{y_0\sqrt{\lambda_R}}\left(\frac{\lambda_I}{\mu+\nu+2}\right)^{p-q}H_q(\tau_0)\right\}}\quad, \tag{7.15}$$

whence for the data of Table III

$$T_a(\tau(t_a^X)) = \frac{3.565u_0+0.223}{0.156u_0+1.004}\ , \tag{7.16}$$

where $u_0 = x_0/y_0$. Let us also record here that (3.11) yields

$$t = \left(\frac{\{\mu + \nu + 2\}\tau}{2\lambda_I}\right)^{2/(\mu+\nu+2)} - C \ . \tag{7.17}$$

We will again illustrate further computations for $x_0 = 10$ and $y_0 = 30$. From (7.14) we see that the X force can be annihilated in finite time (but again we must investigate whether or not $t_a^X \leq t_{max}$). In this case (7.16) becomes

$$T_q(\tau(t_a^X)) = 1.33651 \ , \tag{7.18}$$

whence Table 8A of the Appendix and linear interpolation yield

$$\tau(t_a^X) = 1.397 \ , \tag{7.19}$$

so that by (7.17)

$$t_a^X = 10.63 \text{ minutes} \ . \tag{7.20}$$

Since $t_{max} = R_0/v = 9.32$ minutes $< t_a^X$, we see that the attacking Y force overruns the defender's position before annihilation of the X force occurs. Thus, the battle ends with $x_f = x(t_f) > 0$ and $y_f > 0$ at $t_f = t_{max} = 9.32$ minutes. Corresponding to $t_f = 9.32$ minutes is $\tau_f = 1.1318$, and then Table 8A of the Appendix yields

$$F_q(\tau_f = 1.1318) = 1.589 \ , \qquad H_p(1.1318) = 1.973 \ , \tag{7.21}$$

whence via (2.4), (4.8), (4.9), and (7.13) we obtain

$$x_f = x(t_f) = x(r = 0) = 1.35 \ . \tag{7.22}$$

Some further numerical results are given in Table V. Again, these parametric results should be contrasted with the single $\mu = 1$, $\nu = 2$ force-level trajectory shown in Figure 3 of [5].

8. Final Remarks

In the previous section above, we have seen how the LCS functions allow one to conveniently obtain much valuable information about the model (2.1) with power attrition-rate coefficients (3.8) without having to explicitly compute the entire force-level trajectories. Previously we were limited to computing only force-level trajectories (see [4-5]). With the availability of these tabulations of LCS functions (see the Appendix of this report and [8]), we can now tell who is going to be annihilated and when this event will happen without having to compute the trajectories. Not only did we answer questions about the qualitative behavior of the model (e.g. force annihilation) for specific values of, for example, initial force levels but also for a range of values of the initial force ratio (i.e. parametric analysis of model behavior).

Table V. Annihilation of the X Force as a Function of the Initial Force Ratio for R_0 = 1250 meters

(x_0/y_0)	t_a^X (minutes)	r_a^X (meters)
0.333	10.63	———†
0.250	7.56	235.9
0.200	6.17	422.8

†t_{max} = 9.32 minutes and $x_f = x(r=0) = 1.35$.

The results of this report may be used for other parametric analyses, e.g. parametric dependence of battle outcome on attrition-rate coefficients. Thus, the contents of this report allow one to develop important insights into the dynamics of combat between two homogeneous forces with temporal variations in fire effectiveness. With the availability of tabulations of the LCS functions, one can now analyze such combat modelled by the power attrition-rate coefficients (3.8) with somewhat the same facility as he can for the constant-coefficient case and thus aid in parametric analyses. For further discussions of the significance of such results for military operations research, the reader is directed to [6] and [7].

REFERENCES

1. M. ABRAMOWITZ and I. STEGUN (Editors), Handbook of Mathematical Functions, National Bureau of Standards Applied Mathematics Series, No. 55, Washington, D.C., 1964.

2. K. KNOPP, Infinite Sequences and Series, Dover, New York, 1956.

3. F. W. LANCHESTER, "Aircraft in Warfare: The Dawn of the Fourth Arm-No. V., The Principle of Concentration," Engineering 98, 422-423 (1914) (reprinted on pp. 2138-2148 of The World of Mathematics, J. Newman (Editor), Simon and Schuster, New York, 1956).

4. J. G. TAYLOR, "Solving Lanchester-Type Equations for 'Modern Warfare' with Variable Cofficients," Opns. Res. 22, 756-770 (1974).

5. J. G. TAYLOR and G. G. BROWN, "Canonical Methods in the Solution of Variable-Coefficient Lanchester-Type Equations of Modern Warfare," Opns. Res. 24, 44-69 (1976).

6. J. G. TAYLOR and G. G. BROWN, "Further Canonical Methods in the Solution of Variable-Coefficient Lanchester-Type Equations of Modern Warfare," NPS55-77-27, Naval Postgraduate School, Monterey, California, June 1977.

7. J. G. TAYLOR and C. COMSTOCK, "Force-Annihilation Conditions for Variable-Coefficient Lanchester-Type Equations of Modern Warfare," Naval Res. Log. Quart. 24, 349-371 (1977).

8. J. G. TAYLOR and G. G. BROWN, "A Short Table of Lanchester-Clifford-Schläfli Functions," NPS55-77-42, Naval Postgraduate School, Monterey, California, October 1977.

APPENDIX: **Tabulation of the LCS Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for α = 1/2, 1/3, 2/3, 1/4, 3/4, 1/5, 2/5, 3/5, 4/5, 2/7, 3/7, 4/7, 5/7, 4/9, 5/9, 3/11, 5/11, 6/11, 8/11, 5/13, 8/13, 5/17, 12/17, 5/21, and 16/21.**

$\alpha = 1/2$

x	$F_{1/2}(x)$	$H_{1/2}(x)$	$T_{1/2}(x)$	x	$F_{1/2}(x)$	$H_{1/2}(x)$	$T_{1/2}(x)$	x	$F_{1/2}(x)$	$H_{1/2}(x)$	$T_{1/2}(x)$
0.0	1.00000	0.0	0.0	0.50	1.12763	0.52110	0.46212	1.00	1.54308	1.17520	0.76159
0.01	1.00005	0.01000	0.01000	0.51	1.13289	0.53240	0.46995	1.01	1.55491	1.19069	0.76576
0.02	1.00020	0.02000	0.02000	0.52	1.13827	0.54375	0.47770	1.02	1.56689	1.20630	0.76987
0.03	1.00045	0.03000	0.02999	0.53	1.14377	0.55516	0.48538	1.03	1.57904	1.22203	0.77391
0.04	1.00080	0.04001	0.03998	0.54	1.14938	0.56663	0.49299	1.04	1.59134	1.23788	0.77789
0.05	1.00125	0.05002	0.04996	0.55	1.15510	0.57815	0.50052	1.05	1.60379	1.25386	0.78181
0.06	1.00180	0.06004	0.05993	0.56	1.16094	0.58973	0.50798	1.06	1.61641	1.26996	0.78566
0.07	1.00245	0.07006	0.06989	0.57	1.16690	0.60137	0.51536	1.07	1.62919	1.28619	0.78946
0.08	1.00320	0.08009	0.07983	0.58	1.17297	0.61307	0.52267	1.08	1.64214	1.30254	0.79320
0.09	1.00405	0.09012	0.08976	0.59	1.17916	0.62483	0.52990	1.09	1.65525	1.31903	0.79688
0.10	1.00500	0.10017	0.09967	0.60	1.18547	0.63665	0.53705	1.10	1.66852	1.33565	0.80050
0.11	1.00606	0.11022	0.10956	0.61	1.19189	0.64854	0.54413	1.11	1.68196	1.35240	0.80406
0.12	1.00721	0.12029	0.11943	0.62	1.19844	0.66049	0.55113	1.12	1.69557	1.36929	0.80757
0.13	1.00846	0.13037	0.12927	0.63	1.20510	0.67251	0.55805	1.13	1.70934	1.38631	0.81102
0.14	1.00982	0.14046	0.13909	0.64	1.21189	0.68459	0.56490	1.14	1.72329	1.40347	0.81441
0.15	1.01127	0.15056	0.14889	0.65	1.21879	0.69675	0.57167	1.15	1.73741	1.42078	0.81775
0.16	1.01283	0.16068	0.15865	0.66	1.22582	0.70897	0.57836	1.16	1.75171	1.43822	0.82104
0.17	1.01448	0.17082	0.16838	0.67	1.23297	0.72126	0.58498	1.17	1.76618	1.45581	0.82427
0.18	1.01624	0.18097	0.17808	0.68	1.24025	0.73363	0.59152	1.18	1.78083	1.47355	0.82745
0.19	1.01810	0.19115	0.18775	0.69	1.24765	0.74607	0.59798	1.19	1.79565	1.49143	0.83058
0.20	1.02007	0.20134	0.19738	0.70	1.25517	0.75858	0.60437	1.20	1.81066	1.50946	0.83365
0.21	1.02213	0.21155	0.20697	0.71	1.26282	0.77117	0.61068	1.21	1.82584	1.52764	0.83668
0.22	1.02430	0.22178	0.21652	0.72	1.27059	0.78384	0.61691	1.22	1.84121	1.54598	0.83965
0.23	1.02657	0.23203	0.22603	0.73	1.27849	0.79659	0.62307	1.23	1.85676	1.56447	0.84258
0.24	1.02894	0.24231	0.23550	0.74	1.28652	0.80941	0.62915	1.24	1.87250	1.58311	0.84546
0.25	1.03141	0.25261	0.24492	0.75	1.29468	0.82232	0.63515	1.25	1.88842	1.60192	0.84828
0.26	1.03399	0.26294	0.25430	0.76	1.30297	0.83530	0.64108	1.26	1.90454	1.62088	0.85106
0.27	1.03667	0.27329	0.26362	0.77	1.31139	0.84838	0.64693	1.27	1.92084	1.64001	0.85380
0.28	1.03946	0.28367	0.27291	0.78	1.31994	0.86153	0.65271	1.28	1.93734	1.65930	0.85648
0.29	1.04235	0.29408	0.28213	0.79	1.32862	0.87478	0.65841	1.29	1.95403	1.67876	0.85913
0.30	1.04534	0.30452	0.29131	0.80	1.33743	0.88811	0.66404	1.30	1.97091	1.69838	0.86172
0.31	1.04844	0.31499	0.30044	0.81	1.34638	0.90152	0.66959	1.31	1.98800	1.71818	0.86428
0.32	1.05164	0.32549	0.30951	0.82	1.35547	0.91503	0.67507	1.32	2.00528	1.73814	0.86678
0.33	1.05495	0.33602	0.31852	0.83	1.36468	0.92863	0.68048	1.33	2.02276	1.75828	0.86925
0.34	1.05836	0.34659	0.32748	0.84	1.37404	0.94233	0.68581	1.34	2.04044	1.77860	0.87167
0.35	1.06188	0.35719	0.33638	0.85	1.38353	0.95612	0.69107	1.35	2.05833	1.79909	0.87405
0.36	1.06550	0.36783	0.34521	0.86	1.39316	0.97000	0.69626	1.36	2.07643	1.81977	0.87639
0.37	1.06923	0.37850	0.35399	0.87	1.40293	0.98398	0.70137	1.37	2.09473	1.84062	0.87869
0.38	1.07307	0.38921	0.36271	0.88	1.41284	0.99806	0.70642	1.38	2.11324	1.86166	0.88095
0.39	1.07702	0.39996	0.37136	0.89	1.42289	1.01224	0.71139	1.39	2.13196	1.88289	0.88317
0.40	1.08107	0.41075	0.37995	0.90	1.43309	1.02652	0.71630	1.40	2.15090	1.90430	0.88535
0.41	1.08523	0.42158	0.38847	0.91	1.44342	1.04090	0.72113	1.41	2.17005	1.92591	0.88749
0.42	1.08950	0.43246	0.39693	0.92	1.45390	1.05539	0.72590	1.42	2.18942	1.94770	0.88960
0.43	1.09388	0.44337	0.40532	0.93	1.46453	1.06998	0.73059	1.43	2.20900	1.96970	0.89167
0.44	1.09837	0.45434	0.41364	0.94	1.47530	1.08468	0.73522	1.44	2.22881	1.99188	0.89370
0.45	1.10297	0.46534	0.42190	0.95	1.48623	1.09948	0.73978	1.45	2.24884	2.01427	0.89569
0.46	1.10768	0.47640	0.43008	0.96	1.49729	1.11440	0.74428	1.46	2.26910	2.03686	0.89765
0.47	1.11250	0.48750	0.43820	0.97	1.50851	1.12943	0.74870	1.47	2.28958	2.05965	0.89958
0.48	1.11743	0.49865	0.44624	0.98	1.51988	1.14457	0.75307	1.48	2.31029	2.08265	0.90147
0.49	1.12247	0.50984	0.45422	0.99	1.53141	1.15983	0.75736	1.49	2.33123	2.10586	0.90332
0.50	1.12763	0.52110	0.46212	1.00	1.54308	1.17520	0.76159	1.50	2.35241	2.12928	0.90515

TABLE 1A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 1/2$ and x from 0.00 to 1.50.

$\alpha = 1/2$

x	$F_{1/2}(x)$	$H_{1/2}(x)$	$T_{1/2}(x)$
1.50	2.35241	2.12928	0.90515
1.51	2.37382	2.15291	0.90696
1.52	2.39567	2.17676	0.90870
1.53	2.41736	2.20082	0.91042
1.54	2.43949	2.22510	0.91212
1.55	2.46186	2.24961	0.91379
1.56	2.48448	2.27434	0.91542
1.57	2.50735	2.29930	0.91703
1.58	2.53047	2.32449	0.91860
1.59	2.55384	2.34991	0.92015
1.60	2.57746	2.37557	0.92167
1.61	2.60135	2.40146	0.92316
1.62	2.62549	2.42760	0.92462
1.63	2.64990	2.45397	0.92606
1.64	2.67457	2.48059	0.92747
1.65	2.69951	2.50746	0.92886
1.66	2.72472	2.53459	0.93022
1.67	2.75021	2.56196	0.93155
1.68	2.77596	2.58959	0.93286
1.69	2.80200	2.61748	0.93415
1.70	2.82832	2.64563	0.93541
1.71	2.85491	2.67405	0.93665
1.72	2.88180	2.70273	0.93786
1.73	2.90897	2.73168	0.93906
1.74	2.93643	2.76091	0.94023
1.75	2.96419	2.79041	0.94138
1.76	2.99224	2.82020	0.94250
1.77	3.02059	2.85026	0.94361
1.78	3.04925	2.88061	0.94470
1.79	3.07821	2.91125	0.94576
1.80	3.10747	2.94217	0.94681
1.81	3.13705	2.97340	0.94783
1.82	3.16694	3.00492	0.94884
1.83	3.19715	3.03674	0.94983
1.84	3.22768	3.06886	0.95080
1.85	3.25853	3.10129	0.95175
1.86	3.28970	3.13403	0.95268
1.87	3.32121	3.16709	0.95359
1.88	3.35305	3.20046	0.95449
1.89	3.38522	3.23415	0.95537
1.90	3.41773	3.26816	0.95624
1.91	3.45058	3.30250	0.95709
1.92	3.48378	3.33718	0.95792
1.93	3.51733	3.37218	0.95873
1.94	3.55123	3.40752	0.95953
1.95	3.58548	3.44321	0.96032
1.96	3.62009	3.47923	0.96109
1.97	3.65507	3.51561	0.96185
1.98	3.69041	3.55234	0.96259
1.99	3.72611	3.58942	0.96331
2.00	3.76220	3.62686	0.96403

x	$F_{1/2}(x)$	$H_{1/2}(x)$	$T_{1/2}(x)$
2.0	3.76220	3.62686	0.96403
2.1	4.14431	4.02186	0.97045
2.2	4.56791	4.45711	0.97574
2.3	5.03722	4.93696	0.98010
2.4	5.55695	5.46623	0.98367
2.5	6.13229	6.05020	0.98661
2.6	6.76901	6.69473	0.98903
2.7	7.47347	7.40626	0.99101
2.8	8.25273	8.19192	0.99263
2.9	9.11458	9.05956	0.99396
3.0	10.06766	10.01787	0.99505
3.1	11.12150	11.07645	0.99595
3.2	12.28665	12.24588	0.99668
3.3	13.57476	13.53788	0.99728
3.4	14.99874	14.96536	0.99777
3.5	16.57282	16.54263	0.99818
3.6	18.31278	18.28546	0.99851
3.7	20.23601	20.21129	C.99878
3.8	22.36178	22.33941	0.99900
3.9	24.71135	24.69110	0.99918
4.0	27.30823	27.28992	0.99933
4.1	30.17843	30.16186	0.99945
4.2	33.35066	33.33567	0.99955
4.3	36.85668	36.84311	0.99963
4.4	40.73157	40.71930	0.99970
4.5	45.01412	45.00301	0.99975
4.6	49.74718	49.73713	0.99980
4.7	54.97813	54.96904	0.99983
4.8	60.75932	60.75109	0.99986
4.9	67.14861	67.14117	0.99989
5.0	74.20995	74.20321	0.99991
5.1	82.01400	82.00791	0.99993
5.2	90.63888	90.63336	0.99994
5.3	100.17090	100.16591	0.99995
5.4	110.70547	110.70095	0.99996
5.5	122.34801	122.34392	0.99997
5.6	135.21505	135.21135	C.99997
5.7	149.43537	149.43203	0.99998
5.8	165.15129	165.14827	0.99998
5.9	182.52010	182.51736	C.99998
6.0	201.71564	201.71316	0.99999

x	$F_{1/2}(x)$	$H_{1/2}(x)$	$T_{1/2}(x)$
6.0	201.71564	201.71316	0.99999
6.1	222.93001	222.92776	0.99999
6.2	246.37554	246.37351	0.99999
6.3	272.28687	272.28504	0.99999
6.4	300.92335	300.92169	0.99999
6.5	332.57157	332.57006	1.00000
6.6	367.54827	367.54691	1.00000
6.7	406.20353	406.20230	1.00000
6.8	448.92420	448.92309	1.00000
6.9	496.13786	496.13685	1.00000
7.0	548.31704	548.31612	1.00000
7.1	605.98395	605.98312	1.00000
7.2	669.71576	669.71501	1.00000
7.3	740.15030	740.14963	1.00000
7.4	817.99252	817.99191	1.00000
7.5	904.02148	904.02093	1.00000
7.6	999.09820	999.09770	1.00000
7.7	1104.17422	1104.17377	1.00000
7.8	1220.30119	1220.30078	1.00000
7.9	1348.64135	1348.64098	1.00000
8.0	1490.47916	1490.47883	1.00000
8.1	1647.23419	1647.23389	1.00000
8.2	1820.47529	1820.47502	1.00000
8.3	2011.93632	2011.93607	1.00000
8.4	2223.53349	2223.53326	1.00000
8.5	2457.38452	2457.38432	1.00000
8.6	2715.82989	2715.82970	1.00000
8.7	3001.45619	3001.45603	1.00000
8.8	3317.12208	3317.12193	1.00000
8.9	3665.98684	3665.98670	1.00000
9.0	4051.54203	4051.54190	1.00000
9.1	4477.64641	4477.64630	1.00000
9.2	4948.56458	4948.56448	1.00000
9.3	5469.00965	5469.00956	1.00000
9.4	6044.19041	6044.19032	1.00000
9.5	6679.86345	6679.86338	1.00000
9.6	7382.39082	7382.39075	1.00000
9.7	8158.80363	8158.80357	1.00000
9.8	9016.87249	9016.87244	1.00000
9.9	9965.18524	9965.18519	1.00000
10.0	11013.23292	11013.23287	1.00000

TABLE 1B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 1/2$ and x from 1.50 to 10.0.

$\alpha = 1/3$

x	$F_{1/3}(x)$	$H_{2/3}(x)$	$T_{1/3}(x)$
0.0	1.00000	0.0	0.0
0.01	1.00008	0.00128	0.00128
0.02	1.00030	0.00323	0.00323
0.03	1.00068	0.00555	0.00555
0.04	1.00120	0.00815	0.00814
0.05	1.00188	0.01097	0.01095
0.06	1.00270	0.01399	0.01395
0.07	1.00368	0.01719	0.01712
0.08	1.00480	0.02054	0.02044
C.09	1.00608	0.02404	0.02389
0.10	1.00751	0.02767	0.02747
0.11	1.00909	0.03143	0.03115
0.12	1.01081	0.03531	0.03493
0.13	1.01270	0.03930	0.03881
0.14	1.01473	0.04340	0.04277
0.15	1.01691	0.04760	0.04681
0.16	1.01925	0.05191	0.05093
0.17	1.02173	0.05630	0.05511
C.18	1.02437	0.06079	0.05935
0.19	1.02717	0.06537	0.06365
0.20	1.03011	0.07004	0.06799
0.21	1.03321	0.07480	0.07239
0.22	1.03646	0.07963	0.07683
0.23	1.03987	0.08455	0.08131
0.24	1.04343	0.08955	0.08583
0.25	1.04715	0.09463	0.09037
0.26	1.05102	0.09979	0.09494
0.27	1.05505	0.10502	0.09954
0.28	1.05923	0.11033	0.10416
0.29	1.06357	0.11571	0.10880
0.30	1.06807	0.12117	0.11345
0.31	1.07273	0.12670	0.11811
0.32	1.07754	0.13230	0.12278
C.33	1.08251	0.13798	0.12746
0.34	1.08764	0.14372	0.13214
C.35	1.09293	0.14954	0.13683
C.36	1.09839	0.15543	0.14151
0.37	1.10400	0.16139	0.14618
C.38	1.10977	0.16742	0.15086
0.39	1.11571	0.17352	0.15552
C.40	1.12181	0.17968	0.16017
0.41	1.12807	0.18592	0.16481
0.42	1.13450	0.19223	0.16944
0.43	1.14109	0.19861	0.17405
0.44	1.14785	0.20505	0.17864
C.45	1.15478	0.21157	0.18321
0.46	1.16187	0.21815	0.18776
C.47	1.16913	0.22481	0.19229
0.48	1.17656	0.23154	0.19679
0.49	1.18416	0.23833	0.20127
0.50	1.19193	0.24520	0.20571

x	$F_{1/3}(x)$	$H_{2/3}(x)$	$T_{1/3}(x)$
C.50	1.19193	0.24520	0.20571
0.51	1.19988	0.25214	0.21013
0.52	1.20799	0.25914	0.21452
0.53	1.21628	0.26622	0.21888
C.54	1.22474	0.27337	0.22321
0.55	1.23338	0.28059	0.22750
0.56	1.24219	0.28789	0.23176
0.57	1.25118	0.29525	0.23598
0.58	1.26035	0.30269	0.24016
0.59	1.26970	0.31020	0.24431
0.60	1.27923	0.31779	0.24842
0.61	1.28894	0.32545	0.25249
C.62	1.29883	0.33318	0.25652
0.63	1.30891	0.34099	0.26052
0.64	1.31917	0.34888	0.26447
0.65	1.32962	0.35684	0.26838
0.66	1.34025	0.36488	0.27225
0.67	1.35107	0.37299	0.27607
0.68	1.36208	0.38119	0.27985
C.69	1.37329	0.38946	0.28360
0.70	1.38468	0.39781	0.28729
C.71	1.39627	0.40624	0.29095
0.72	1.40805	0.41475	0.29456
C.73	1.42003	0.42334	0.29812
0.74	1.43220	0.43202	0.30164
0.75	1.44457	0.44077	0.30512
0.76	1.45715	0.44961	C.30856
C.77	1.46992	0.45853	0.31195
0.78	1.48290	0.46754	0.31529
0.79	1.49608	0.47664	0.31859
C.80	1.50947	0.48582	0.32185
C.81	1.52306	0.49508	0.32506
0.82	1.53686	0.50444	0.32822
0.83	1.55088	0.51388	0.33135
0.84	1.56510	0.52341	0.33443
0.85	1.57954	0.53304	0.33746
0.86	1.59419	0.54275	0.34045
0.87	1.60906	0.55256	0.34340
0.88	1.62415	0.56246	0.34631
0.89	1.63946	0.57245	0.34917
0.90	1.65499	0.58254	0.35199
C.91	1.67074	0.59272	0.35477
0.92	1.68672	0.60300	0.35750
0.93	1.70292	0.61338	0.36019
C.94	1.71936	0.62386	0.36284
0.95	1.73602	0.63443	0.36545
C.96	1.75292	0.64511	0.36802
0.97	1.77005	0.65589	0.37055
C.98	1.78742	0.66677	0.37304
C.99	1.80503	0.67776	0.37548
1.00	1.82287	0.68885	0.37789

x	$F_{1/3}(x)$	$H_{2/3}(x)$	$T_{1/3}(x)$
1.00	1.82287	0.68885	0.37789
1.01	1.84096	0.70005	0.38026
1.02	1.85929	0.71135	0.38259
1.03	1.87787	0.72276	0.38488
1.04	1.89670	0.73428	0.38714
1.05	1.91578	0.74592	0.38935
1.06	1.93511	0.75766	0.39153
1.07	1.95469	0.76952	0.39368
1.08	1.97453	0.78149	0.39578
1.09	1.99463	0.79357	0.39785
1.10	2.01500	0.80578	0.39989
1.11	2.03562	0.81810	0.40189
1.12	2.05651	0.83054	0.40386
1.13	2.07767	0.84310	0.40579
1.14	2.09910	0.85578	0.40769
1.15	2.12081	0.86858	0.40955
1.16	2.14279	0.88151	0.41138
1.17	2.16504	0.89456	0.41318
1.18	2.18758	0.90774	0.41495
1.19	2.21040	0.92105	0.41669
1.20	2.23350	0.93449	0.41840
1.21	2.25690	0.94806	0.42007
1.22	2.28058	0.96176	0.42172
1.23	2.30456	0.97560	0.42333
1.24	2.32883	0.98957	0.42492
1.25	2.35340	1.00367	0.42648
1.26	2.37827	1.01792	0.42801
1.27	2.40345	1.03230	0.42951
1.28	2.42893	1.04683	0.43098
1.29	2.45473	1.06150	0.43243
1.30	2.48083	1.07631	0.43385
1.31	2.50725	1.09127	0.43525
1.32	2.53399	1.10638	0.43661
1.33	2.56105	1.12163	0.43796
1.34	2.58844	1.13704	0.43928
1.35	2.61615	1.15260	0.44057
1.36	2.64419	1.16831	0.44184
1.37	2.67257	1.18418	0.44309
1.38	2.70128	1.20020	0.44431
1.39	2.73034	1.21639	0.44551
1.40	2.75973	1.23273	0.44668
1.41	2.78947	1.24924	0.44784
1.42	2.81957	1.26591	0.44897
1.43	2.85001	1.28274	0.45008
1.44	2.88081	1.29975	0.45117
1.45	2.91197	1.31692	0.45224
1.46	2.94350	1.33427	0.45329
1.47	2.97539	1.35179	0.45432
1.48	3.00765	1.36948	0.45533
1.49	3.04029	1.38735	0.45632
1.50	3.07330	1.40540	0.45729

TABLE 2A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 1/3$ and x from 0.00 to 1.50.

$\alpha = 1/3$

x	$F_{1/3}(x)$	$H_{2/3}(x)$	$T_{1/3}(x)$
1.50	3.07330	1.40540	0.45729
1.51	3.10669	1.42363	0.45825
1.52	3.14047	1.44204	0.45918
1.53	3.17464	1.46064	0.46010
1.54	3.20920	1.47943	0.46100
1.55	3.24416	1.49840	0.46188
1.56	3.27951	1.51757	0.46274
1.57	3.31527	1.53692	0.46359
1.58	3.35144	1.55648	0.46442
1.59	3.38802	1.57622	0.46524
1.60	3.42501	1.59617	0.46603
1.61	3.46243	1.61632	0.46682
1.62	3.50027	1.63668	0.46759
1.63	3.53854	1.65724	0.46834
1.64	3.57724	1.67800	0.46908
1.65	3.61637	1.69898	0.46980
1.66	3.65595	1.72017	0.47051
1.67	3.69598	1.74158	0.47121
1.68	3.73645	1.76320	0.47189
1.69	3.77738	1.78504	0.47256
1.70	3.81877	1.80710	0.47322
1.71	3.86062	1.82939	0.47386
1.72	3.90294	1.85191	0.47449
1.73	3.94573	1.87465	0.47511
1.74	3.98900	1.89762	0.47571
1.75	4.03275	1.92083	0.47631
1.76	4.07699	1.94428	0.47689
1.77	4.12172	1.96796	0.47746
1.78	4.16695	1.99189	0.47802
1.79	4.21267	2.01606	0.47857
1.80	4.25891	2.04048	0.47911
1.81	4.30566	2.06514	0.47963
1.82	4.35292	2.09006	0.48015
1.83	4.40071	2.11523	0.48066
1.84	4.44903	2.14067	0.48115
1.85	4.49787	2.16636	0.48164
1.86	4.54726	2.19231	0.48212
1.87	4.59719	2.21853	0.48258
1.88	4.64767	2.24502	0.48304
1.89	4.69870	2.27178	0.48349
1.90	4.75030	2.29882	0.48393
1.91	4.80246	2.32613	0.48436
1.92	4.85519	2.35373	0.48479
1.93	4.90850	2.38160	0.48520
1.94	4.96239	2.40977	0.48561
1.95	5.01688	2.43822	0.48600
1.96	5.07195	2.46697	0.48639
1.97	5.12763	2.49601	0.48678
1.98	5.18392	2.52535	0.48715
1.99	5.24082	2.55499	0.48752
2.00	5.29834	2.58494	0.48788

x	$F_{1/3}(x)$	$H_{2/3}(x)$	$T_{1/3}(x)$
2.0	5.29834	2.58494	0.48788
2.1	5.90906	2.90196	0.49110
2.2	6.58916	3.25333	0.49374
2.3	7.34609	3.64286	0.49589
2.4	8.18812	4.07480	0.49765
2.5	9.12445	4.55385	0.49908
2.6	10.16526	5.08521	0.50025
2.7	11.32190	5.67464	0.50121
2.8	12.60691	6.32854	0.50199
2.9	14.03424	7.05399	0.50263
3.0	15.61932	7.85882	0.50315
3.1	17.37931	8.75173	0.50357
3.2	19.33319	9.74236	0.50392
3.3	21.50203	10.84137	0.50420
3.4	23.90917	12.06058	0.50443
3.5	26.58048	13.41311	0.50462
3.6	29.54465	14.91345	0.50478
3.7	32.83344	16.57770	0.50490
3.8	36.48208	18.42367	0.50501
3.9	40.52959	20.47111	0.50509
4.0	45.01920	22.74186	0.50516
4.1	49.99881	25.26018	0.50522
4.2	55.52151	28.05289	0.50526
4.3	61.64609	31.14972	0.50530
4.4	68.43768	34.58361	0.50533
4.5	75.96846	38.39105	0.50536
4.6	84.31835	42.61245	0.50538
4.7	93.57590	47.29256	0.50539
4.8	103.83919	52.48098	0.50541
4.9	115.21685	58.23262	0.50542
5.0	127.82922	64.60830	0.50543
5.1	141.80955	71.67541	0.50543
5.2	157.30546	79.50854	0.50544
5.3	174.48042	88.19033	0.50545
5.4	193.51547	97.81231	0.50545
5.5	214.61111	108.47582	0.50545
5.6	237.98938	120.29309	0.50546
5.7	263.89617	133.38841	0.50546
5.8	292.60376	147.89943	0.50546
5.9	324.41368	163.97856	0.50546
6.0	359.65982	181.79456	0.50546

x	$F_{1/3}(x)$	$H_{2/3}(x)$	$T_{1/3}(x)$
6.0	359.65982	181.79456	0.50546
6.1	398.71187	201.53431	0.50546
6.2	441.97922	223.40475	0.50546
6.3	489.91515	247.63498	0.50547
6.4	543.02156	274.47872	0.50547
6.5	601.85414	304.21683	0.50547
6.6	667.02816	337.16033	0.50547
6.7	739.22482	373.65355	0.50547
6.8	819.19834	414.07770	0.50547
6.9	907.78370	458.85486	0.50547
7.0	1005.90533	508.45229	0.50547
7.1	1114.58667	563.38731	0.50547
7.2	1234.96073	624.23262	0.50547
7.3	1368.28181	691.62223	0.50547
7.4	1515.93846	766.25801	0.50547
7.5	1679.46784	848.91694	0.50547
7.6	1860.57158	940.45914	0.50547
7.7	2061.13333	1041.83675	0.50547
7.8	2283.23826	1154.10374	0.50547
7.9	2529.19452	1278.42680	0.50547
8.0	2801.55706	1416.09741	0.50547
8.1	3103.15401	1568.54507	0.50547
8.2	3437.11583	1737.35213	0.50547
8.3	3806.90755	1924.27007	0.50547
8.4	4216.36450	2131.23751	0.50547
8.5	4669.73184	2360.40025	0.50547
8.6	5171.70827	2614.13334	0.50547
8.7	5727.49440	2895.06550	0.50547
8.8	6342.84633	3206.10628	0.50547
8.9	7024.13486	3550.47590	0.50547
9.0	7778.41109	3931.73848	0.50547
9.1	8613.47893	4353.83863	0.50547
9.2	9537.97538	4821.14209	0.50547
9.3	10561.45936	5338.48059	0.50547
9.4	11694.51000	5911.20154	0.50547
9.5	12948.83537	6545.22299	0.50547
9.6	14337.39281	7247.09447	0.50547
9.7	15874.52207	8024.06427	0.50547
9.8	17576.09265	8884.15390	0.50547
9.9	19459.66675	9836.24050	0.50547
10.0	21544.67965	10890.14799	0.50547

TABLE 2B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 1/3$ and x from 1.50 to 10.0.

$\alpha = 2/3$

x	$F_{2/3}(x)$	$H_{1/3}(x)$	$T_{2/3}(x)$
0.0	1.00000	0.0	0.0
0.01	1.00004	0.08772	0.08772
0.02	1.00015	0.13926	0.13924
0.03	1.00034	0.18250	0.18244
0.04	1.00060	0.22111	0.22098
0.05	1.00094	0.25662	0.25638
0.06	1.00135	0.28984	0.28945
0.07	1.00184	0.32129	0.32070
0.08	1.00240	0.35130	0.35046
0.09	1.00304	0.38012	0.37897
0.10	1.00375	0.40793	0.40640
0.11	1.00454	0.43486	0.43289
0.12	1.00541	0.46103	0.45855
0.13	1.00635	0.48653	0.48346
0.14	1.00736	0.51142	0.50769
0.15	1.00845	0.53579	0.53130
0.16	1.00962	0.55967	0.55434
0.17	1.01086	0.58311	0.57685
0.18	1.01218	0.60616	0.59886
0.19	1.01357	0.62884	0.62042
0.20	1.01505	0.65119	0.64154
0.21	1.01659	0.67323	0.66225
0.22	1.01822	0.69500	0.68256
0.23	1.01992	0.71650	0.70251
0.24	1.02169	0.73777	0.72211
0.25	1.02355	0.75882	0.74136
0.26	1.02548	0.77966	0.76029
0.27	1.02749	0.80032	0.77891
0.28	1.02957	0.82080	0.79722
0.29	1.03174	0.84112	0.81525
0.30	1.03398	0.86129	0.83299
0.31	1.03630	0.88133	0.85046
0.32	1.03870	0.90124	0.86766
0.33	1.04117	0.92103	0.88461
0.34	1.04373	0.94071	0.90130
0.35	1.04636	0.96030	0.91775
0.36	1.04907	0.97979	0.93396
0.37	1.05187	0.99921	0.94994
0.38	1.05474	1.01855	0.96569
0.39	1.05769	1.03782	0.98121
0.40	1.06072	1.05703	0.99652
0.41	1.06384	1.07619	1.01161
0.42	1.06703	1.09530	1.02649
0.43	1.07030	1.11436	1.04116
0.44	1.07366	1.13339	1.05563
0.45	1.07710	1.15239	1.06990
0.46	1.08062	1.17137	1.08398
0.47	1.08422	1.19032	1.09786
0.48	1.08790	1.20926	1.11155
0.49	1.09167	1.22819	1.12505
0.50	1.09552	1.24711	1.13837

x	$F_{2/3}(x)$	$H_{1/3}(x)$	$T_{2/3}(x)$
0.50	1.09552	1.24711	1.13837
0.51	1.09946	1.26603	1.15151
0.52	1.10347	1.28495	1.16446
0.53	1.10758	1.30389	1.17724
0.54	1.11176	1.32283	1.18985
0.55	1.11604	1.34178	1.20228
0.56	1.12039	1.36076	1.21454
0.57	1.12484	1.37976	1.22663
0.58	1.12937	1.39879	1.23856
0.59	1.13398	1.41784	1.25032
0.60	1.13869	1.43694	1.26192
0.61	1.14348	1.45606	1.27337
0.62	1.14836	1.47523	1.28465
0.63	1.15332	1.49445	1.29578
0.64	1.15838	1.51371	1.30675
0.65	1.16352	1.53302	1.31757
0.66	1.16876	1.55239	1.32824
0.67	1.17409	1.57181	1.33875
0.68	1.17950	1.59130	1.34913
0.69	1.18501	1.61084	1.35935
0.70	1.19061	1.63046	1.36943
0.71	1.19630	1.65014	1.37937
0.72	1.20208	1.66990	1.38917
0.73	1.20796	1.68973	1.39883
0.74	1.21393	1.70964	1.40835
0.75	1.21999	1.72963	1.41774
0.76	1.22615	1.74970	1.42699
0.77	1.23241	1.76987	1.43610
0.78	1.23876	1.79012	1.44509
0.79	1.24521	1.81046	1.45394
0.80	1.25175	1.83090	1.46267
0.81	1.25840	1.85143	1.47127
0.82	1.26514	1.87207	1.47974
0.83	1.27198	1.89281	1.48809
0.84	1.27892	1.91365	1.49631
0.85	1.28595	1.93461	1.50441
0.86	1.29309	1.95567	1.51240
0.87	1.30034	1.97685	1.52026
0.88	1.30768	1.99815	1.52801
0.89	1.31513	2.01956	1.53564
0.90	1.32268	2.04110	1.54316
0.91	1.33033	2.06275	1.55056
0.92	1.33809	2.08454	1.55785
0.93	1.34595	2.10646	1.56503
0.94	1.35392	2.12850	1.57210
0.95	1.36200	2.15068	1.57906
0.96	1.37019	2.17300	1.58592
0.97	1.37848	2.19546	1.59267
0.98	1.38688	2.21806	1.59931
0.99	1.39540	2.24081	1.60586
1.00	1.40402	2.26370	1.61230

x	$F_{2/3}(x)$	$H_{1/3}(x)$	$T_{2/3}(x)$
1.00	1.40402	2.26370	1.61230
1.01	1.41275	2.28674	1.61864
1.02	1.42160	2.30994	1.62488
1.03	1.43056	2.33328	1.63103
1.04	1.43964	2.35679	1.63708
1.05	1.44882	2.38046	1.64303
1.06	1.45813	2.40429	1.64889
1.07	1.46755	2.42828	1.65465
1.08	1.47709	2.45245	1.66033
1.09	1.48674	2.47678	1.66591
1.10	1.49652	2.50129	1.67140
1.11	1.50641	2.52597	1.67681
1.12	1.51643	2.55083	1.68213
1.13	1.52656	2.57587	1.68736
1.14	1.53682	2.60109	1.69251
1.15	1.54721	2.62650	1.69758
1.16	1.55772	2.65210	1.70256
1.17	1.56835	2.67789	1.70746
1.18	1.57911	2.70388	1.71228
1.19	1.58999	2.73006	1.71702
1.20	1.60101	2.75644	1.72169
1.21	1.61215	2.78302	1.72627
1.22	1.62343	2.80981	1.73079
1.23	1.63484	2.83680	1.73522
1.24	1.64637	2.86401	1.73959
1.25	1.65805	2.89143	1.74388
1.26	1.66985	2.91906	1.74809
1.27	1.68179	2.94691	1.75224
1.28	1.69387	2.97499	1.75632
1.29	1.70609	3.00328	1.76033
1.30	1.71844	3.03181	1.76427
1.31	1.73094	3.06056	1.76815
1.32	1.74358	3.08955	1.77196
1.33	1.75635	3.11877	1.77571
1.34	1.76928	3.14823	1.77939
1.35	1.78234	3.17794	1.78301
1.36	1.79556	3.20788	1.78657
1.37	1.80892	3.23807	1.79006
1.38	1.82242	3.26852	1.79350
1.39	1.83608	3.29921	1.79688
1.40	1.84989	3.33017	1.80020
1.41	1.86385	3.36138	1.80346
1.42	1.87796	3.39285	1.80667
1.43	1.89223	3.42459	1.80982
1.44	1.90665	3.45660	1.81291
1.45	1.92123	3.48888	1.81596
1.46	1.93597	3.52143	1.81895
1.47	1.95087	3.55426	1.82188
1.48	1.96593	3.58737	1.82477
1.49	1.98115	3.62076	1.82761
1.50	1.99654	3.65444	1.83039

TABLE 3A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 2/3$ and x from 0.00 to 1.50.

$\alpha = 2/3$

x	$F_{2/3}(x)$	$H_{1/3}(x)$	$T_{2/3}(x)$
1.50	1.99654	3.65444	1.83039
1.51	2.01209	3.68842	1.83313
1.52	2.02781	3.72268	1.83582
1.53	2.04369	3.75724	1.83846
1.54	2.05975	3.79211	1.84105
1.55	2.07598	3.82727	1.84360
1.56	2.09237	3.86274	1.84610
1.57	2.10895	3.89853	1.84856
1.58	2.12570	3.93462	1.85098
1.59	2.14262	3.97103	1.85335
1.60	2.15973	4.00777	1.85568
1.61	2.17701	4.04483	1.85797
1.62	2.19448	4.08221	1.86022
1.63	2.21213	4.11993	1.86243
1.64	2.22996	4.15798	1.86459
1.65	2.24798	4.19636	1.86672
1.66	2.26619	4.23509	1.86881
1.67	2.28459	4.27417	1.87087
1.68	2.30318	4.31360	1.87288
1.69	2.32197	4.35337	1.87486
1.70	2.34095	4.39351	1.87681
1.71	2.360[illegible]2	4.43400	1.87672
1.72	2.37950	4.47486	1.88059
1.73	2.39907	4.51609	1.88243
1.74	2.41885	4.55768	1.88424
1.75	2.43883	4.59966	1.88601
1.76	2.45901	4.64201	1.88775
1.77	2.47940	4.68475	1.88946
1.78	2.50001	4.72787	1.89114
1.79	2.52082	4.77139	1.89279
1.80	2.54185	4.81530	1.89441
1.81	2.56309	4.85961	1.89600
1.82	2.58455	4.90433	1.89756
1.83	2.60623	4.94945	1.89909
1.84	2.62813	4.99499	1.90059
1.85	2.65025	5.04094	1.90207
1.86	2.67259	5.08732	1.90351
1.87	2.69517	5.13412	1.90493
1.88	2.71797	5.18135	1.90633
1.89	2.74100	5.22901	1.90770
1.90	2.76427	5.27711	1.90904
1.91	2.78777	5.32565	1.91036
1.92	2.81152	5.37465	1.91165
1.93	2.83550	5.42409	1.91293
1.94	2.85972	5.47399	1.91417
1.95	2.88418	5.52435	1.91540
1.96	2.90890	5.57518	1.91660
1.97	2.93386	5.62648	1.91778
1.98	2.95907	5.67825	1.91893
1.99	2.98453	5.73051	1.92007
2.00	3.01025	5.78325	1.92118

x	$F_{2/3}(x)$	$H_{1/3}(x)$	$T_{2/3}(x)$
2.0	3.01025	5.78325	1.92118
2.1	3.28205	6.33842	1.93124
2.2	3.58216	6.94779	1.93955
2.3	3.91334	7.61702	1.94643
2.4	4.27863	8.35230	1.95209
2.5	4.68142	9.16046	1.95677
2.6	5.12542	10.04900	1.96062
2.7	5.61474	11.02615	1.96379
2.8	6.15390	12.10099	1.96639
2.9	6.74791	13.28351	1.96854
3.0	7.40228	14.58471	1.97030
3.1	8.12310	16.01669	1.97175
3.2	8.91707	17.59281	1.97294
3.3	9.79160	19.32776	1.97391
3.4	10.75486	21.23775	1.97471
3.5	11.81582	23.34063	1.97537
3.6	12.98444	25.65607	1.97591
3.7	14.27164	28.20577	1.97635
3.8	15.68949	31.01364	1.97671
3.9	17.25130	34.10602	1.97701
4.0	18.97175	37.51199	1.97726
4.1	20.86700	41.26358	1.97746
4.2	22.95492	45.39611	1.97762
4.3	25.25517	49.94852	1.97775
4.4	27.78944	54.96375	1.97786
4.5	30.58167	60.48916	1.97795
4.6	33.65824	66.57697	1.97803
4.7	37.04825	73.28475	1.97809
4.8	40.78379	80.67601	1.97814
4.9	44.90025	88.82076	1.97818
5.0	49.43666	97.79625	1.97821
5.1	54.43607	107.68763	1.97824
5.2	59.94596	118.58886	1.97826
5.3	66.01869	130.60352	1.97828
5.4	72.71202	143.84591	1.97830
5.5	80.08966	158.44205	1.97831
5.6	88.22187	174.53096	1.97832
5.7	97.18616	192.26599	1.97833
5.8	107.06803	211.81628	1.97833
5.9	117.96178	233.36842	1.97834
6.0	129.97145	257.12820	1.97834

x	$F_{2/3}(x)$	$H_{1/3}(x)$	$T_{2/3}(x)$
6.0	129.97145	257.12820	1.97834
6.1	143.21179	283.32268	1.97835
6.2	157.80940	312.20230	1.97835
6.3	173.90393	344.04335	1.97835
6.4	191.64943	379.15061	1.97836
6.5	211.21588	417.86035	1.97836
6.6	232.79078	460.54351	1.97836
6.7	256.58098	507.60934	1.97836
6.8	282.81472	559.50936	1.97836
6.9	311.74379	616.74170	1.97836
7.0	343.64598	679.85596	1.97836
7.1	378.82779	749.45850	1.97836
7.2	417.62741	826.21836	1.97836
7.3	460.41794	910.87370	1.97836
7.4	507.61109	1004.23900	1.97836
7.5	559.66109	1107.21292	1.97836
7.6	617.06916	1220.78706	1.97836
7.7	680.38836	1346.05555	1.97836
7.8	750.22894	1484.22569	1.97836
7.9	827.26427	1636.62967	1.97836
8.0	912.23739	1804.73751	1.97836
8.1	1005.96825	1990.17133	1.97836
8.2	1109.36164	2194.72114	1.97836
8.3	1223.41598	2420.36220	1.97836
8.4	1349.23309	2669.27429	1.97836
8.5	1488.02882	2943.86283	1.97836
8.6	1641.14495	3246.78232	1.97836
8.7	1810.06220	3580.96219	1.97836
8.8	1996.41466	3949.63526	1.97836
8.9	2202.00570	4356.36923	1.97836
9.0	2428.82550	4805.10143	1.97836
9.1	2679.07046	5300.17714	1.97836
9.2	2955.16461	5846.39194	1.97836
9.3	3259.78315	6449.03839	1.97836
9.4	3595.87862	7113.95767	1.97836
9.5	3966.70960	7847.59643	1.97836
9.6	4375.87251	8657.06970	1.97836
9.7	4827.33666	9550.23026	1.97836
9.8	5325.48299	10535.74517	1.97836
9.9	5875.14679	11623.18037	1.97836
10.0	6481.66483	12823.09399	1.97836

TABLE 3B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 2/3$ and x from 1.50 to 10.0.

$\alpha = 1/4$

x	$F_{1/4}(x)$	$H_{3/4}(x)$	$T_{1/4}(x)$	x	$F_{1/4}(x)$	$H_{3/4}(x)$	$T_{1/4}(x)$	x	$F_{1/4}(x)$	$H_{3/4}(x)$	$T_{1/4}(x)$
0.0	1.00000	0.0	0.0	0.50	1.25631	0.17269	0.13746	1.00	2.10378	0.54188	0.25757
0.01	1.00010	0.00047	0.00047	0.51	1.26693	0.17815	0.14061	1.01	2.12817	0.55153	0.25916
0.02	1.00040	0.00133	0.00133	0.52	1.27779	0.18368	0.14375	1.02	2.15290	0.56129	0.26071
0.03	1.00090	0.00245	0.00245	0.53	1.28887	0.18928	0.14686	1.03	2.17796	0.57115	0.26224
C.04	1.00160	0.00377	0.00377	0.54	1.30020	0.19496	0.14995	1.04	2.20337	0.58111	0.26374
0.05	1.00250	0.00527	0.00526	0.55	1.31175	0.20071	0.15301	1.05	2.22912	0.59118	0.26521
0.06	1.00360	0.00693	0.00691	0.56	1.32355	0.20653	0.15604	1.06	2.25522	0.60136	0.26665
0.07	1.00490	0.00874	0.00869	C.57	1.33558	0.21242	0.15905	1.07	2.28166	0.61165	0.26807
0.08	1.00640	0.01068	0.01061	0.58	1.34786	0.21839	0.16203	1.08	2.30846	0.62205	0.26946
0.09	1.00811	0.01274	0.01264	0.59	1.36037	0.22443	0.16498	1.09	2.33561	0.63256	0.27083
0.10	1.01001	0.01493	0.01473	0.60	1.37313	0.23054	0.16789	1.10	2.36313	0.64318	0.27217
0.11	1.01211	0.01723	0.01702	0.61	1.38614	0.23673	0.17078	1.11	2.39100	0.65391	0.27349
0.12	1.01442	0.01964	0.01936	0.62	1.39939	0.24299	0.17364	1.12	2.41924	0.66475	0.27478
C.13	1.01693	0.02215	0.02178	0.63	1.41289	0.24933	0.17647	1.13	2.44785	0.67572	0.27604
0.14	1.01964	0.02476	0.02429	C.64	1.42663	0.25575	0.17927	1.14	2.47683	0.68679	0.27729
0.15	1.02255	0.02747	0.02687	0.65	1.44063	0.26224	0.18203	1.15	2.50619	0.69799	0.27851
C.16	1.02567	0.03028	0.02952	0.66	1.45488	0.26880	0.18476	1.16	2.53592	0.70930	0.27970
0.17	1.02898	0.03318	0.03224	0.67	1.46939	0.27545	0.18746	1.17	2.56604	0.72074	0.28087
C.18	1.03251	0.03617	0.03503	0.68	1.48415	0.28217	0.19012	1.18	2.59655	0.73229	0.28202
0.19	1.03623	0.03924	0.03787	0.69	1.49917	0.28897	0.19275	1.19	2.62744	0.74397	0.28315
0.20	1.04016	0.04241	0.04077	C.70	1.51445	0.29584	0.19535	1.20	2.65873	0.75577	0.28426
0.21	1.04429	0.04565	0.04372	0.71	1.52999	0.30280	0.19791	1.21	2.69042	0.76770	0.28534
0.22	1.04863	0.04898	0.04671	G.72	1.54580	0.30984	0.20044	1.22	2.72250	0.77975	0.28641
0.23	1.05318	0.05239	0.04975	0.73	1.56186	0.31695	0.20293	1.23	2.75499	0.79193	0.28745
0.24	1.05793	0.05588	0.05282	C.74	1.57820	0.32415	0.20539	1.24	2.78789	0.80424	0.28848
0.25	1.06289	0.05945	0.05594	0.75	1.59481	0.33143	0.20782	1.25	2.82120	0.81668	0.28948
0.26	1.06806	0.06310	0.05908	0.76	1.61168	0.33879	0.21021	1.26	2.85493	0.82925	0.29046
C.27	1.07343	0.06683	0.06226	0.77	1.62883	0.34623	0.21256	1.27	2.88908	0.84195	0.29143
C.28	1.07902	C.07063	0.06546	0.78	1.64626	0.35376	0.21488	1.28	2.92365	0.85479	0.29237
0.29	1.08481	0.07451	0.06868	C.79	1.66396	0.36137	0.21717	1.29	2.95865	0.86777	0.29330
C.30	1.09081	0.07846	0.07193	0.80	1.68194	0.36906	0.21942	1.30	2.99408	0.88088	0.29421
0.31	1.09703	0.08249	0.07519	0.81	1.70021	0.37684	0.22164	1.31	3.02995	0.89413	0.29510
C.32	1.10345	0.08659	0.07847	0.82	1.71875	0.38470	0.22383	1.32	3.06626	0.90752	0.29597
0.33	1.11009	0.09076	0.08176	0.83	1.73759	0.39266	0.22598	1.33	3.10301	0.92105	0.29683
0.34	1.11694	0.09501	0.08506	0.84	1.75671	0.40070	0.22809	1.34	3.14022	0.93473	0.29766
C.35	1.12401	0.09933	0.08837	0.85	1.77612	0.40882	0.23018	1.35	3.17787	0.94855	0.29849
C.36	1.13129	0.10372	0.09168	0.86	1.79582	0.41704	0.23223	1.36	3.21599	0.96252	0.29929
0.37	1.13878	0.10818	0.09500	C.87	1.81582	0.42535	0.23425	1.37	3.25457	0.97663	0.30008
0.38	1.14650	0.11272	0.09832	C.88	1.83612	0.43374	C.23623	1.38	3.29361	0.99090	0.30085
0.39	1.15443	0.11732	0.10163	0.89	1.85671	0.44223	0.23818	1.39	3.33313	1.00531	0.30161
0.40	1.16258	0.12200	0.10494	0.90	1.87761	0.45081	0.24010	1.40	3.37312	1.01988	0.30235
0.41	1.17094	0.12675	0.10825	0.91	1.89881	0.45949	0.24199	1.41	3.41360	1.03460	0.30308
0.42	1.17953	0.13157	0.11155	0.92	1.92032	0.46825	0.24384	1.42	3.45456	1.04948	0.30380
C.43	1.18834	0.13646	0.11483	G.93	1.94214	0.47712	0.24566	1.43	3.49601	1.06452	0.30449
0.44	1.19738	0.14142	0.11811	0.94	1.96427	0.48607	0.24746	1.44	3.53795	1.07971	0.30518
0.45	1.20663	0.14646	0.12138	C.95	1.98672	0.49513	0.24922	1.45	3.58040	1.09507	0.30585
C.46	1.21611	0.15156	0.12463	0.96	2.00949	0.50428	0.25095	1.46	3.62335	1.11059	0.30651
0.47	1.22582	0.15674	0.12786	0.97	2.03257	0.51353	0.25265	1.47	3.66681	1.12627	0.30715
0.48	1.23575	0.16198	0.13108	C.98	2.05598	0.52288	0.25432	1.48	3.71079	1.14212	0.30778
0.49	1.24592	0.16730	0.13428	0.99	2.07971	0.53233	0.25596	1.49	3.75529	1.15814	0.30840
0.50	1.25631	0.17269	0.13746	1.00	2.10378	0.54188	0.25757	1.50	3.80031	1.17433	0.30901

TABLE 4A. Lanchester-Clifford-Schläfli Functions $F_{\alpha}(x)$, $H_{1-\alpha}(x)$, and $T_{\alpha}(x)$ for $\alpha = 1/4$ and x from 0.00 to 1.50.

$\alpha = 1/4$

x	$F_{1/4}(x)$	$H_{3/4}(x)$	$T_{1/4}(x)$
1.50	3.80031	1.17433	0.30901
1.51	3.84587	1.19069	0.30960
1.52	3.89196	1.20722	0.31018
1.53	3.93859	1.22393	0.31075
1.54	3.98577	1.24081	0.31131
1.55	4.03350	1.25788	0.31186
1.56	4.08179	1.27512	0.31239
1.57	4.13065	1.29255	0.31292
1.58	4.18007	1.31017	0.31343
1.59	4.23007	1.32797	0.31394
1.60	4.28065	1.34596	0.31443
1.61	4.33182	1.36414	0.31491
1.62	4.38358	1.38251	0.31538
1.63	4.43594	1.40108	0.31585
1.64	4.48890	1.41985	0.31630
1.65	4.54248	1.43882	0.31675
1.66	4.59667	1.45798	0.31718
1.67	4.65149	1.47736	0.31761
1.68	4.70694	1.49694	0.31803
1.69	4.76302	1.51672	0.31844
1.70	4.81975	1.53672	0.31884
1.71	4.87713	1.55693	0.31923
1.72	4.93516	1.57735	0.31962
1.73	4.99386	1.59800	0.31999
1.74	5.05322	1.61886	0.32036
1.75	5.11327	1.63994	0.32072
1.76	5.17400	1.66125	0.32108
1.77	5.23541	1.68279	0.32142
1.78	5.29753	1.70455	0.32176
1.79	5.36035	1.72655	0.32210
1.80	5.42389	1.74878	0.32242
1.81	5.48814	1.77125	0.32274
1.82	5.55312	1.79396	0.32305
1.83	5.61884	1.81691	0.32336
1.84	5.68530	1.84010	0.32366
1.85	5.75251	1.86354	0.32395
1.86	5.82047	1.88724	0.32424
1.87	5.88921	1.91118	0.32452
1.88	5.95871	1.93538	0.32480
1.89	6.02900	1.95984	0.32507
1.90	6.10008	1.98456	0.32533
1.91	6.17196	2.00954	0.32559
1.92	6.24464	2.03479	0.32585
1.93	6.31814	2.06031	0.32610
1.94	6.39246	2.08611	0.32634
1.95	6.46761	2.11217	0.32658
1.96	6.54360	2.13852	0.32681
1.97	6.62044	2.16515	0.32704
1.98	6.69814	2.19206	0.32726
1.99	6.77671	2.21926	0.32748
2.00	6.85616	2.24675	0.32770

x	$F_{1/4}(x)$	$H_{3/4}(x)$	$T_{1/4}(x)$
2.0	6.85616	2.24675	0.32770
2.1	7.70085	2.53835	0.32962
2.2	8.64388	2.86267	0.33118
2.3	9.69609	3.22343	0.33245
2.4	10.86951	3.62473	0.33348
2.5	12.17756	4.07113	0.33431
2.6	13.63512	4.56771	0.33500
2.7	15.25875	5.12007	0.33555
2.8	17.06686	5.73448	0.33600
2.9	19.07988	6.41786	0.33637
3.0	21.32051	7.17792	0.33667
3.1	23.81395	8.02318	0.33691
3.2	26.58819	8.96313	0.33711
3.3	29.67429	10.00828	0.33727
3.4	33.10675	11.17032	0.33740
3.5	36.92382	12.46219	0.33751
3.6	41.16800	13.89826	0.33760
3.7	45.88641	15.49447	0.33767
3.8	51.13136	17.26852	0.33773
3.9	56.96088	19.24004	0.33778
4.0	63.43934	21.43078	0.33782
4.1	70.63817	23.86490	0.33785
4.2	78.63660	26.56919	0.33787
4.3	87.52252	29.57336	0.33789
4.4	97.39340	32.91036	0.33791
4.5	108.35735	36.61674	0.33793
4.6	120.53430	40.73304	0.33794
4.7	134.05721	45.30420	0.33795
4.8	149.07356	50.38008	0.33795
4.9	165.74688	56.01595	0.33796
5.0	184.25850	62.27311	0.33797
5.1	204.80949	69.21950	0.33797
5.2	227.62277	76.93050	0.33797
5.3	252.94553	85.48964	0.33798
5.4	281.05178	94.98954	0.33798
5.5	312.24535	105.53289	0.33798
5.6	346.86301	117.23353	0.33798
5.7	385.27813	130.21764	0.33798
5.8	427.90458	144.62511	0.33798
5.9	475.20112	160.61101	0.33799
6.0	527.67626	178.34720	0.33799

x	$F_{1/4}(x)$	$H_{3/4}(x)$	$T_{1/4}(x)$
6.0	527.67626	178.34720	0.33799
6.1	585.89365	198.02419	0.33799
6.2	650.47799	219.85313	0.33799
6.3	722.12168	244.06805	0.33799
6.4	801.59208	270.92829	0.33799
6.5	889.73967	300.72132	0.33799
6.6	987.50692	333.76568	0.33799
6.7	1095.93831	370.41439	0.33799
6.8	1216.19128	411.05867	0.33799
6.9	1349.54844	456.13200	0.33799
7.0	1497.43105	506.11478	0.33799
7.1	1661.41396	561.53928	0.33799
7.2	1843.24219	622.99529	0.33799
7.3	2044.84923	691.13633	0.33799
7.4	2268.37739	766.68645	0.33799
7.5	2516.20022	850.44792	0.33799
7.6	2790.94750	943.30954	0.33799
7.7	3095.53275	1046.25608	0.33799
7.8	3433.18381	1160.37849	0.33799
7.9	3807.47665	1286.88542	0.33799
8.0	4222.37283	1427.11584	0.33799
8.1	4682.26100	1582.55306	0.33799
8.2	5192.00279	1754.84026	0.33799
8.3	5756.98374	1945.79769	0.33799
8.4	6383.16955	2157.44170	0.33799
8.5	7077.16850	2392.00581	0.33799
8.6	7846.30050	2651.96407	0.33799
8.7	8698.67355	2940.05690	0.33799
8.8	9643.26842	3259.31970	0.33799
8.9	10690.03241	3613.11455	0.33799
9.0	11849.98315	4005.16529	0.33799
9.1	13135.32354	4439.59636	0.33799
9.2	14559.56902	4920.97585	0.33799
9.3	16137.68846	5454.36306	0.33799
9.4	17886.26020	6045.36129	0.33799
9.5	19823.64472	6700.17618	0.33799
9.6	21970.17593	7425.68038	0.33799
9.7	24348.37283	8229.48506	0.33799
9.8	26983.17397	9120.01918	0.33799
9.9	29902.19693	10106.61719	0.33799
10.0	33136.02562	11199.61611	0.33799

TABLE 4B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 1/4$ and x from 1.50 to 10.0.

$\alpha = 3/4$

x	$F_{3/4}(x)$	$H_{1/4}(x)$	$T_{3/4}(x)$
C.0	1.00000	0.0	0.0
0.01	1.00003	0.28285	0.28284
C.02	1.00013	0.40003	0.39998
0.03	1.00030	0.48999	0.48984
0.04	1.00053	0.56587	0.56556
C.05	1.00083	0.63277	0.63224
C.06	1.00120	0.69332	0.69249
0.C7	1.00163	0.74907	0.74784
0.08	1.00213	0.80102	0.79932
0.09	1.00270	0.84990	0.84761
0.10	1.00334	0.89622	0.89324
0.11	1.00404	0.94035	0.93657
0.12	1.00480	0.98262	0.97792
0.13	1.00564	1.02325	1.01752
0.14	1.00654	1.06245	1.05555
0.15	1.00751	1.10038	1.09218
0.16	1.00855	1.13717	1.12753
0.17	1.00965	1.17294	1.16173
0.18	1.01083	1.20779	1.19486
0.19	1.01206	1.24180	1.22700
0.20	1.01337	1.27505	1.25823
0.21	1.01475	1.30761	1.28861
0.22	1.01619	1.33953	1.31819
0.23	1.01770	1.37086	1.34702
0.24	1.01928	1.40165	1.37514
0.25	1.02093	1.43195	1.40260
0.26	1.02264	1.46179	1.42943
C.27	1.02443	1.49121	1.45565
0.28	1.02628	1.52023	1.48130
0.29	1.02820	1.54889	1.50641
0.30	1.03019	1.57722	1.53099
0.31	1.03225	1.60523	1.55507
0.32	1.03438	1.63295	1.57867
0.33	1.03658	1.66041	1.60181
0.34	1.03885	1.68762	1.62450
0.35	1.04119	1.71460	1.64676
0.36	1.04360	1.74136	1.66861
0.37	1.04608	1.76793	1.69005
0.38	1.04863	1.79432	1.71110
0.39	1.05125	1.82054	1.73178
0.40	1.05395	1.84661	1.75209
0.41	1.05671	1.87254	1.77204
0.42	1.05954	1.89834	1.79165
0.43	1.06245	1.92402	1.81092
C.44	1.06543	1.94960	1.82987
0.45	1.06848	1.97508	1.84849
C.46	1.07161	2.00048	1.86680
0.47	1.07480	2.02580	1.88481
0.48	1.07807	2.05105	1.90252
0.49	1.08142	2.07625	1.91994
C.50	1.08483	2.10140	1.93707

x	$F_{3/4}(x)$	$H_{1/4}(x)$	$T_{3/4}(x)$
0.50	1.08483	2.10140	1.93707
0.51	1.08832	2.12650	1.95393
0.52	1.09189	2.15158	1.97051
0.53	1.09553	2.17663	1.98683
C.54	1.09924	2.20166	2.00288
0.55	1.10303	2.22667	2.01868
0.56	1.10690	2.25169	2.03423
0.57	1.11084	2.27670	2.04953
0.58	1.11486	2.30172	2.06459
C.59	1.11895	2.32676	2.07942
C.60	1.12312	2.35182	2.09401
0.61	1.12737	2.37690	2.10837
0.62	1.13169	2.40202	2.12250
0.63	1.13610	2.42717	2.13641
0.64	1.14058	2.45237	2.15011
0.65	1.14514	2.47761	2.16359
0.66	1.14978	2.50291	2.17686
C.67	1.15450	2.52827	2.18993
0.68	1.15930	2.55369	2.20279
C.69	1.16418	2.57917	2.21545
0.70	1.16914	2.60474	2.22792
0.71	1.17418	2.63037	2.24019
0.72	1.17930	2.65609	2.25226
0.73	1.18450	2.68190	2.26415
C.74	1.18979	2.70780	2.27586
C.75	1.19516	2.73379	2.28738
C.76	1.20062	2.75989	2.29872
C.77	1.20615	2.78609	2.30989
C.78	1.21178	2.81239	2.32088
0.79	1.21748	2.83881	2.33170
0.80	1.22328	2.86534	2.34235
0.81	1.22916	2.89200	2.35283
C.82	1.23512	2.91878	2.36315
0.83	1.24117	2.94568	2.37331
0.84	1.24731	2.97272	2.38331
0.85	1.25354	2.99990	2.39315
0.86	1.25985	3.02721	2.40283
C.87	1.26626	3.05467	2.41236
0.88	1.27275	3.08228	2.42174
C.89	1.27934	3.11003	2.43098
0.90	1.28601	3.13795	2.44006
0.91	1.29278	3.16601	2.44900
0.92	1.29963	3.19425	2.45780
0.93	1.30658	3.22264	2.46646
0.94	1.31363	3.25121	2.47499
0.95	1.32076	3.27995	2.48337
0.96	1.32800	3.30886	2.49162
C.97	1.33532	3.33796	2.49974
0.98	1.34274	3.36724	2.50773
0.99	1.35026	3.39670	2.51559
1.00	1.35788	3.42636	2.52332

x	$F_{3/4}(x)$	$H_{1/4}(x)$	$T_{3/4}(x)$
1.00	1.35788	3.42636	2.52332
1.01	1.36559	3.45621	2.53093
1.02	1.37340	3.48625	2.53841
1.03	1.38131	3.51650	2.54578
1.04	1.38932	3.54695	2.55302
1.05	1.39743	3.57761	2.56015
1.06	1.40564	3.60848	2.56716
1.07	1.41395	3.63957	2.57405
1.08	1.42236	3.67087	2.58083
1.09	1.43088	3.70240	2.58750
1.10	1.43950	3.73415	2.59407
1.11	1.44822	3.76613	2.60052
1.12	1.45705	3.79834	2.60687
1.13	1.46599	3.83079	2.61311
1.14	1.47503	3.86347	2.61925
1.15	1.48418	3.89640	2.62528
1.16	1.49344	3.92958	2.63122
1.17	1.50281	3.96300	2.63706
1.18	1.51229	3.99668	2.64280
1.19	1.52188	4.03061	2.64844
1.20	1.53158	4.06480	2.65400
1.21	1.54139	4.09926	2.65945
1.22	1.55132	4.13398	2.66482
1.23	1.56136	4.16897	2.67009
1.24	1.57152	4.20424	2.67528
1.25	1.58179	4.23979	2.68038
1.26	1.59218	4.27562	2.68539
1.27	1.60268	4.31173	2.69032
1.28	1.61331	4.34813	2.69516
1.29	1.62405	4.38482	2.69992
1.30	1.63492	4.42181	2.70460
1.31	1.64590	4.45909	2.70921
1.32	1.65701	4.49669	2.71373
1.33	1.66825	4.53458	2.71817
1.34	1.67960	4.57279	2.72254
1.35	1.69109	4.61131	2.72683
1.36	1.70270	4.65015	2.73105
1.37	1.71443	4.68931	2.73520
1.38	1.72630	4.72880	2.73927
1.39	1.73829	4.76861	2.74328
1.40	1.75041	4.80876	2.74721
1.41	1.76267	4.84925	2.75108
1.42	1.77506	4.89007	2.75488
1.43	1.78758	4.93125	2.75862
1.44	1.80024	4.97277	2.76228
1.45	1.81303	5.01464	2.76589
1.46	1.82596	5.05687	2.76943
1.47	1.83903	5.09945	2.77291
1.48	1.85223	5.14241	2.77633
1.49	1.86558	5.18573	2.77969
1.50	1.87907	5.22942	2.78299

TABLE 5A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/4$ and x from 0.00 to 1.50.

$\alpha = 3/4$

x	$F_{3/4}(x)$	$H_{1/4}(x)$	$T_{3/4}(x)$
1.50	1.87907	5.22942	2.78299
1.51	1.89270	5.27350	2.78623
1.52	1.90668	5.31795	2.78941
1.53	1.92040	5.36279	2.79254
1.54	1.93446	5.40801	2.79561
1.55	1.94868	5.45363	2.79863
1.56	1.96304	5.49965	2.80160
1.57	1.97755	5.54607	2.80451
1.58	1.99222	5.59289	2.80737
1.59	2.00704	5.64013	2.81018
1.60	2.02201	5.68778	2.81294
1.61	2.03713	5.73585	2.81565
1.62	2.05242	5.78434	2.81831
1.63	2.06786	5.83326	2.82092
1.64	2.08346	5.88261	2.82349
1.65	2.09922	5.93241	2.82601
1.66	2.11514	5.98264	2.82849
1.67	2.13122	6.03332	2.83092
1.68	2.14747	6.08445	2.83331
1.69	2.16389	6.13603	2.83565
1.70	2.18047	6.18808	2.83795
1.71	2.19723	6.24059	2.84021
1.72	2.21415	6.29357	2.84243
1.73	2.23124	6.34703	2.84461
1.74	2.24851	6.40096	2.84675
1.75	2.26596	6.45538	2.84885
1.76	2.28358	6.51029	2.85092
1.77	2.30138	6.56569	2.85294
1.78	2.31935	6.62159	2.85493
1.79	2.33751	6.67800	2.85688
1.80	2.35585	6.73492	2.85880
1.81	2.37438	6.79235	2.86068
1.82	2.39309	6.85030	2.86253
1.83	2.41199	6.90877	2.86434
1.84	2.43108	6.96778	2.86612
1.85	2.45036	7.02732	2.86787
1.86	2.46983	7.08741	2.86959
1.87	2.48950	7.14804	2.87127
1.88	2.50937	7.20922	2.87292
1.89	2.52943	7.27096	2.87455
1.90	2.54969	7.33326	2.87614
1.91	2.57015	7.39613	2.87770
1.92	2.59081	7.45957	2.87924
1.93	2.61168	7.52360	2.88075
1.94	2.63276	7.58821	2.88222
1.95	2.65405	7.65341	2.88368
1.96	2.67554	7.71921	2.88510
1.97	2.69725	7.78562	2.88650
1.98	2.71918	7.85263	2.88787
1.99	2.74132	7.92025	2.88922
2.00	2.76367	7.98850	2.89054

x	$F_{3/4}(x)$	$H_{1/4}(x)$	$T_{3/4}(x)$
2.0	2.76367	7.98850	2.89054
2.1	2.99970	8.70654	2.90247
2.2	3.25984	9.49380	2.91235
2.3	3.54639	10.35732	2.92052
2.4	3.86190	11.30482	2.92727
2.5	4.20915	12.34477	2.93284
2.6	4.59124	13.48645	2.93743
2.7	5.01157	14.74009	2.94121
2.8	5.47389	16.11690	2.94433
2.9	5.98232	17.62923	2.94689
3.0	6.54143	19.29064	2.94900
3.1	7.15622	21.11607	2.95073
3.2	7.83223	23.12194	2.95215
3.3	8.57555	25.32635	2.95332
3.4	9.39287	27.74918	2.95428
3.5	10.29158	30.41235	2.95507
3.6	11.27981	33.33997	2.95572
3.7	12.36654	36.55859	2.95625
3.8	13.56162	40.09746	2.95669
3.9	14.87592	43.98876	2.95705
4.0	16.32142	48.26796	2.95734
4.1	17.91130	52.97409	2.95758
4.2	19.66009	58.15016	2.95778
4.3	21.58379	63.84353	2.95794
4.4	23.70002	70.10637	2.95807
4.5	26.02821	76.99614	2.95818
4.6	28.58973	84.57615	2.95827
4.7	31.40816	92.91611	2.95834
4.8	34.50945	102.09286	2.95840
4.9	37.92220	112.19102	2.95845
5.0	41.67792	123.30382	2.95849
5.1	45.81133	135.53399	2.95853
5.2	50.36069	148.99473	2.95855
5.3	55.36813	163.81073	2.95857
5.4	60.88010	180.11942	2.95859
5.5	66.94778	198.07221	2.95861
5.6	73.62756	217.83597	2.95862
5.7	80.98160	239.59457	2.95863
5.8	89.07837	263.55064	2.95864
5.9	97.99335	289.92750	2.95864
6.0	107.80972	318.97126	2.95865

x	$F_{3/4}(x)$	$H_{1/4}(x)$	$T_{3/4}(x)$
6.0	107.80972	318.97126	2.95865
6.1	118.61917	350.95316	2.95865
6.2	130.52272	386.17215	2.95866
6.3	143.63175	424.95772	2.95866
6.4	158.06900	467.67305	2.95866
6.5	173.96977	514.71843	2.95867
6.6	191.48319	566.53511	2.95867
6.7	210.77365	623.60946	2.95867
6.8	232.02236	686.47762	2.95867
6.9	255.42908	755.73062	2.95867
7.0	281.21402	832.01997	2.95867
7.1	309.61993	916.06393	2.95867
7.2	340.91444	1008.65430	2.95867
7.3	375.39259	1110.66402	2.95867
7.4	413.37966	1223.05550	2.95867
7.5	455.23428	1346.88978	2.95867
7.6	501.35184	1483.33670	2.95867
7.7	552.16828	1633.68608	2.95867
7.8	608.16425	1799.36002	2.95867
7.9	669.86974	1981.92656	2.95867
8.0	737.86911	2183.11464	2.95867
8.1	812.80670	2404.83066	2.95867
8.2	895.39301	2649.17676	2.95867
8.3	986.41151	2918.47093	2.95867
8.4	1086.72611	3215.26927	2.95867
8.5	1197.28949	3542.39043	2.95867
8.6	1319.15223	3902.94271	2.95867
8.7	1453.47287	4300.35385	2.95868
8.8	1601.52902	4738.40392	2.95868
8.9	1764.72967	5221.26163	2.95868
9.0	1944.62868	5753.52437	2.95868
9.1	2142.93973	6340.26235	2.95868
9.2	2361.55278	6987.06735	2.95868
9.3	2602.55224	7700.10648	2.95868
9.4	2868.23703	8486.18146	2.95868
9.5	3161.14265	9352.79405	2.95868
9.6	3484.06564	10308.21826	2.95868
9.7	3840.09044	11361.57997	2.95868
9.8	4232.61910	12522.94477	2.95868
9.9	4665.40409	13803.41494	2.95868
10.0	5142.58436	15215.23636	2.95868

TABLE 5B. Lanchester-Clifford-Schläfli Functions $F_{\alpha}(x)$, $H_{1-\alpha}(x)$, and $T_{\alpha}(x)$ for $\alpha = 3/4$ and x from 1.50 to 10.0.

$\alpha = 1/5$

x	$F_{1/5}(x)$	$H_{4/5}(x)$	$T_{1/5}(x)$	x	$F_{1/5}(x)$	$H_{4/5}(x)$	$T_{1/5}(x)$	x	$F_{1/5}(x)$	$H_{4/5}(x)$	$T_{1/5}(x)$
0.0	1.00000	0.0	0.0	0.50	1.32072	0.14080	0.10661	1.00	2.38524	0.47223	0.19798
0.01	1.00013	0.00026	0.00026	0.51	1.33402	0.14553	0.10909	1.01	2.41596	0.48109	0.19913
C.02	1.00050	0.00079	0.00079	0.52	1.34762	0.15034	0.11156	1.02	2.44711	0.49005	0.20025
0.03	1.00113	0.00151	0.00151	0.53	1.36151	0.15521	0.11400	1.03	2.47869	0.49911	0.20136
0.04	1.00200	0.00239	0.00239	0.54	1.37569	0.16016	0.11642	1.04	2.51070	0.50827	0.20244
0.05	1.00313	0.00342	0.00341	0.55	1.39018	0.16518	0.11882	1.C5	2.54315	0.51753	0.20350
0.06	1.00450	0.00458	0.00456	0.56	1.40496	0.17027	0.12119	1.06	2.57604	0.52691	0.20454
C.C7	1.00613	0.00586	0.00582	0.57	1.42004	0.17543	0.12354	1.07	2.60937	0.53638	0.20556
0.08	1.00801	0.00725	0.00720	0.58	1.43542	0.18066	0.12586	1.08	2.64315	0.54597	0.20656
C.09	1.01013	0.00876	0.00867	0.59	1.45111	0.18597	0.12816	1.09	2.67739	0.55566	0.20754
0.10	1.01251	0.01037	0.01024	0.60	1.46711	0.19135	0.13043	1.10	2.71209	0.56547	0.20850
0.11	1.01514	0.01208	0.01190	0.61	1.48341	0.19680	0.13267	1.11	2.74724	0.57538	0.20944
0.12	1.01803	0.01389	0.01365	0.62	1.50002	0.20233	C.13488	1.12	2.78286	0.58540	0.21036
0.13	1.02116	0.01580	0.01547	0.63	1.51695	0.20793	0.13707	1.13	2.81895	0.59554	0.21126
C.14	1.02455	0.01779	0.01737	0.64	1.53419	0.21360	0.13923	1.14	2.85552	0.60579	0.21215
0.15	1.02819	0.01988	0.01933	C.65	1.55174	0.21935	0.14136	1.15	2.89257	0.61616	0.21301
0.16	1.03209	0.02205	0.02136	0.66	1.56962	0.22518	0.14346	1.16	2.93010	0.62664	0.21386
0.17	1.03623	0.02431	0.02346	0.67	1.58781	0.23108	0.14553	1.17	2.96812	0.63723	0.21469
0.18	1.04064	0.02665	0.02561	C.68	1.60633	0.23706	0.14758	1.18	3.00663	0.64795	0.21551
0.19	1.04529	0.02907	0.02781	0.69	1.62518	0.24311	0.14959	1.19	3.04564	0.65879	0.21631
0.20	1.05021	0.03157	0.03006	0.70	1.64435	0.24924	0.15158	1.20	3.08515	0.66975	0.21709
0.21	1.05538	0.03416	0.03236	0.71	1.66385	0.25545	0.15353	1.21	3.12517	0.68082	0.21785
0.22	1.06081	0.03682	0.03471	0.72	1.68369	0.26174	0.15546	1.22	3.16570	0.69203	0.21860
0.23	1.06649	0.03956	0.03709	0.73	1.70386	0.26811	0.15735	1.23	3.20675	0.70335	0.21934
0.24	1.07243	0.04237	0.03951	0.74	1.72436	0.27455	0.15922	1.24	3.24832	0.71481	0.22005
0.25	1.07863	0.04526	0.04196	0.75	1.74521	0.28108	0.16106	1.25	3.29042	0.72639	C.22076
0.26	1.08510	0.04823	0.04444	C.76	1.76640	0.28769	0.16287	1.26	3.33305	0.73810	0.22145
0.27	1.09182	0.05127	0.04696	C.77	1.78794	0.29437	0.16464	1.27	3.37621	0.74994	0.22212
0.28	1.09880	0.05438	0.04949	0.78	1.80982	0.30114	0.16639	1.28	3.41992	0.76191	0.22278
0.29	1.10605	0.05757	0.05205	0.79	1.83205	0.30800	0.16811	1.29	3.46418	0.77401	0.22343
0.30	1.11356	0.06082	0.05462	0.80	1.85464	0.31493	0.16981	1.30	3.50900	0.78624	0.22407
0.31	1.12133	0.06415	0.05721	0.81	1.87759	0.32195	0.17147	1.31	3.55437	0.79862	0.22469
0.32	1.12937	0.06756	0.05982	0.82	1.90089	0.32905	0.17311	1.32	3.60030	0.81113	0.22529
0.33	1.13768	0.07103	0.06243	0.83	1.92455	0.33624	0.17471	1.33	3.64681	0.82377	0.22589
C.34	1.14625	0.07457	0.06506	0.84	1.94858	0.34352	0.17629	1.34	3.69389	0.83656	0.22647
0.35	1.15509	0.07819	0.06769	0.85	1.97298	0.35088	0.17784	1.35	3.74156	0.84949	0.22704
0.36	1.16420	0.08187	0.07033	0.86	1.99775	0.35833	0.17937	1.36	3.78981	0.86256	0.22760
0.37	1.17358	0.08563	0.07296	0.87	2.02289	0.36587	0.18086	1.37	3.83865	0.87577	0.22815
0.38	1.18323	0.08945	0.07560	C.88	2.04841	0.37349	0.18233	1.38	3.88809	0.88913	0.22868
0.39	1.19315	0.09335	0.07824	C.89	2.07431	0.38121	0.18378	1.39	3.93814	0.90264	C.22921
0.40	1.20335	0.09731	0.08087	0.90	2.10059	0.38901	0.18519	1.40	3.98880	0.91630	0.22972
0.41	1.21383	0.10135	0.08349	C.91	2.12726	0.39691	0.18658	1.41	4.04008	0.93011	0.23022
0.42	1.22458	0.10545	0.08611	0.92	2.15432	0.40490	0.18795	1.42	4.09198	0.94407	0.23071
0.43	1.23561	0.10963	0.08872	0.93	2.18177	0.41298	0.18929	1.43	4.14451	0.95818	0.23119
0.44	1.24692	0.11387	0.09132	0.94	2.20962	0.42116	0.19060	1.44	4.19767	0.97245	0.23166
0.45	1.25851	0.11818	0.09391	0.55	2.23787	0.42943	0.19189	1.45	4.25148	0.98688	0.23212
0.46	1.27038	0.12257	0.09648	C.96	2.26652	0.43779	0.19316	1.46	4.30594	1.00146	0.23258
0.47	1.28253	0.12702	0.09904	0.97	2.29558	0.44626	0.19440	1.47	4.36105	1.01620	0.23302
0.48	1.29497	0.13154	0.10158	0.98	2.32505	0.45482	0.19562	1.48	4.41683	1.03111	0.23345
0.49	1.30770	0.13614	0.10410	0.99	2.35494	0.46347	0.19681	1.49	4.47327	1.04618	0.23387
C.50	1.32072	0.14080	0.10661	1.00	2.38524	0.47223	0.19798	1.50	4.53040	1.06142	0.23429

TABLE 6A. Lanchester-Clifford-Schläfli Functions $F_{\alpha}(x)$, $H_{1-\alpha}(x)$, and $T_{\alpha}(x)$ for $\alpha = 1/5$ and x from 0.00 to 1.50.

$\alpha = 1/5$

x	$F_{1/5}(x)$	$H_{4/5}(x)$	$T_{1/5}(x)$
1.50	4.53040	1.06142	0.23429
1.51	4.58820	1.07682	0.23469
1.52	4.64669	1.09240	0.23509
1.53	4.70588	1.10814	0.23548
1.54	4.76578	1.12406	0.23586
1.55	4.82639	1.14015	0.23623
1.56	4.88771	1.15642	0.23660
1.57	4.94976	1.17286	0.23695
1.58	5.01255	1.18949	0.23730
1.59	5.07607	1.20630	0.23764
1.60	5.14035	1.22330	0.23798
1.61	5.20538	1.24048	0.23831
1.62	5.27117	1.25785	0.23863
1.63	5.33774	1.27541	0.23894
1.64	5.40509	1.29316	0.23925
1.65	5.47322	1.31111	0.23955
1.66	5.54216	1.32925	0.23984
1.67	5.61189	1.34759	0.24013
1.68	5.68244	1.36614	0.24041
1.69	5.75382	1.38488	0.24069
1.70	5.82602	1.40383	0.24096
1.71	5.89906	1.42299	0.24122
1.72	5.97295	1.44236	0.24148
1.73	6.04770	1.46195	0.24174
1.74	6.12331	1.48174	0.24198
1.75	6.19979	1.50175	0.24223
1.76	6.27716	1.52199	0.24246
1.77	6.35542	1.54244	0.24270
1.78	6.43459	1.56312	0.24292
1.79	6.51467	1.58402	0.24315
1.80	6.59566	1.60516	0.24337
1.81	6.67759	1.62652	0.24358
1.82	6.76046	1.64812	0.24379
1.83	6.84428	1.66995	0.24399
1.84	6.92907	1.69203	0.24419
1.85	7.01482	1.71434	0.24439
1.86	7.10155	1.73690	0.24458
1.87	7.18928	1.75971	0.24477
1.88	7.27801	1.78276	0.24495
1.89	7.36775	1.80607	0.24513
1.90	7.45851	1.82963	0.24531
1.91	7.55031	1.85346	0.24548
1.92	7.64315	1.87754	0.24565
1.93	7.73705	1.90188	0.24581
1.94	7.83201	1.92649	0.24598
1.55	7.92806	1.95137	0.24614
1.96	8.02519	1.97653	0.24629
1.97	8.12343	2.00195	0.24644
1.98	8.22278	2.02766	0.24659
1.99	8.32325	2.05365	0.24674
2.00	8.42486	2.07992	0.24688

x	$F_{1/5}(x)$	$H_{4/5}(x)$	$T_{1/5}(x)$
2.0	8.42486	2.07992	0.24688
2.1	9.50623	2.35895	0.24815
2.2	10.71544	2.67002	0.24917
2.3	12.06679	3.01677	0.25001
2.4	13.57620	3.40328	0.25068
2.5	15.26139	3.83405	0.25123
2.6	17.14209	4.31413	0.25167
2.7	19.24023	4.84908	0.25203
2.8	21.58022	5.44513	0.25232
2.9	24.18919	6.10916	0.25256
3.0	27.09729	6.84885	0.25275
3.1	30.33805	7.67272	0.25291
3.2	33.94870	8.59022	0.25304
3.3	37.97065	9.61186	0.25314
3.4	42.44987	10.74932	0.25322
3.5	47.43742	12.01556	0.25329
3.6	52.99005	13.42498	0.25335
3.7	59.17075	14.99356	0.25339
3.8	66.04948	16.73907	0.25343
3.9	73.70395	18.68120	0.25346
4.0	82.22040	20.84185	0.25349
4.1	91.69462	23.24531	0.25351
4.2	102.23292	25.91854	0.25352
4.3	113.95332	28.89149	0.25354
4.4	126.98683	32.19738	0.25355
4.5	141.47886	35.87310	0.25356
4.6	157.59081	39.95957	0.25357
4.7	175.50179	44.50223	0.25357
4.8	195.41055	49.55148	0.25358
4.9	217.53767	55.16326	0.25358
5.0	242.12789	61.39965	0.25358
5.1	269.45279	68.32952	0.25359
5.2	299.81367	76.02927	0.25359
5.3	333.54482	84.58370	0.25359
5.4	371.01708	94.08684	0.25359
5.5	412.64189	104.64303	0.25359
5.6	458.87562	116.36803	0.25359
5.7	510.22452	129.39020	0.25359
5.8	567.25012	143.85195	0.25360
5.9	630.57526	159.91124	0.25360
6.0	700.89071	177.74325	0.25360

x	$F_{1/5}(x)$	$H_{4/5}(x)$	$T_{1/5}(x)$
6.0	700.89071	177.74325	0.25360
6.1	778.96261	197.54227	0.25360
6.2	865.64062	219.52377	0.25360
6.3	961.86701	243.92671	0.25360
6.4	1068.68667	271.01608	0.25360
6.5	1187.25832	301.08572	0.25360
6.6	1318.86678	334.45147	0.25360
6.7	1464.93670	371.50461	0.25360
6.8	1627.04773	412.61574	0.25360
6.9	1806.95125	458.23901	0.25360
7.0	2006.58906	508.86685	0.25360
7.1	2228.11398	565.04522	0.25360
7.2	2473.91267	627.37937	0.25360
7.3	2746.63101	696.54029	0.25360
7.4	3049.20213	773.27182	0.25360
7.5	3384.87750	858.39852	0.25360
7.6	3757.26135	952.83443	0.25360
7.7	4170.34888	1057.59271	0.25360
7.8	4628.56851	1173.79641	0.25360
7.9	5136.82869	1302.69030	0.25360
8.0	5700.56986	1445.65407	0.25360
8.1	6325.82188	1604.21688	0.25360
8.2	7019.26772	1780.07351	0.25360
8.3	7788.31405	1975.10229	0.25360
8.4	8641.16934	2191.38488	0.25360
8.5	9586.93047	2431.22821	0.25360
8.6	10635.67862	2697.18887	0.25360
8.7	11798.58552	2992.09998	0.25360
8.8	13088.03108	3319.10107	0.25360
8.9	14517.73379	3681.67111	0.25360
9.0	16102.89504	4083.66516	0.25360
9.1	17860.35910	4529.35490	0.25360
9.2	19808.79019	5023.47352	0.25360
9.3	21968.86871	5571.26556	0.25360
9.4	24363.50854	6178.54192	0.25360
9.5	27018.09769	6851.74096	0.25360
9.6	29960.76485	7557.99607	0.25360
9.7	33222.67468	8425.21055	0.25360
9.8	36838.35470	9342.14050	0.25360
9.9	40846.05746	10358.48672	0.25360
10.0	45288.16157	11484.99634	0.25360

TABLE 6B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 1/5$ and x from 1.50 to 10.0.

$\alpha = 2/5$

x	$F_{2/5}(x)$	$H_{3/5}(x)$	$T_{2/5}(x)$	x	$F_{2/5}(x)$	$H_{3/5}(x)$	$T_{2/5}(x)$	x	$F_{2/5}(x)$	$H_{3/5}(x)$	$T_{2/5}(x)$
0.0	1.00000	0.0	0.0	0.50	1.15977	0.32826	0.28304	1.00	1.68278	0.84439	0.50178
0.01	1.00006	0.00289	0.00289	0.51	1.16637	0.33668	0.28865	1.01	1.69773	0.85707	0.50483
0.02	1.00025	0.00664	0.00663	0.52	1.17312	0.34516	0.29422	1.02	1.71288	0.86986	0.50784
0.03	1.00056	0.01079	0.01079	0.53	1.18001	0.35371	0.29975	1.03	1.72823	0.88276	0.51079
0.04	1.00100	0.01525	0.01523	0.54	1.18704	0.36233	0.30524	1.04	1.74378	0.89578	0.51370
0.05	1.00156	0.01993	0.01990	0.55	1.19422	0.37102	0.31068	1.05	1.75954	0.90891	0.51656
0.06	1.00225	0.02481	0.02475	0.56	1.20155	0.37977	0.31607	1.06	1.77551	0.92216	0.51938
0.07	1.00306	0.02986	0.02977	0.57	1.20902	0.38860	0.32141	1.07	1.79168	0.93553	0.52215
0.08	1.00400	0.03506	0.03492	0.58	1.21664	0.39749	0.32671	1.08	1.80806	0.94901	0.52488
0.09	1.00507	0.04039	0.04018	0.59	1.22441	0.40646	0.33196	1.09	1.82466	0.96261	0.52756
0.10	1.00626	0.04584	0.04556	0.60	1.23232	0.41549	0.33716	1.10	1.84146	0.97634	0.53020
0.11	1.00757	0.05142	0.05103	0.61	1.24039	0.42460	0.34231	1.11	1.85848	0.99019	0.53279
0.12	1.00901	0.05710	0.05659	0.62	1.24861	0.43378	0.34741	1.12	1.87572	1.00416	0.53535
0.13	1.01058	0.06288	0.06222	0.63	1.25698	0.44304	0.35246	1.13	1.89318	1.01826	0.53786
0.14	1.01227	0.06875	0.06792	0.64	1.26550	0.45237	0.35746	1.14	1.91086	1.03248	0.54032
0.15	1.01409	0.07472	0.07368	0.65	1.27417	0.46177	0.36241	1.15	1.92876	1.04683	0.54275
0.16	1.01604	0.08078	0.07950	0.66	1.28300	0.47125	0.36730	1.16	1.94688	1.06131	0.54514
0.17	1.01811	0.08692	0.08537	0.67	1.29198	0.48080	0.37214	1.17	1.96523	1.07593	0.54748
0.18	1.02031	0.09314	0.09129	0.68	1.30112	0.49043	0.37693	1.18	1.98381	1.09067	0.54979
0.19	1.02264	0.09944	0.09724	0.69	1.31042	0.50014	0.38166	1.19	2.00262	1.10555	0.55206
0.20	1.02509	0.10582	0.10323	0.70	1.31988	0.50992	0.38634	1.20	2.02166	1.12057	0.55428
0.21	1.02767	0.11227	0.10925	0.71	1.32949	0.51979	0.39097	1.21	2.04093	1.13572	0.55647
0.22	1.03038	0.11880	0.11529	0.72	1.33927	0.52973	0.39554	1.22	2.06044	1.15102	0.55863
0.23	1.03322	0.12539	0.12136	0.73	1.34921	0.53976	0.40006	1.23	2.08019	1.16645	0.56074
0.24	1.03619	0.13206	0.12745	0.74	1.35930	0.54987	0.40452	1.24	2.10018	1.18202	0.56282
0.25	1.03928	0.13880	0.13355	0.75	1.36957	0.56006	0.40893	1.25	2.12041	1.19774	0.56486
0.26	1.04251	0.14560	0.13966	0.76	1.37999	0.57033	0.41328	1.26	2.14089	1.21360	0.56687
0.27	1.04586	0.15247	0.14578	0.77	1.39059	0.58069	0.41758	1.27	2.16161	1.22961	0.56884
0.28	1.04934	0.15941	0.15191	0.78	1.40135	0.59113	0.42183	1.28	2.18258	1.24577	0.57078
0.29	1.05296	0.16641	0.15804	0.79	1.41227	0.60166	0.42602	1.29	2.20380	1.26208	0.57268
0.30	1.05670	0.17348	0.16417	0.80	1.42337	0.61227	0.43016	1.30	2.22528	1.27854	0.57455
0.31	1.06058	0.18061	0.17030	0.81	1.43464	0.62298	0.43424	1.31	2.24701	1.29515	0.57639
0.32	1.06459	0.18781	0.17642	0.82	1.44608	0.63377	0.43827	1.32	2.26900	1.31192	0.57819
0.33	1.06873	0.19507	0.18253	0.83	1.45769	0.64465	0.44224	1.33	2.29125	1.32884	0.57996
0.34	1.07300	0.20240	0.18863	0.84	1.46947	0.65562	0.44616	1.34	2.31377	1.34592	0.58170
0.35	1.07740	0.20979	0.19471	0.85	1.48143	0.66669	0.45003	1.35	2.33654	1.36316	0.58341
0.36	1.08194	0.21724	0.20079	0.86	1.49357	0.67784	0.45384	1.36	2.35959	1.38057	0.58509
0.37	1.08661	0.22475	0.20684	0.87	1.50588	0.68909	0.45760	1.37	2.38291	1.39814	0.58674
0.38	1.09142	0.23233	0.21287	0.88	1.51838	0.70044	0.46131	1.38	2.40650	1.41587	0.58835
0.39	1.09636	0.23997	0.21888	0.89	1.53105	0.71188	0.46496	1.39	2.43036	1.43377	0.58994
0.40	1.10144	0.24768	0.22487	0.90	1.54391	0.72342	0.46856	1.40	2.45450	1.45184	0.59150
0.41	1.10665	0.25545	0.23083	0.91	1.55695	0.73506	0.47211	1.41	2.47892	1.47009	0.59303
0.42	1.11200	0.26328	0.23676	0.92	1.57017	0.74679	0.47561	1.42	2.50363	1.48850	0.59454
0.43	1.11748	0.27118	0.24267	0.93	1.58358	0.75863	0.47906	1.43	2.52862	1.50709	0.59601
0.44	1.12311	0.27914	0.24854	0.94	1.59718	0.77057	0.48246	1.44	2.55390	1.52586	0.59746
0.45	1.12887	0.28716	0.25438	0.95	1.61096	0.78261	0.48580	1.45	2.57946	1.54480	0.59889
0.46	1.13477	0.29525	0.26019	0.96	1.62494	0.79475	0.48910	1.46	2.60533	1.56393	0.60028
0.47	1.14081	0.30340	0.26596	0.97	1.63911	0.80700	0.49234	1.47	2.63148	1.58324	0.60165
0.48	1.14699	0.31162	0.27169	0.98	1.65347	0.81936	0.49554	1.48	2.65794	1.60273	0.60300
0.49	1.15331	0.31991	0.27738	0.99	1.66802	0.83182	0.49868	1.49	2.68470	1.62241	0.60432
0.50	1.15977	0.32826	0.28304	1.00	1.68278	0.84439	0.50178	1.50	2.71176	1.64228	0.60561

TABLE 7A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 2/5$ and x from 0.00 to 1.50.

$\alpha = 2/5$

x	$F_{2/5}(x)$	$H_{3/5}(x)$	$T_{2/5}(x)$
1.50	2.71176	1.64228	0.60561
1.51	2.73913	1.66234	0.60689
1.52	2.76681	1.68259	0.60813
1.53	2.79481	1.70304	0.60936
1.54	2.82312	1.72369	0.61056
1.55	2.85175	1.74453	0.61174
1.56	2.88070	1.76558	0.61290
1.57	2.90998	1.78683	0.61403
1.58	2.93959	1.80828	0.61515
1.59	2.96952	1.82995	0.61624
1.60	2.99980	1.85182	0.61731
1.61	3.03041	1.87391	0.61837
1.62	3.06136	1.89621	0.61940
1.63	3.09266	1.91873	0.62041
1.64	3.12430	1.94147	0.62141
1.65	3.15630	1.96443	0.62238
1.66	3.18865	1.98761	0.62334
1.67	3.22136	2.01102	0.62428
1.68	3.25443	2.03466	0.62520
1.69	3.28786	2.05854	0.62610
1.70	3.32166	2.08264	0.62699
1.71	3.35584	2.10699	0.62786
1.72	3.39039	2.13157	0.62871
1.73	3.42532	2.15640	0.62955
1.74	3.46064	2.18146	0.63037
1.75	3.49634	2.20678	0.63117
1.76	3.53243	2.23235	0.63196
1.77	3.56892	2.25817	0.63273
1.78	3.60580	2.28424	0.63349
1.79	3.64309	2.31057	0.63423
1.80	3.68078	2.33716	0.63496
1.81	3.71888	2.36402	0.63568
1.82	3.75740	2.39114	0.63638
1.83	3.79634	2.41853	0.63707
1.84	3.83569	2.44620	0.63775
1.85	3.87548	2.47413	0.63841
1.86	3.91569	2.50235	0.63906
1.87	3.95634	2.53085	0.63969
1.88	3.99743	2.55963	0.64032
1.89	4.03897	2.58869	0.64093
1.90	4.08095	2.61805	0.64153
1.91	4.12338	2.64770	0.64212
1.92	4.16627	2.67764	0.64270
1.93	4.20963	2.70789	0.64326
1.94	4.25345	2.73844	0.64382
1.55	4.29774	2.76929	0.64436
1.96	4.34250	2.80045	0.64489
1.97	4.38775	2.83192	0.64542
1.98	4.43348	2.86371	0.64593
1.99	4.47970	2.89582	0.64643
2.0C	4.52641	2.92825	0.64692

x	$F_{2/5}(x)$	$H_{3/5}(x)$	$T_{2/5}(x)$
2.0	4.52641	2.92825	0.64692
2.1	5.02188	3.27101	0.65135
2.2	5.57258	3.64995	0.65498
2.3	6.18434	4.06905	0.65796
2.4	6.86361	4.53271	0.66040
2.5	7.61753	5.04580	0.66239
2.6	8.45406	5.61371	0.66403
2.7	9.38197	6.24240	0.66536
2.8	10.41103	6.93848	0.66645
2.9	11.55204	7.70923	0.66735
3.0	12.81695	8.56274	0.66808
3.1	14.21903	9.50795	0.66868
3.2	15.77295	10.55473	0.66917
3.3	17.49496	11.71404	0.66957
3.4	19.40306	12.99799	0.66989
3.5	21.51718	14.41998	0.67016
3.6	23.85938	15.99486	0.67038
3.7	26.45408	17.73903	0.67056
3.8	29.32832	19.67067	0.67071
3.9	32.51202	21.80988	0.67083
4.0	36.03831	24.17894	0.67092
4.1	39.94386	26.80246	0.67100
4.2	44.26924	29.70771	0.67107
4.3	49.05939	32.92486	0.67112
4.4	54.36401	36.48730	0.67117
4.5	60.23811	40.43196	0.67120
4.6	66.74260	44.79975	0.67123
4.7	73.94486	49.63591	0.67126
4.8	81.91947	54.99052	0.67128
4.9	90.74895	60.91899	0.67129
5.0	100.52464	67.48265	0.67130
5.1	111.34759	74.74935	0.67132
5.2	123.32965	82.79418	0.67132
5.3	136.59457	91.70023	0.67133
5.4	151.27930	101.55944	0.67134
5.5	167.53537	112.47355	0.67134
5.6	185.53044	124.55513	0.67135
5.7	205.45005	137.92875	0.67135
5.8	227.49948	152.73222	0.67135
5.9	251.90588	169.11805	0.67135
6.0	278.92057	187.25497	0.67136

x	$F_{2/5}(x)$	$H_{3/5}(x)$	$T_{2/5}(x)$
6.0	278.92057	187.25497	0.67136
6.1	308.82162	207.32967	0.67136
6.2	341.91671	229.54871	0.67136
6.3	378.54625	254.14063	0.67136
6.4	419.08687	281.35829	0.67136
6.5	463.95527	311.48146	0.67136
6.6	513.61248	344.81964	0.67136
6.7	568.56856	381.71529	0.67136
6.8	629.38782	422.54725	0.67136
6.9	696.69459	467.73468	0.67136
7.0	771.17956	517.74129	0.67136
7.1	853.60686	573.08008	0.67136
7.2	944.82186	634.31861	0.67136
7.3	1043.75977	702.08474	0.67136
7.4	1157.45522	777.07309	0.67136
7.5	1281.05275	860.05207	0.67136
7.6	1417.81857	951.87175	0.67136
7.7	1569.15340	1053.47253	0.67136
7.8	1736.60676	1165.89472	0.67136
7.9	1921.89281	1290.28911	0.67136
8.0	2126.90775	1427.92878	0.67136
8.1	2353.74921	1580.22198	0.67136
8.2	2604.73758	1748.72653	0.67136
8.3	2882.43966	1935.16571	0.67136
8.4	3189.69479	2141.44573	0.67136
8.5	3529.64379	2369.67524	0.67136
8.6	3905.76091	2622.18672	0.67136
8.7	4321.88925	2901.56028	0.67136
8.8	4782.27981	3210.64990	0.67136
8.9	5291.63481	3552.61247	0.67136
9.0	5855.15553	3930.93995	0.67136
9.1	6478.59521	4349.49486	0.67136
9.2	7168.31763	4812.54961	0.67136
9.3	7931.36179	5324.82992	0.67136
9.4	8775.51354	5891.56294	0.67136
9.5	9709.38476	6518.53038	0.67136
9.6	10742.50093	7212.12729	0.67136
9.7	11885.39794	7979.42709	0.67136
9.8	13149.72926	8828.25351	0.67136
9.9	14548.38436	9767.26006	0.67136
10.0	16095.61973	10806.01804	0.67136

TABLE 7B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 2/5$ and x from 1.50 to 10.0.

$\alpha = 3/5$

x	$F_{3/5}(x)$	$H_{2/5}(x)$	$T_{3/5}(x)$
0.0	1.00000	0.0	0.0
0.01	1.00004	0.03607	0.03607
0.02	1.00017	0.06280	0.06279
0.03	1.00038	0.08687	0.08684
0.04	1.00067	0.10937	0.10929
0.05	1.00104	0.13076	0.13063
0.06	1.00150	0.15133	0.15110
0.07	1.00204	0.17123	0.17088
0.08	1.00267	0.19058	0.19008
0.09	1.00338	0.20948	0.20877
0.10	1.00417	0.22748	0.22703
0.11	1.00505	0.24613	0.24490
0.12	1.00601	0.26398	0.26241
0.13	1.00705	0.28157	0.27959
0.14	1.00818	0.29891	0.29648
0.15	1.00939	0.31603	0.31309
0.16	1.01069	0.33296	0.32944
0.17	1.01207	0.34971	0.34554
0.18	1.01353	0.36631	0.36141
0.19	1.01508	0.38275	0.37706
0.20	1.01672	0.39906	0.39250
0.21	1.01844	0.41525	0.40773
0.22	1.02026	0.43132	0.42276
0.23	1.02213	0.44729	0.43761
0.24	1.02411	0.46317	0.45227
0.25	1.02617	0.47897	0.46675
0.26	1.02832	0.49468	0.48106
0.27	1.03055	0.51032	0.49520
0.28	1.03287	0.52590	0.50917
0.29	1.03527	0.54142	0.52298
0.30	1.03776	0.55689	0.53662
0.31	1.04034	0.57231	0.55012
0.32	1.04301	0.58769	0.56345
0.33	1.04576	0.60303	0.57664
0.34	1.04860	0.61834	0.58968
0.35	1.05153	0.63362	0.60257
0.36	1.05455	0.64887	0.61531
0.37	1.05765	0.66411	0.62791
0.38	1.06085	0.67933	0.64037
0.39	1.06413	0.69454	0.65268
0.40	1.06750	0.70974	0.66486
0.41	1.07097	0.72494	0.67690
0.42	1.07452	0.74013	0.68880
0.43	1.07816	0.75532	0.70057
0.44	1.08189	0.77052	0.71220
0.45	1.08572	0.78573	0.72370
0.46	1.08963	0.80095	0.73506
0.47	1.09364	0.81618	0.74630
0.48	1.09774	0.83143	0.75740
0.49	1.10193	0.84670	0.76838
0.5C	1.10622	0.86199	0.77922

x	$F_{3/5}(x)$	$H_{2/5}(x)$	$T_{3/5}(x)$
0.50	1.10622	0.86199	0.77922
0.51	1.11060	0.87731	0.78994
0.52	1.11507	0.89265	0.80054
0.53	1.11963	0.90803	0.81100
C.54	1.12429	0.92343	0.82134
0.55	1.12905	0.93887	0.83156
0.56	1.13390	0.95435	0.84166
0.57	1.13885	0.96987	0.85163
0.58	1.14389	0.98544	0.86148
0.59	1.14903	1.00104	0.87121
0.60	1.15427	1.01670	0.88081
0.61	1.15960	1.03240	0.89030
0.62	1.16504	1.04815	0.89968
0.63	1.17057	1.06396	0.90893
0.64	1.17620	1.07983	0.91807
C.65	1.18193	1.09575	0.92709
0.66	1.18776	1.11174	0.93599
0.67	1.19370	1.12778	0.94478
0.68	1.19973	1.14389	0.95346
0.69	1.20587	1.16007	0.96202
0.70	1.21211	1.17632	0.97048
0.71	1.21845	1.19264	0.97882
0.72	1.22489	1.20903	0.98705
0.73	1.23145	1.22550	0.99517
0.74	1.23810	1.24204	1.00318
C.75	1.24486	1.25866	1.01109
0.76	1.25173	1.27537	1.01889
C.77	1.25870	1.29216	1.02658
0.78	1.26579	1.30903	1.03416
0.79	1.27298	1.32599	1.04165
0.80	1.28028	1.34304	1.04903
0.81	1.28769	1.36019	1.05630
0.82	1.29521	1.37742	1.06348
0.83	1.30284	1.39475	1.07055
0.84	1.31058	1.41218	1.07753
0.85	1.31843	1.42971	1.08440
C.86	1.32640	1.44734	1.09118
0.87	1.33448	1.46508	1.09786
0.88	1.34268	1.48292	1.10445
0.89	1.35099	1.50086	1.11094
0.90	1.35942	1.51892	1.11733
0.91	1.36797	1.53709	1.12363
0.92	1.37663	1.55537	1.12984
0.93	1.38541	1.57377	1.13596
0.54	1.39431	1.59229	1.14199
0.55	1.40333	1.61092	1.14792
0.96	1.41248	1.62968	1.15377
0.97	1.42174	1.64856	1.15953
C.98	1.43113	1.66757	1.16521
0.99	1.44064	1.68670	1.17080
1.00	1.45028	1.70597	1.17630

x	$F_{3/5}(x)$	$H_{2/5}(x)$	$T_{3/5}(x)$
1.00	1.45028	1.70597	1.17630
1.01	1.46004	1.72536	1.18172
1.02	1.46993	1.74489	1.18706
1.03	1.47995	1.76456	1.19231
1.04	1.49009	1.78436	1.19748
1.05	1.50037	1.80431	1.20258
1.C6	1.51077	1.82439	1.20759
1.07	1.52131	1.84463	1.21253
1.08	1.53198	1.86500	1.21738
1.C9	1.54278	1.88553	1.22217
1.10	1.55371	1.90621	1.22687
1.11	1.56479	1.92704	1.23150
1.12	1.57599	1.94802	1.23606
1.13	1.58734	1.96917	1.24055
1.14	1.59882	1.99047	1.24496
1.15	1.61044	2.01193	1.24930
1.16	1.62221	2.03356	1.25357
1.17	1.63411	2.05535	1.25778
1.18	1.64616	2.07731	1.26191
1.19	1.65836	2.09944	1.26598
1.20	1.67069	2.12175	1.26998
1.21	1.68318	2.14423	1.27392
1.22	1.69581	2.16688	1.27779
1.23	1.70859	2.18972	1.28159
1.24	1.72152	2.21274	1.28534
1.25	1.73460	2.23594	1.28902
1.26	1.74784	2.25932	1.29264
1.27	1.76123	2.28290	1.29620
1.28	1.77477	2.30667	1.29970
1.29	1.78847	2.33063	1.30314
1.30	1.80233	2.35479	1.30653
1.31	1.81634	2.37914	1.30985
1.32	1.83052	2.40369	1.31312
1.33	1.84485	2.42845	1.31634
1.34	1.85935	2.45342	1.31950
1.35	1.87402	2.47859	1.32261
1.36	1.88885	2.50397	1.32566
1.37	1.90384	2.52956	1.32866
1.38	1.91901	2.55537	1.33161
1.39	1.93434	2.58140	1.33451
1.40	1.94985	2.60765	1.33736
1.41	1.96553	2.63412	1.34016
1.42	1.98138	2.66082	1.34291
1.43	1.99741	2.68775	1.34562
1.44	2.01361	2.71490	1.34828
1.45	2.03000	2.74229	1.35089
1.46	2.04656	2.76992	1.35345
1.47	2.06331	2.79779	1.35597
1.48	2.08024	2.82589	1.35845
1.49	2.09735	2.85425	1.36088
1.5C	2.11465	2.88285	1.36327

TABLE 8A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/5$ and x from 0.00 to 1.50.

$\alpha = 3/5$

x	$F_{3/5}(x)$	$H_{2/5}(x)$	$T_{3/5}(x)$
1.50	2.11465	2.88285	1.36327
1.51	2.13214	2.91169	1.36562
1.52	2.14982	2.94080	1.36792
1.53	2.16770	2.97015	1.37019
1.54	2.18576	2.99977	1.37241
1.55	2.20402	3.02965	1.37460
1.56	2.22248	3.05979	1.37675
1.57	2.24113	3.09020	1.37886
1.58	2.25999	3.12088	1.38093
1.59	2.27904	3.15183	1.38296
1.60	2.29830	3.18306	1.38496
1.61	2.31777	3.21456	1.38692
1.62	2.33744	3.24635	1.38885
1.63	2.35733	3.27843	1.39074
1.64	2.37742	3.31079	1.39260
1.65	2.39773	3.34344	1.39442
1.66	2.41825	3.37639	1.39621
1.67	2.43899	3.40964	1.39797
1.68	2.45995	3.44319	1.39970
1.69	2.48113	3.47704	1.40139
1.70	2.50253	3.51120	1.40306
1.71	2.52416	3.54567	1.40469
1.72	2.54601	3.58045	1.40630
1.73	2.56810	3.61555	1.40787
1.74	2.59041	3.65098	1.40942
1.75	2.61296	3.68672	1.41094
1.76	2.63574	3.72280	1.41243
1.77	2.65876	3.75920	1.41389
1.78	2.68202	3.79594	1.41533
1.79	2.70553	3.83302	1.41674
1.80	2.72927	3.87044	1.41812
1.81	2.75327	3.90820	1.41948
1.82	2.77751	3.94632	1.42081
1.83	2.80200	3.98478	1.42212
1.84	2.82675	4.02361	1.42341
1.85	2.85175	4.06279	1.42467
1.86	2.87701	4.10234	1.42590
1.87	2.90253	4.14225	1.42712
1.88	2.92831	4.18253	1.42831
1.89	2.95436	4.22320	1.42948
1.90	2.98067	4.26423	1.43063
1.91	3.00726	4.30566	1.43175
1.92	3.03412	4.34747	1.43286
1.93	3.06125	4.38967	1.43394
1.94	3.08866	4.43226	1.43501
1.95	3.11636	4.47526	1.43605
1.96	3.14433	4.51865	1.43708
1.97	3.17259	4.56246	1.43809
1.98	3.20114	4.60668	1.43907
1.99	3.22998	4.65131	1.44004
2.00	3.25912	4.69636	1.44099

x	$F_{3/5}(x)$	$H_{2/5}(x)$	$T_{3/5}(x)$
2.0	3.25912	4.69636	1.44099
2.1	3.56725	5.17096	1.44957
2.2	3.90799	5.69257	1.45665
2.3	4.28459	6.26617	1.46249
2.4	4.70063	6.89726	1.46731
2.5	5.16006	7.59185	1.47127
2.6	5.66727	8.35659	1.47453
2.7	6.22710	9.19878	1.47722
2.8	6.84489	10.12649	1.47942
2.9	7.52655	11.14858	1.48123
3.0	8.27860	12.27485	1.48272
3.1	9.10823	13.51608	1.48394
3.2	10.02339	14.88417	1.48494
3.3	11.03285	16.39224	1.48577
3.4	12.14631	18.05476	1.48644
3.5	13.37444	19.88770	1.48699
3.6	14.72906	21.90868	1.48745
3.7	16.22317	24.13713	1.48782
3.8	17.87117	26.59449	1.48812
3.9	19.68890	29.30442	1.48837
4.0	21.69389	32.29303	1.48858
4.1	23.90546	35.58913	1.48874
4.2	26.34495	39.22452	1.48888
4.3	29.03589	43.23429	1.48899
4.4	32.00427	47.65715	1.48909
4.5	35.27878	52.53584	1.48916
4.6	38.89107	57.91754	1.48922
4.7	42.87609	63.85430	1.48928
4.8	47.27239	70.40357	1.48932
4.9	52.12255	77.62878	1.48935
5.0	57.47356	85.59991	1.48938
5.1	63.37728	94.39423	1.48940
5.2	69.89096	104.09703	1.48942
5.3	77.07779	114.80242	1.48944
5.4	85.00753	126.61432	1.48945
5.5	93.75716	139.64742	1.48946
5.6	103.41170	154.02832	1.48947
5.7	114.06496	169.89679	1.48947
5.8	125.82052	187.40709	1.48948
5.9	138.79270	206.72954	1.48948
6.0	153.10773	228.05212	1.48949

x	$F_{3/5}(x)$	$H_{2/5}(x)$	$T_{3/5}(x)$
6.0	153.10773	228.05212	1.48949
6.1	168.90493	251.58239	1.48949
6.2	186.33813	277.54946	1.48949
6.3	205.57712	306.20625	1.48950
6.4	226.80937	337.83198	1.48950
6.5	250.24183	372.73492	1.48950
6.6	276.10298	411.25538	1.48950
6.7	304.64504	453.76907	1.48950
6.8	336.14649	500.69077	1.48950
6.9	370.91477	552.47842	1.48950
7.0	409.28931	609.63759	1.48950
7.1	451.64484	672.72646	1.48950
7.2	498.39511	742.36131	1.48950
7.3	549.99691	819.22253	1.48950
7.4	606.95457	904.06134	1.48950
7.5	669.82494	997.70714	1.48950
7.6	739.22282	1101.07568	1.48950
7.7	815.82701	1215.17807	1.48950
7.8	900.38700	1341.13066	1.48950
7.9	993.73032	1480.16606	1.48950
8.0	1096.77069	1633.64526	1.48950
8.1	1210.51696	1803.07095	1.48950
8.2	1336.08310	1990.10239	1.48950
8.3	1474.69908	2196.57164	1.48950
8.4	1627.72303	2424.50162	1.48951
8.5	1796.65455	2676.12602	1.48951
8.6	1983.14952	2953.91126	1.48951
8.7	2189.03632	3260.58073	1.48951
8.8	2416.33389	3599.14166	1.48951
8.9	2667.27158	3972.91466	1.48951
9.0	2944.51108	4385.56643	1.48951
9.1	3250.17066	4841.14586	1.48951
9.2	3587.85195	5344.12390	1.48951
9.3	3960.66950	5899.43758	1.48951
9.4	4372.28341	6512.53863	1.48951
9.5	4826.73538	7189.44720	1.48951
9.6	5328.48855	7936.81115	1.48951
9.7	5882.47146	8761.97155	1.48951
9.8	6494.12659	9673.03503	1.48951
9.9	7169.46404	10678.95366	1.48951
10.0	7915.12075	11789.61318	1.48951

TABLE 8B. **Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/5$ and x from 1.50 to 10.0.**

$\alpha = 4/5$

x	$F_{4/5}(x)$	$H_{1/5}(x)$	$T_{4/5}(x)$	x	$F_{4/5}(x)$	$H_{1/5}(x)$	$T_{4/5}(x)$	x	$F_{4/5}(x)$	$H_{1/5}(x)$	$T_{4/5}(x)$
0.0	1.00000	0.0	0.0	0.50	1.07949	3.02345	2.80081	1.00	1.33486	4.62477	3.46461
0.01	1.00003	0.60057	0.60056	0.51	1.08276	3.05377	2.82035	1.01	1.34206	4.66104	3.47305
0.02	1.00013	0.79251	0.79241	0.52	1.08610	3.08403	2.83955	1.02	1.34936	4.69737	3.48134
0.03	1.00028	0.93215	0.93189	0.53	1.08951	3.11425	2.85840	1.03	1.35674	4.73435	3.48950
0.04	1.00050	1.04599	1.04547	C.54	1.09299	3.14444	2.87693	1.04	1.36422	4.77139	3.49752
C.05	1.00078	1.14306	1.14297	0.55	1.09654	3.17461	2.89513	1.05	1.37179	4.80869	3.50541
0.06	1.00113	1.23068	1.22929	0.56	1.10015	3.20477	2.91302	1.06	1.37946	4.84626	3.51317
0.C7	1.00153	1.30930	1.30730	0.57	1.10384	3.23493	2.93060	1.07	1.38722	4.88410	3.52080
0.C8	1.00200	1.38157	1.37881	C.58	1.10761	3.26509	2.94788	1.08	1.39507	4.92222	3.52830
0.09	1.00253	1.44873	1.44507	0.59	1.11144	3.29526	2.96486	1.09	1.40302	4.96061	3.53567
0.10	1.00313	1.51169	1.50698	0.60	1.11534	3.32546	2.98156	1.10	1.41107	4.99929	3.54292
0.11	1.00378	1.57112	1.56520	0.61	1.11932	3.35569	2.99798	1.11	1.41921	5.03826	3.55005
0.12	1.00450	1.62754	1.62024	0.62	1.12337	3.38596	3.01411	1.12	1.42745	5.07752	3.55706
0.13	1.00529	1.68137	1.67253	C.63	1.12749	3.41627	3.02998	1.13	1.43579	5.11708	3.56395
0.14	1.00613	1.73293	1.72237	0.64	1.13169	3.44664	3.04558	1.14	1.44423	5.15693	3.57072
C.15	1.00704	1.78249	1.77003	0.65	1.13595	3.47706	3.06092	1.15	1.45276	5.19710	3.57739
0.16	1.00801	1.83029	1.81574	0.66	1.14030	3.50755	3.07600	1.16	1.46140	5.23757	3.58393
0.17	1.00905	1.87650	1.85967	C.67	1.14471	3.53812	3.09083	1.17	1.47014	5.27835	3.59037
0.18	1.01015	1.92129	1.90199	0.68	1.14920	3.56876	3.10542	1.18	1.47898	5.31946	3.59670
0.19	1.01131	1.96481	1.94284	0.69	1.15377	3.59949	3.11977	1.19	1.48793	5.36088	3.60292
0.20	1.01253	2.00716	1.98231	0.70	1.15841	3.63032	3.13387	1.20	1.49697	5.40263	3.60903
0.21	1.01382	2.04846	2.02053	0.71	1.16313	3.66124	3.14775	1.21	1.50613	5.44472	3.61505
0.22	1.01518	2.08880	2.05757	0.72	1.16792	3.69226	3.16139	1.22	1.51538	5.48714	3.62095
0.23	1.01659	2.12825	2.09352	C.73	1.17279	3.72340	3.17482	1.23	1.52475	5.52989	3.62676
0.24	1.01807	2.16691	2.12844	C.74	1.17774	3.75465	3.18802	1.24	1.53421	5.57299	3.63247
0.25	1.01962	2.20482	2.16240	0.75	1.18276	3.78603	3.20100	1.25	1.54379	5.61644	3.63808
0.26	1.02122	2.24204	2.19545	0.76	1.18787	3.81753	3.21377	1.26	1.55348	5.66024	3.64360
0.27	1.02290	2.27865	2.22764	C.77	1.19305	3.84916	3.22633	1.27	1.56327	5.70440	3.64902
0.28	1.02463	2.31467	2.25902	C.78	1.19830	3.88093	3.23868	1.28	1.57317	5.74892	3.65435
0.29	1.02644	2.35015	2.28963	0.79	1.20364	3.91284	3.25084	1.29	1.58319	5.79380	3.65958
0.30	1.02830	2.38515	2.31950	0.80	1.20906	3.94491	3.26279	1.30	1.59331	5.83905	3.66473
0.31	1.03023	2.41968	2.34868	0.81	1.21456	3.97712	3.27455	1.31	1.60355	5.88468	3.66978
0.32	1.03223	2.45380	2.37718	0.82	1.22014	4.00950	3.28611	1.32	1.61390	5.93069	3.67475
0.33	1.03429	2.48752	2.40505	0.83	1.22579	4.04204	3.29748	1.33	1.62437	5.97708	3.67964
0.34	1.03642	2.52088	2.43231	0.84	1.23153	4.07474	3.30867	1.34	1.63495	6.02385	3.68444
C.35	1.03861	2.55391	2.45897	0.85	1.23736	4.10762	3.31968	1.35	1.64564	6.07102	3.68915
0.36	1.04087	2.58663	2.48507	0.86	1.24326	4.14068	3.33050	1.36	1.65645	6.11859	3.69379
0.37	1.04319	2.61906	2.51063	C.87	1.24925	4.17392	3.34115	1.37	1.66738	6.16655	3.69834
0.38	1.04558	2.65124	2.53566	0.88	1.25532	4.20735	3.35162	1.38	1.67843	6.21493	3.70281
0.39	1.04804	2.68317	2.56019	C.89	1.26147	4.24097	3.36192	1.39	1.68960	6.26371	3.70721
0.40	1.05056	2.71488	2.58422	0.90	1.26771	4.27478	3.37205	1.40	1.70089	6.31291	3.71153
0.41	1.05315	2.74639	2.60779	0.91	1.27403	4.30880	3.38201	1.41	1.71230	6.36252	3.71577
0.42	1.05580	2.77771	2.63089	0.92	1.28044	4.34303	3.39181	1.42	1.72383	6.41256	3.71994
C.43	1.05853	2.80886	2.65356	0.93	1.28694	4.37746	3.40145	1.43	1.73549	6.46303	3.72404
0.44	1.06132	2.83987	2.67579	C.94	1.29352	4.41211	3.41093	1.44	1.74727	6.51394	3.72806
0.45	1.06418	2.87073	2.69761	C.95	1.30019	4.44698	3.42026	1.45	1.75918	6.56528	3.73202
0.46	1.06710	2.90147	2.71902	C.96	1.30695	4.48207	3.42943	1.46	1.77121	6.61707	3.73590
0.47	1.07010	2.93210	2.74003	0.97	1.31379	4.51739	3.43844	1.47	1.78337	6.66930	3.73972
0.48	1.07316	2.96263	2.76066	0.98	1.32072	4.55295	3.44731	1.48	1.79566	6.72198	3.74347
C.49	1.07629	2.99308	2.78092	0.99	1.32775	4.58874	3.45604	1.49	1.80808	6.77513	3.74715
0.50	1.07949	3.02345	2.80081	1.00	1.33486	4.62477	3.46461	1.5C	1.82062	6.82873	3.75077

TABLE 9A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 4/5$ and x from 0.00 to 1.50.

$\alpha = 4/5$

x	$F_{4/5}(x)$	$H_{1/5}(x)$	$T_{4/5}(x)$
1.50	1.82062	6.82873	3.75077
1.51	1.83330	6.88281	3.75432
1.52	1.84612	6.93736	3.75781
1.53	1.85906	6.99238	3.76124
1.54	1.87214	7.04789	3.76461
1.55	1.88536	7.10388	3.76791
1.56	1.89872	7.16037	3.77116
1.57	1.91221	7.21735	3.77435
1.58	1.92584	7.27484	3.77749
1.59	1.93961	7.33283	3.78057
1.60	1.95353	7.39134	3.78359
1.61	1.96758	7.45037	3.78656
1.62	1.98179	7.50992	3.78947
1.63	1.99613	7.57000	3.79234
1.64	2.01062	7.63062	3.79515
1.65	2.02527	7.69178	3.79791
1.66	2.04006	7.75348	3.80062
1.67	2.05500	7.81573	3.80328
1.68	2.07009	7.87854	3.80590
1.69	2.08533	7.94192	3.80847
1.70	2.10073	8.00586	3.81099
1.71	2.11628	8.07037	3.81346
1.72	2.13200	8.13547	3.81589
1.73	2.14786	8.20115	3.81828
1.74	2.16389	8.26742	3.82062
1.75	2.18008	8.33429	3.82292
1.76	2.19643	8.40176	3.82518
1.77	2.21295	8.46984	3.82740
1.78	2.22963	8.53854	3.82958
1.79	2.24648	8.60786	3.83171
1.80	2.26349	8.67780	3.83381
1.81	2.28068	8.74838	3.83587
1.82	2.29803	8.81960	3.83790
1.83	2.31556	8.89146	3.83988
1.84	2.33326	8.96398	3.84183
1.85	2.35113	9.03716	3.84374
1.86	2.36919	9.11100	3.84562
1.87	2.38742	9.18551	3.84747
1.88	2.40583	9.26070	3.84928
1.89	2.42442	9.33658	3.85105
1.90	2.44320	9.41315	3.85280
1.91	2.46216	9.49041	3.85451
1.92	2.48131	9.56839	3.85619
1.93	2.50064	9.64707	3.85784
1.94	2.52017	9.72647	3.85946
1.95	2.53988	9.80660	3.86104
1.96	2.55979	9.88746	3.86260
1.97	2.57990	9.96906	3.86413
1.98	2.60020	10.05141	3.86564
1.99	2.62070	10.13452	3.86711
2.00	2.64139	10.21838	3.86856

x	$F_{4/5}(x)$	$H_{1/5}(x)$	$T_{4/5}(x)$
2.0	2.64139	10.21838	3.86856
2.1	2.85978	11.10058	3.88162
2.2	3.10023	12.06747	3.89244
2.3	3.36483	13.12750	3.90139
2.4	3.65585	14.28993	3.90878
2.5	3.97583	15.56493	3.91488
2.6	4.32755	16.96362	3.91992
2.7	4.71406	18.49825	3.92406
2.8	5.13873	20.18227	3.92748
2.9	5.60529	22.03044	3.93029
3.0	6.11783	24.05901	3.93261
3.1	6.68084	26.28582	3.93451
3.2	7.29929	28.73051	3.93607
3.3	7.97862	31.41467	3.93736
3.4	8.72485	34.36206	3.93841
3.5	9.54459	37.59880	3.93928
3.6	10.44511	41.15365	3.93999
3.7	11.43442	45.05822	3.94058
3.8	12.52134	49.34733	3.94106
3.9	13.71558	54.05928	3.94145
4.0	15.02781	59.23621	3.94177
4.1	16.46979	64.92454	3.94204
4.2	18.05446	71.17530	3.94226
4.3	19.79607	78.04472	3.94243
4.4	21.71031	85.59465	3.94258
4.5	23.81444	93.89320	3.94270
4.6	26.12747	103.01536	3.94280
4.7	28.67033	113.04365	3.94288
4.8	31.46606	124.06897	3.94295
4.9	34.54004	136.19136	3.94300
5.0	37.92019	149.52099	3.94304
5.1	41.63729	164.17919	3.94308
5.2	45.72521	180.29953	3.94311
5.3	50.22124	198.02911	3.94313
5.4	55.16647	217.52993	3.94315
5.5	60.60614	238.98039	3.94317
5.6	66.59008	262.57698	3.94318
5.7	73.17316	288.53610	3.94320
5.8	80.41583	317.09608	3.94320
5.9	88.38466	348.51946	3.94321
6.0	97.15298	383.09540	3.94322

x	$F_{4/5}(x)$	$H_{1/5}(x)$	$T_{4/5}(x)$
6.0	97.15298	383.09540	3.94322
6.1	106.80157	421.14242	3.94322
6.2	117.41941	463.01142	3.94323
6.3	129.10452	509.08890	3.94323
6.4	141.96489	559.80068	3.94323
6.5	156.11948	615.61587	3.94324
6.6	171.69934	677.05126	3.94324
6.7	188.84889	744.67626	3.94324
6.8	207.72720	819.11820	3.94324
6.9	228.50956	901.06828	3.94324
7.0	251.38912	991.28809	3.94324
7.1	276.57868	1090.61681	3.94324
7.2	304.31274	1199.97911	3.94324
7.3	334.84970	1320.39393	3.94324
7.4	368.47431	1452.98408	3.94324
7.5	405.50035	1598.98691	3.94324
7.6	446.27361	1759.76597	3.94324
7.7	491.17519	1936.82395	3.94324
7.8	540.62505	2131.81696	3.94324
7.9	595.08607	2346.57016	3.94324
8.0	655.06836	2583.09512	3.94325
8.1	721.13418	2843.60889	3.94325
8.2	793.90321	3130.55508	3.94325
8.3	874.05848	3446.62701	3.94325
8.4	962.35283	3794.79337	3.94325
8.5	1059.61611	4178.32639	3.94325
8.6	1166.76302	4600.83300	3.94325
8.7	1284.80185	5066.28910	3.94325
8.8	1414.84405	5579.07745	3.94325
8.9	1558.11484	6144.02939	3.94325
9.0	1715.96487	6766.47083	3.94325
9.1	1889.88308	7452.27307	3.94325
9.2	2081.51091	8207.90869	3.94325
9.3	2292.65795	9040.51334	3.94325
9.4	2525.31920	9957.95379	3.94325
9.5	2781.69411	10968.90301	3.94325
9.6	3064.20757	12082.92298	3.94325
9.7	3375.53310	13310.55601	3.94325
9.8	3718.61835	14663.42546	3.94325
9.9	4096.71333	16154.34682	3.94325
10.0	4513.40140	17797.45024	3.94325

TABLE 9B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 4/5$ and x from 1.50 to 10.0.

$\alpha = 2/7$

x	$F_{2/7}(x)$	$H_{5/7}(x)$	$T_{2/7}(x)$	x	$F_{2/7}(x)$	$H_{5/7}(x)$	$T_{2/7}(x)$	x	$F_{2/7}(x)$	$H_{5/7}(x)$	$T_{2/7}(x)$
0.0	1.00000	0.0	0.0	0.50	1.22412	0.20034	0.16366	1.00	1.96323	0.59952	0.30537
0.01	1.00009	0.00072	0.00072	0.51	1.23340	0.20639	0.16733	1.01	1.98447	0.60980	0.30728
C.02	1.00035	0.00195	0.00194	0.52	1.24288	0.21251	0.17098	1.02	2.00599	0.62018	0.30916
0.03	1.00079	0.00347	0.00347	0.53	1.25257	0.21870	0.17460	1.03	2.02781	0.63067	0.31101
0.04	1.00140	0.00524	0.00523	C.54	1.26246	0.22497	0.17820	1.04	2.04993	0.64126	0.31282
0.05	1.00219	0.00720	0.00719	0.55	1.27256	0.23130	0.18176	1.05	2.07233	0.65197	0.31461
C.06	1.00315	0.00935	0.00932	C.56	1.28286	0.23771	0.18530	1.06	2.09504	0.66278	0.31636
0.C7	1.00429	0.01166	0.01161	0.57	1.29337	0.24419	0.18880	1.07	2.11805	0.67370	0.31808
0.08	1.00560	0.01411	0.01403	0.58	1.30410	0.25075	0.19228	1.08	2.14137	0.68474	0.31977
0.09	1.00709	0.01670	0.01658	0.59	1.31503	0.25738	0.19572	1.09	2.16499	0.69588	0.32143
0.10	1.00876	0.01942	0.01925	0.60	1.32617	0.26408	0.19913	1.10	2.18892	0.70714	0.32306
0.11	1.01060	0.02225	0.02202	0.61	1.33753	0.27086	0.20251	1.11	2.21317	0.71852	0.32466
0.12	1.01262	0.02521	0.02489	C.62	1.34910	0.27772	0.20585	1.12	2.23773	0.73001	0.32623
0.13	1.01481	0.02827	0.02786	C.63	1.36088	0.28465	0.20916	1.13	2.26261	0.74162	0.32777
0.14	1.01718	0.03144	0.03091	0.64	1.37289	0.29165	0.21244	1.14	2.28781	0.75335	0.32929
0.15	1.01973	0.03471	0.03404	C.65	1.38511	0.29873	0.21567	1.15	2.31333	0.76519	0.33078
0.16	1.02246	0.03808	0.03725	0.66	1.39755	0.30589	0.21888	1.16	2.33918	0.77716	0.33224
0.17	1.02536	0.04155	0.04052	C.67	1.41021	0.31312	0.22204	1.17	2.36536	0.78925	0.33367
0.18	1.02844	0.04511	0.04386	0.68	1.42310	0.32044	0.22517	1.18	2.39188	0.80146	0.33508
0.19	1.03170	0.04875	0.04726	C.69	1.43621	0.32783	0.22826	1.19	2.41873	0.81380	0.33646
0.20	1.03514	0.05249	0.05071	0.70	1.44954	0.33530	0.23131	1.20	2.44592	0.82626	0.33781
0.21	1.03875	0.05631	0.05421	0.71	1.46311	0.34285	0.23433	1.21	2.47345	0.83886	0.33914
0.22	1.04255	0.06022	0.05776	0.72	1.47690	0.35048	0.23731	1.22	2.50133	0.85158	0.34045
0.23	1.04653	0.06421	0.06136	0.73	1.49092	0.35819	0.24025	1.23	2.52955	0.86443	0.34173
C.24	1.05068	0.06828	0.06499	0.74	1.50517	0.36598	0.24315	1.24	2.55813	0.87741	0.34299
0.25	1.05502	0.07244	0.06866	0.75	1.51966	0.37386	0.24601	1.25	2.58707	0.89052	0.34422
C.26	1.05954	0.07667	0.07236	0.76	1.53439	0.38181	0.24884	1.26	2.61636	0.90377	0.34543
0.27	1.06424	0.08098	0.07609	0.77	1.54935	0.38985	0.25162	1.27	2.64601	0.91715	0.34662
0.28	1.06912	0.08536	0.07984	0.78	1.56455	0.39798	0.25437	1.28	2.67603	0.93068	0.34778
0.29	1.07419	0.08982	0.08362	0.79	1.57999	0.40618	0.25708	1.29	2.70642	0.94434	0.34892
C.30	1.07944	0.09436	0.08742	0.80	1.59567	0.41448	0.25975	1.30	2.73718	0.95814	0.35004
0.31	1.08488	0.09898	0.09123	0.81	1.61159	0.42286	0.26239	1.31	2.76831	0.97208	0.35114
0.32	1.09050	0.10366	0.09506	0.82	1.62777	0.43133	0.26498	1.32	2.79983	0.98616	0.35222
0.33	1.09630	0.10842	0.09890	0.83	1.64419	0.43988	0.26754	1.33	2.83173	1.00039	0.35328
0.34	1.10229	0.11326	0.10275	0.84	1.66086	0.44852	0.27005	1.34	2.86401	1.01477	0.35432
C.35	1.10847	0.11816	0.10660	C.85	1.67778	0.45725	0.27254	1.35	2.89669	1.02929	0.35533
0.36	1.11484	0.12314	0.11046	0.86	1.69496	0.46608	0.27498	1.36	2.92975	1.04396	0.35633
0.37	1.12139	0.12819	0.11432	0.87	1.71239	0.47499	0.27738	1.37	2.96322	1.05878	0.35731
0.38	1.12813	0.13332	0.11818	0.88	1.73008	0.48399	0.27975	1.38	2.99709	1.07376	0.35827
C.39	1.13507	0.13851	0.12203	0.89	1.74803	0.49309	0.28208	1.39	3.03136	1.08889	0.35921
0.40	1.14219	0.14378	0.12588	0.90	1.76624	0.50228	0.28438	1.40	3.06605	1.10417	0.36013
0.41	1.14951	0.14911	0.12972	C.91	1.78471	0.51157	0.28664	1.41	3.10114	1.11962	0.36103
0.42	1.15701	0.15452	0.13355	0.92	1.80345	0.52095	0.28886	1.42	3.13666	1.13522	0.36192
0.43	1.16472	0.16000	0.13737	0.93	1.82246	0.53042	0.29105	1.43	3.17259	1.15098	0.36279
0.44	1.17261	0.16555	0.14118	0.94	1.84174	0.53999	0.29320	1.44	3.20895	1.16691	0.36364
0.45	1.18070	0.17117	0.14497	C.95	1.86130	0.54966	0.29531	1.45	3.24574	1.18300	0.36448
0.46	1.18899	0.17686	0.14875	C.96	1.88112	0.55943	0.29739	1.46	3.28297	1.19925	0.36530
0.47	1.19747	0.18263	0.15251	C.97	1.90123	0.56930	0.29944	1.47	3.32063	1.21568	0.36610
C.48	1.20615	0.18846	0.15625	0.98	1.92161	0.57927	0.30145	1.48	3.35874	1.23227	0.36688
0.49	1.21503	0.19436	0.15997	0.99	1.94228	0.58934	0.30343	1.49	3.39729	1.24903	0.36766
C.50	1.22412	0.20034	0.16366	1.00	1.96323	0.59952	0.30537	1.50	3.43629	1.26597	0.36841

TABLE 10A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 2/7$ and x from 0.00 to 1.50.

$\alpha = 2/7$

x	$F_{2/7}(x)$	$H_{5/7}(x)$	$T_{2/7}(x)$
1.50	3.43629	1.26597	0.36841
1.51	3.47575	1.28309	0.36915
1.52	3.51567	1.30038	0.36988
1.53	3.55606	1.31785	0.37059
1.54	3.59691	1.33550	0.37129
1.55	3.63824	1.35333	0.37197
1.56	3.68005	1.37135	0.37264
1.57	3.72234	1.38956	0.37330
1.58	3.76511	1.40795	0.37395
1.59	3.80839	1.42654	0.37458
1.60	3.85216	1.44531	0.37520
1.61	3.89643	1.46429	0.37580
1.62	3.94121	1.48346	0.37640
1.63	3.98651	1.50283	0.37698
1.64	4.03232	1.52240	0.37755
1.65	4.07865	1.54217	0.37811
1.66	4.12552	1.56216	0.37866
1.67	4.17292	1.58234	0.37919
1.68	4.22086	1.60274	0.37972
1.69	4.26934	1.62336	0.38024
1.70	4.31838	1.64418	0.38074
1.71	4.36797	1.66523	0.38124
1.72	4.41812	1.68649	0.38172
1.73	4.46884	1.70798	0.38220
1.74	4.52014	1.72969	0.38266
1.75	4.57201	1.75162	0.38312
1.76	4.62447	1.77379	0.38357
1.77	4.67752	1.79618	0.38400
1.78	4.73116	1.81882	0.38443
1.79	4.78541	1.84168	0.38485
1.80	4.84027	1.86479	0.38527
1.81	4.89574	1.88814	0.38567
1.82	4.95183	1.91173	0.38607
1.83	5.00856	1.93557	0.38645
1.84	5.06591	1.95966	0.38683
1.85	5.12391	1.98401	0.38721
1.86	5.18256	2.00860	0.38757
1.87	5.24186	2.03346	0.38793
1.88	5.30182	2.05858	0.38828
1.89	5.36245	2.08396	0.38862
1.90	5.42375	2.10960	0.38896
1.91	5.48573	2.13552	0.38929
1.92	5.54841	2.16170	0.38961
1.93	5.61177	2.18817	0.38992
1.94	5.67585	2.21490	0.39023
1.95	5.74063	2.24193	0.39054
1.96	5.80612	2.26923	0.39083
1.97	5.87235	2.29682	0.39112
1.98	5.93930	2.32470	0.39141
1.99	6.00700	2.35288	0.39169
2.00	6.07544	2.38135	0.39196

x	$F_{2/7}(x)$	$H_{5/7}(x)$	$T_{2/7}(x)$
2.0	6.07544	2.38135	0.39196
2.1	6.80269	2.68307	0.39441
2.2	7.61372	3.01814	0.39641
2.3	8.51765	3.39030	0.39803
2.4	9.52461	3.80370	0.39935
2.5	10.64589	4.26296	0.40043
2.6	11.89402	4.77319	0.40131
2.7	13.28291	5.34007	0.40203
2.8	14.82801	5.96989	0.40261
2.9	16.54648	6.66962	0.40308
3.0	18.45736	7.44701	0.40347
3.1	20.58178	8.31065	0.40379
3.2	22.94317	9.27007	0.40404
3.3	25.56756	10.33582	0.40426
3.4	28.48380	11.51961	0.40443
3.5	31.72390	12.83443	0.40457
3.6	35.32336	14.29469	0.40468
3.7	39.32155	15.91635	0.40477
3.8	43.76214	17.71712	0.40485
3.9	48.69354	19.71663	0.40491
4.0	54.16945	21.93665	0.40496
4.1	60.24938	24.40130	0.40501
4.2	66.99933	27.13734	0.40504
4.3	74.49248	30.17442	0.40507
4.4	82.80993	33.54542	0.40509
4.5	92.04161	37.28678	0.40511
4.6	102.28718	41.43889	0.40512
4.7	113.65714	46.04653	0.40514
4.8	126.27394	51.15932	0.40515
4.9	140.27331	56.83226	0.40515
5.0	155.80568	63.12631	0.40516
5.1	173.03779	70.10904	0.40517
5.2	192.15439	77.85530	0.40517
5.3	213.36024	86.44808	0.40517
5.4	236.88226	95.97931	0.40518
5.5	262.97188	106.55088	0.40518
5.6	291.90773	118.27569	0.40518
5.7	323.99854	131.27884	0.40518
5.8	359.58639	145.69894	0.40518
5.9	399.05030	161.68955	0.40519
6.0	442.81022	179.42086	0.40519

x	$F_{2/7}(x)$	$H_{5/7}(x)$	$T_{2/7}(x)$
6.0	442.81022	179.42086	0.40519
6.1	491.33142	199.08137	0.40519
6.2	545.12935	220.87995	0.40519
6.3	604.77509	245.04800	0.40519
6.4	670.90131	271.84186	0.40519
6.5	744.20885	301.54552	0.40519
6.6	825.47413	334.47357	0.40519
6.7	915.55721	370.97450	0.40519
6.8	1015.41081	411.43435	0.40519
6.9	1126.09024	456.28073	0.40519
7.0	1248.76448	505.98728	0.40519
7.1	1384.72833	561.07865	0.40519
7.2	1535.41592	622.13594	0.40519
7.3	1702.41573	689.80279	0.40519
7.4	1887.48712	764.79207	0.40519
7.5	2092.57865	847.89333	0.40519
7.6	2319.84844	939.98101	0.40519
7.7	2571.68659	1042.02357	0.40519
7.8	2850.74013	1155.09354	0.40519
7.9	3159.94055	1280.37876	0.40519
8.0	3502.53428	1419.19463	0.40519
8.1	3882.11651	1572.99791	0.40519
8.2	4302.66855	1743.40178	0.40519
8.3	4768.59922	1932.19265	0.40519
8.4	5284.79066	2141.34873	0.40519
8.5	5856.64912	2373.06056	0.40519
8.6	6490.16098	2629.75379	0.40519
8.7	7191.95501	2914.11433	0.40519
8.8	7969.37115	3229.11626	0.40519
8.9	8830.53666	3578.05267	0.40519
9.0	9784.45041	3964.56982	0.40519
9.1	10841.07625	4392.70497	0.40519
9.2	12011.66627	4866.92821	0.40519
9.3	13307.77514	5392.18883	0.40519
9.4	14743.58670	5973.96657	0.40519
9.5	16333.85403	6618.32837	0.40519
9.6	18095.15451	7331.99124	0.40519
9.7	20045.84147	8122.39178	0.40519
9.8	22206.23412	8997.76315	0.40519
9.9	24598.82785	9967.22027	0.40519
10.0	27248.52692	11040.85413	0.40519

TABLE 10B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 2/7$ and x from 1.50 to 10.0.

$\alpha = 3/7$

x	$F_{3/7}(x)$	$H_{4/7}(x)$	$T_{3/7}(x)$
0.0	1.00000	0.0	0.0
0.01	1.00006	0.00410	0.00410
0.02	1.00023	0.00906	0.00906
0.03	1.00053	0.01441	0.01440
0.04	1.00093	0.02002	0.02000
0.05	1.00146	0.02584	0.02580
0.06	1.00210	0.03183	0.03176
0.07	1.00286	0.03797	0.03786
0.08	1.00374	0.04424	0.04408
0.09	1.00473	0.05063	0.05039
0.10	1.00584	0.05713	0.05679
0.11	1.00707	0.06372	0.06327
0.12	1.00841	0.07041	0.06982
0.13	1.00987	0.07719	0.07643
0.14	1.01145	0.08404	0.08309
0.15	1.01315	0.09098	0.08980
0.16	1.01497	0.09799	0.09655
0.17	1.01690	0.10508	0.10333
0.18	1.01895	0.11223	0.11015
0.19	1.02112	0.11946	0.11699
0.20	1.02342	0.12675	0.12385
0.21	1.02582	0.13410	0.13073
0.22	1.02835	0.14152	0.13762
0.23	1.03100	0.14900	0.14452
0.24	1.03377	0.15655	0.15143
0.25	1.03666	0.16415	0.15835
0.26	1.03967	0.17182	0.16526
0.27	1.04280	0.17954	0.17217
0.28	1.04605	0.18732	0.17908
0.29	1.04942	0.19516	0.18597
0.30	1.05291	0.20306	0.19286
0.31	1.05653	0.21102	0.19973
0.32	1.06027	0.21904	0.20658
0.33	1.06413	0.22711	0.21342
0.34	1.06812	0.23524	0.22024
0.35	1.07223	0.24343	0.22703
0.36	1.07646	0.25167	0.23380
0.37	1.08082	0.25998	0.24054
0.38	1.08530	0.26834	0.24725
0.39	1.08991	0.27676	0.25393
0.40	1.09465	0.28524	0.26058
0.41	1.09951	0.29378	0.26719
0.42	1.10450	0.30238	0.27377
0.43	1.10961	0.31104	0.28031
0.44	1.11486	0.31976	0.28681
0.45	1.12023	0.32853	0.29327
0.46	1.12574	0.33737	0.29969
0.47	1.13137	0.34627	0.30607
0.48	1.13713	0.35523	0.31240
0.49	1.14303	0.36426	0.31868
0.50	1.14905	0.37335	0.32492

x	$F_{3/7}(x)$	$H_{4/7}(x)$	$T_{3/7}(x)$
0.50	1.14905	0.37335	0.32492
0.51	1.15521	0.38250	0.33111
0.52	1.16150	0.39171	0.33725
0.53	1.16792	0.40099	0.34333
0.54	1.17448	0.41033	0.34937
0.55	1.16118	0.41974	0.35536
0.56	1.18801	0.42922	0.36129
0.57	1.19497	0.43876	0.36717
0.58	1.20208	0.44837	0.37300
0.59	1.20932	0.45805	0.37877
0.60	1.21670	0.46780	0.38449
0.61	1.22422	0.47762	0.39015
0.62	1.23188	0.48751	0.39575
0.63	1.23968	0.49748	0.40130
0.64	1.24762	0.50751	0.40678
0.65	1.25570	0.51762	0.41221
0.66	1.26393	0.52780	0.41759
0.67	1.27230	0.53806	0.42290
0.68	1.28082	0.54839	0.42815
0.69	1.28949	0.55880	0.43335
0.70	1.29830	0.56928	0.43849
0.71	1.30726	0.57985	0.44356
0.72	1.31636	0.59049	0.44858
0.73	1.32562	0.60122	0.45354
0.74	1.33503	0.61202	0.45843
0.75	1.34459	0.62291	0.46327
0.76	1.35430	0.63388	0.46805
0.77	1.36417	0.64494	0.47277
0.78	1.37419	0.65608	0.47743
0.79	1.38437	0.66730	0.48203
0.80	1.39470	0.67862	0.48657
0.81	1.40520	0.69002	0.49105
0.82	1.41585	0.70151	0.49547
0.83	1.42666	0.71309	0.49983
0.84	1.43764	0.72476	0.50414
0.85	1.44877	0.73653	0.50838
0.86	1.46007	0.74839	0.51257
0.87	1.47154	0.76034	0.51670
0.88	1.48317	0.77239	0.52077
0.89	1.49497	0.78453	0.52478
0.90	1.50693	0.79678	0.52874
0.91	1.51907	0.80912	0.53264
0.92	1.53138	0.82156	0.53648
0.93	1.54386	0.83411	0.54027
0.94	1.55651	0.84675	0.54401
0.95	1.56934	0.85950	0.54768
0.96	1.58235	0.87236	0.55131
0.97	1.59553	0.88532	0.55488
0.98	1.60869	0.89839	0.55839
0.99	1.62243	0.91157	0.56186
1.00	1.63616	0.92486	0.56526

x	$F_{3/7}(x)$	$H_{4/7}(x)$	$T_{3/7}(x)$
1.00	1.63616	0.92486	0.56526
1.01	1.65007	0.93826	0.56862
1.02	1.66416	0.95178	0.57193
1.03	1.67844	0.96541	0.57518
1.04	1.69291	0.97915	0.57838
1.05	1.70756	0.99301	0.58154
1.06	1.72241	1.00699	0.58464
1.07	1.73745	1.02109	0.58770
1.08	1.75268	1.03531	0.59070
1.09	1.76811	1.04965	0.59366
1.10	1.78374	1.06412	0.59657
1.11	1.79956	1.07871	0.59943
1.12	1.81559	1.09343	0.60224
1.13	1.83181	1.10827	0.60501
1.14	1.84824	1.12325	0.60774
1.15	1.86488	1.13836	0.61042
1.16	1.88172	1.15360	0.61305
1.17	1.89878	1.16897	0.61564
1.18	1.91604	1.18448	0.61819
1.19	1.93352	1.20013	0.62070
1.20	1.95121	1.21591	0.62316
1.21	1.96912	1.23184	0.62558
1.22	1.98724	1.24791	0.62796
1.23	2.00559	1.26412	0.63030
1.24	2.02416	1.28048	0.63260
1.25	2.04295	1.29698	0.63486
1.26	2.06196	1.31363	0.63708
1.27	2.08121	1.33044	0.63926
1.28	2.10068	1.34739	0.64141
1.29	2.12039	1.36450	0.64351
1.30	2.14033	1.38177	0.64558
1.31	2.16051	1.39919	0.64762
1.32	2.18093	1.41677	0.64962
1.33	2.20158	1.43451	0.65158
1.34	2.22248	1.45241	0.65351
1.35	2.24362	1.47048	0.65541
1.36	2.26501	1.48872	0.65727
1.37	2.28665	1.50712	0.65910
1.38	2.30854	1.52569	0.66089
1.39	2.33068	1.54444	0.66265
1.40	2.35308	1.56336	0.66439
1.41	2.37574	1.58245	0.66609
1.42	2.39866	1.60172	0.66776
1.43	2.42184	1.62118	0.66940
1.44	2.44529	1.64081	0.67101
1.45	2.46901	1.66063	0.67259
1.46	2.49299	1.68063	0.67414
1.47	2.51725	1.70082	0.67567
1.48	2.54178	1.72120	0.67716
1.49	2.56660	1.74177	0.67863
1.50	2.59169	1.76254	0.68007

TABLE 11A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/7$ and x from 0.00 to 1.50.

$\alpha = 3/7$

x	$F_{3/7}(x)$	$H_{4/7}(x)$	$T_{3/7}(x)$
1.50	2.59169	1.76254	0.68007
1.51	2.61706	1.78350	0.68149
1.52	2.64273	1.80466	0.68288
1.53	2.66868	1.82602	0.68424
1.54	2.69492	1.84759	0.68558
1.55	2.72145	1.86936	0.68690
1.56	2.74828	1.89133	0.68819
1.57	2.77542	1.91352	0.68945
1.58	2.80285	1.93591	0.69069
1.55	2.83059	1.95852	0.69191
1.60	2.85864	1.98135	0.69311
1.61	2.88699	2.00440	0.69428
1.62	2.91567	2.02766	0.69544
1.63	2.94466	2.05115	0.69657
1.64	2.97397	2.07487	0.69768
1.65	3.00360	2.09881	0.69877
1.66	3.03356	2.12299	0.69983
1.67	3.06384	2.14739	C.70088
1.68	3.09446	2.17204	0.70191
1.69	3.12542	2.19692	C.70292
1.7C	3.15672	2.22204	0.70391
1.71	3.18835	2.24741	0.70488
1.72	3.22033	2.27302	0.70583
1.73	3.25267	2.29868	0.70677
1.74	3.28535	2.32499	0.70769
1.75	3.31839	2.35136	0.70858
1.76	3.35178	2.37798	0.70947
1.77	3.38555	2.40486	0.71033
1.78	3.41967	2.43201	0.71118
1.79	3.45417	2.45942	0.71201
1.80	3.48904	2.48710	0.71283
1.81	3.52428	2.51504	0.71363
1.82	3.55991	2.54327	0.71442
1.83	3.59592	2.57177	0.71519
1.84	3.63231	2.60054	0.71595
1.85	3.66910	2.62960	0.71669
1.86	3.70629	2.65895	0.71742
1.87	3.74387	2.68859	0.71813
1.88	3.78186	2.71851	0.71883
1.89	3.82025	2.74873	0.71952
1.90	3.85906	2.77925	0.72019
1.91	3.89828	2.81007	0.72085
1.92	3.93792	2.84120	0.72150
1.93	3.97799	2.87263	0.72213
1.94	4.01848	2.90437	0.72275
1.95	4.0594C	2.93643	0.72336
1.56	4.10076	2.96880	0.72396
1.97	4.14256	3.00149	0.72455
1.98	4.18480	3.03451	0.72513
1.95	4.22750	3.06786	0.72569
2.00	4.27065	3.10153	C.72624

x	$F_{3/7}(x)$	$H_{4/7}(x)$	$T_{3/7}(x)$
2.0	4.27065	3.10153	0.72624
2.1	4.72807	3.45728	0.73122
2.2	5.23611	3.85017	0.73531
2.3	5.80002	4.28427	0.73866
2.4	6.42568	4.76410	0.74142
2.5	7.11957	5.29460	0.74367
2.6	7.88889	5.88129	0.74552
2.7	8.74163	6.53024	0.74703
2.8	9.68661	7.24815	0.74827
2.9	10.73361	8.04247	0.74928
3.0	11.89347	8.92139	C.75011
3.1	13.17819	9.89402	0.75079
3.2	14.60103	1C.97038	0.75134
3.3	16.17669	12.16159	0.75180
3.4	17.92145	13.47996	0.75217
3.5	19.85328	14.93907	0.75247
3.6	21.99212	16.55396	0.75272
3.7	24.36000	18.34129	0.75293
3.8	26.98131	20.31944	0.75309
3.9	29.88304	22.50879	0.75323
4.0	33.09505	24.93186	0.75334
4.1	36.65035	27.61356	0.75343
4.2	40.58552	30.58148	0.75351
4.3	44.94097	33.86609	0.75357
4.4	49.76144	37.50113	0.75362
4.5	55.09643	41.52393	0.75366
4.6	61.00067	45.97576	0.75369
4.7	67.53473	50.90229	0.75372
4.8	74.76562	56.35404	0.75374
4.9	82.76745	62.38688	0.75376
5.0	91.62221	69.06263	0.75378
5.1	101.42059	76.44966	0.75379
5.2	112.26292	84.62362	0.75380
5.3	124.26019	93.66816	0.75381
5.4	137.53514	103.67584	0.75381
5.5	152.22357	114.74901	0.75382
5.6	168.47567	127.00092	0.75382
5.7	186.45759	140.55680	0.75383
5.8	206.35310	155.55520	0.75383
5.9	228.36545	172.14934	0.75383
6.0	252.71948	190.50872	0.75383

x	$F_{3/7}(x)$	$H_{4/7}(x)$	$T_{3/7}(x)$
6.0	252.71948	190.50872	0.75383
6.1	279.66387	210.82079	0.75384
6.2	309.47366	233.29292	0.75384
6.3	342.45309	258.15445	0.75384
6.4	378.93865	285.65902	0.75384
6.5	419.30250	316.08721	0.75384
6.6	463.95628	349.74932	0.75384
6.7	513.35525	386.98855	C.75384
6.8	568.00295	428.18449	0.75384
6.9	628.45630	473.75698	0.75384
7.0	695.33122	524.17032	0.75384
7.1	769.30895	579.93806	0.75384
7.2	851.14290	641.62815	0.75384
7.3	941.66633	709.86875	0.75384
7.4	1041.80078	785.35455	0.75384
7.5	1152.56546	868.85388	0.75384
7.6	1275.08753	961.21644	0.75384
7.7	1410.61358	1063.38196	0.75384
7.8	1560.52225	1176.38974	0.75384
7.9	1726.33822	1301.38913	0.75384
8.0	1909.74766	1439.65124	0.75384
8.1	2112.61531	1592.58180	0.75384
8.2	2337.00342	1761.73547	0.75384
8.3	2585.19263	1948.83137	0.75384
8.4	2859.70505	2155.77090	0.75384
8.5	3163.32988	2384.65663	0.75384
8.6	3499.15164	2637.81382	0.75384
8.7	3870.58138	2917.81387	0.75384
8.8	4281.39132	3227.50044	0.75384
8.9	4735.75299	3570.01821	0.75384
9.0	5238.27950	3948.84475	0.75384
9.1	5794.07225	4367.82572	0.75384
9.2	6408.77262	4831.21383	0.75384
9.3	7088.61905	5343.71190	0.75384
9.4	7840.51021	591C.52045	0.75384
9.5	8672.07486	6537.39037	0.75384
9.6	9591.74906	7230.68112	0.75384
9.7	10608.86152	7997.42512	0.75384
9.8	11733.72807	8845.39888	0.75384
9.9	12977.75603	9783.20173	0.75384
10.0	14353.55964	10820.34285	0.75384

TABLE 11B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/7$ and x from 1.50 to 10.0.

$\alpha = 4/7$

x	$F_{4/7}(x)$	$F_{3/7}(x)$	$T_{4/7}(x)$	x	$F_{4/7}(x)$	$H_{3/7}(x)$	$T_{4/7}(x)$	x	$F_{4/7}(x)$	$H_{3/7}(x)$	$T_{4/7}(x)$
0.0	1.00000	0.0	0.0	0.50	1.11157	0.74260	0.66807	1.00	1.47345	1.52541	1.03527
0.01	1.00004	0.02487	0.02487	0.51	1.11617	0.75663	0.67788	1.01	1.48373	1.54354	1.04031
0.02	1.00019	0.04505	0.04504	0.52	1.12087	0.77069	0.68758	1.02	1.49414	1.56180	1.04528
0.03	1.00039	0.06378	0.06376	0.53	1.12566	0.78479	0.69718	1.03	1.50468	1.58018	1.05018
0.04	1.00070	0.08163	0.08157	0.54	1.13056	0.79893	0.70666	1.04	1.51537	1.59870	1.05499
0.05	1.00109	0.09885	0.09874	0.55	1.13556	0.81311	0.71604	1.05	1.52619	1.61736	1.05974
0.06	1.00158	0.11559	0.11541	0.56	1.14066	0.82734	0.72532	1.06	1.53714	1.63615	1.06441
0.07	1.00214	0.13195	0.13167	0.57	1.14586	0.84161	0.73448	1.07	1.54824	1.65508	1.06901
0.08	1.00280	0.14799	0.14758	0.58	1.15116	0.85593	0.74354	1.08	1.55947	1.67415	1.07353
0.09	1.00355	0.16376	0.16318	0.59	1.15656	0.87030	0.75249	1.09	1.57085	1.69336	1.07799
0.10	1.00438	0.17929	0.17851	0.60	1.16206	0.88473	0.76134	1.10	1.58237	1.71271	1.08237
0.11	1.00530	0.19463	0.19360	0.61	1.16767	0.89920	0.77008	1.11	1.59403	1.73221	1.08669
0.12	1.00631	0.20978	0.20847	0.62	1.17338	0.91374	0.77872	1.12	1.60584	1.75186	1.09093
0.13	1.00740	0.22478	0.22313	0.63	1.17920	0.92833	0.78726	1.13	1.61779	1.77166	1.09511
0.14	1.00859	0.23963	0.23759	0.64	1.18512	0.94298	0.79569	1.14	1.62989	1.79161	1.09923
0.15	1.00986	0.25436	0.25188	0.65	1.19114	0.95769	0.80401	1.15	1.64213	1.81172	1.10327
0.16	1.01122	0.26898	0.26599	0.66	1.19727	0.97247	0.81224	1.16	1.65453	1.83198	1.10725
0.17	1.01267	0.28348	0.27994	0.67	1.20351	0.98731	0.82036	1.17	1.66707	1.85240	1.11117
0.18	1.01421	0.29790	0.29373	0.68	1.20985	1.00222	0.82838	1.18	1.67977	1.87298	1.11502
0.19	1.01584	0.31223	0.30737	0.69	1.21630	1.01720	0.83630	1.19	1.69262	1.89372	1.11881
0.20	1.01756	0.32649	0.32086	0.70	1.22286	1.03224	0.84412	1.20	1.70562	1.91463	1.12254
0.21	1.01936	0.34068	0.33421	0.71	1.22953	1.04736	0.85184	1.21	1.71877	1.93570	1.12621
0.22	1.02126	0.35480	0.34742	0.72	1.23631	1.06256	0.85946	1.22	1.73209	1.95694	1.12982
0.23	1.02324	0.36887	0.36049	0.73	1.24320	1.07783	0.86698	1.23	1.74556	1.97835	1.13336
0.24	1.02532	0.38289	0.37343	0.74	1.25020	1.09318	0.87440	1.24	1.75919	1.99994	1.13685
0.25	1.02748	0.39686	0.38625	0.75	1.25731	1.10861	0.88173	1.25	1.77298	2.02170	1.14028
0.26	1.02973	0.41079	0.39893	0.76	1.26453	1.12411	0.88896	1.26	1.78693	2.04364	1.14366
0.27	1.03208	0.42469	0.41149	0.77	1.27186	1.13971	0.89609	1.27	1.80105	2.06575	1.14697
0.28	1.03451	0.43856	0.42393	0.78	1.27931	1.15538	0.90313	1.28	1.81532	2.08805	1.15024
0.29	1.03704	0.45240	0.43624	0.79	1.28688	1.17115	0.91007	1.29	1.82977	2.11053	1.15344
0.30	1.03966	0.46622	0.44843	0.80	1.29455	1.18700	0.91692	1.30	1.84438	2.13320	1.15660
0.31	1.04237	0.48001	0.46050	0.81	1.30235	1.20294	0.92367	1.31	1.85916	2.15606	1.15970
0.32	1.04517	0.49380	0.47246	0.82	1.31026	1.21898	0.93034	1.32	1.87411	2.17910	1.16274
0.33	1.04806	0.50757	0.48429	0.83	1.31828	1.23511	0.93691	1.33	1.88923	2.20234	1.16574
0.34	1.05104	0.52133	0.49601	0.84	1.32643	1.25133	0.94339	1.34	1.90452	2.22578	1.16868
0.35	1.05412	0.53508	0.50761	0.85	1.33469	1.26766	0.94977	1.35	1.91999	2.24941	1.17158
0.36	1.05729	0.54884	0.51910	0.86	1.34307	1.28408	0.95607	1.36	1.93563	2.27324	1.17442
0.37	1.06055	0.56259	0.53047	0.87	1.35158	1.30060	0.96228	1.37	1.95145	2.29728	1.17722
0.38	1.06390	0.57635	0.54173	0.88	1.36020	1.31722	0.96840	1.38	1.96744	2.32152	1.17997
0.39	1.06735	0.59011	0.55287	0.89	1.36895	1.33395	0.97444	1.39	1.98362	2.34596	1.18267
0.40	1.07090	0.60388	0.56390	0.90	1.37762	1.35079	0.98039	1.40	1.99998	2.37062	1.18532
0.41	1.07453	0.61766	0.57482	0.91	1.38681	1.36774	0.98625	1.41	2.01652	2.39549	1.18793
0.42	1.07826	0.63146	0.58562	0.92	1.39593	1.38479	0.99202	1.42	2.03325	2.42057	1.19049
0.43	1.08209	0.64527	0.59632	0.93	1.40517	1.40196	0.99771	1.43	2.05017	2.44587	1.19301
0.44	1.08601	0.65910	0.60690	0.94	1.41454	1.41924	1.00332	1.44	2.06727	2.47138	1.19548
0.45	1.09003	0.67295	0.61737	0.95	1.42403	1.43663	1.00885	1.45	2.08456	2.49712	1.19791
0.46	1.09414	0.68683	0.62773	0.96	1.43366	1.45415	1.01429	1.46	2.10204	2.52308	1.20030
0.47	1.09835	0.70073	0.63798	0.97	1.44341	1.47178	1.01966	1.47	2.11972	2.54928	1.20265
0.48	1.10266	0.71466	0.64812	0.98	1.45329	1.48953	1.02494	1.48	2.13759	2.57569	1.20495
0.49	1.10707	0.72861	0.65815	0.99	1.46330	1.50741	1.03014	1.49	2.15566	2.60235	1.20722
0.50	1.11157	0.74260	0.66807	1.00	1.47345	1.52541	1.03527	1.50	2.17392	2.62923	1.20944

TABLE 12A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 4/7$ and x from 0.00 to 1.50.

$\alpha = 4/7$

x	$F_{4/7}(x)$	$H_{3/7}(x)$	$T_{4/7}(x)$
1.50	2.17392	2.62923	1.20944
1.51	2.19239	2.65636	1.21163
1.52	2.21105	2.68372	1.21377
1.53	2.22992	2.71132	1.21588
1.54	2.24900	2.73917	1.21795
1.55	2.26828	2.76727	1.21999
1.56	2.28777	2.79562	1.22198
1.57	2.30747	2.82423	1.22395
1.58	2.32739	2.85309	1.22587
1.59	2.34752	2.88220	1.22777
1.60	2.36787	2.91158	1.22962
1.61	2.38843	2.94123	1.23145
1.62	2.40922	2.97114	1.23324
1.63	2.43023	3.00133	1.23500
1.64	2.45146	3.03178	1.23673
1.65	2.47292	3.06252	1.23842
1.66	2.49460	3.09353	1.24009
1.67	2.51652	3.12483	1.24172
1.68	2.53867	3.15641	1.24333
1.69	2.56106	3.18828	1.24491
1.70	2.58368	3.22044	1.24645
1.71	2.60654	3.25289	1.24797
1.72	2.62965	3.28565	1.24946
1.73	2.65300	3.31871	1.25093
1.74	2.67659	3.35207	1.25237
1.75	2.70043	3.38573	1.25378
1.76	2.72452	3.41971	1.25516
1.77	2.74887	3.45401	1.25652
1.78	2.77347	3.48862	1.25785
1.79	2.79832	3.52355	1.25916
1.80	2.82344	3.55880	1.26045
1.81	2.84882	3.59439	1.26171
1.82	2.87447	3.63030	1.26295
1.83	2.90038	3.66655	1.26416
1.84	2.92656	3.70314	1.26536
1.85	2.95301	3.74007	1.26653
1.86	2.97974	3.77735	1.26768
1.87	3.00675	3.81497	1.26880
1.88	3.03403	3.85295	1.26991
1.89	3.06160	3.89128	1.27100
1.90	3.08945	3.92997	1.27206
1.91	3.11760	3.96903	1.27311
1.92	3.14603	4.00846	1.27413
1.93	3.17475	4.04825	1.27514
1.94	3.20377	4.08842	1.27613
1.95	3.23309	4.12897	1.27710
1.96	3.26272	4.16991	1.27805
1.97	3.29264	4.21123	1.27898
1.98	3.32288	4.25294	1.27990
1.99	3.35342	4.29504	1.28079
2.00	3.38428	4.33755	1.28168

x	$F_{4/7}(x)$	$H_{3/7}(x)$	$T_{4/7}(x)$
2.0	3.38428	4.33755	1.28168
2.1	3.71076	4.78548	1.28962
2.2	4.07203	5.27811	1.29619
2.3	4.47160	5.82021	1.30159
2.4	4.91330	6.41702	1.30605
2.5	5.40141	7.07432	1.30972
2.6	5.94065	7.79848	1.31273
2.7	6.53623	8.59651	1.31521
2.8	7.19391	9.47614	1.31723
2.9	7.92006	10.44590	1.31892
3.0	8.72171	11.51518	1.32029
3.1	9.60664	12.69435	1.32141
3.2	10.58343	13.99486	1.32234
3.3	11.66155	15.42934	1.32309
3.4	12.85148	17.01171	1.32372
3.5	14.16478	18.75735	1.32422
3.6	15.61420	20.68323	1.32464
3.7	17.21385	22.80807	1.32498
3.8	18.97929	25.15257	1.32526
3.9	20.92769	27.73953	1.32549
4.0	23.07805	30.59416	1.32568
4.1	25.45130	33.74426	1.32584
4.2	28.07058	37.22054	1.32596
4.3	30.96144	41.05691	1.32607
4.4	34.15206	45.29079	1.32615
4.5	37.67360	49.96350	1.32622
4.6	41.56043	55.12066	1.32628
4.7	45.85052	60.81264	1.32632
4.8	50.58579	67.09506	1.32636
4.9	55.81251	74.02933	1.32639
5.0	61.58180	81.68325	1.32642
5.1	67.95006	90.13169	1.32644
5.2	74.97967	99.45731	1.32646
5.3	82.73938	109.75138	1.32647
5.4	91.30517	121.11471	1.32648
5.5	100.76094	133.65857	1.32649
5.6	111.19932	147.50587	1.32650
5.7	122.72263	162.79230	1.32651
5.8	135.44380	179.66772	1.32651
5.9	149.48759	198.29760	1.32652
6.0	164.99174	218.86467	1.32652

x	$F_{4/7}(x)$	$H_{3/7}(x)$	$T_{4/7}(x)$
6.0	164.99174	218.86467	1.32652
6.1	182.10835	241.57070	1.32652
6.2	201.00541	266.63852	1.32652
6.3	221.86839	294.31420	1.32653
6.4	244.90215	324.86946	1.32653
6.5	270.33290	358.60439	1.32653
6.6	298.41044	395.85037	1.32653
6.7	329.41064	436.97335	1.32653
6.8	363.63818	482.37748	1.32653
6.9	401.42949	532.50907	1.32653
7.0	443.15614	587.86102	1.32653
7.1	489.22847	648.97766	1.32653
7.2	540.09905	716.46013	1.32653
7.3	596.27016	790.97233	1.32653
7.4	658.29272	873.24746	1.32653
7.5	726.77774	964.09527	1.32653
7.6	802.39937	1064.41005	1.32653
7.7	885.90216	1175.17944	1.32653
7.8	978.10839	1297.49424	1.32653
7.9	1079.92621	1432.55915	1.32653
8.0	1192.35862	1581.70466	1.32653
8.1	1316.51334	1746.40024	1.32653
8.2	1453.61383	1928.26881	1.32653
8.3	1605.01131	2129.10284	1.32653
8.4	1772.19815	2350.88200	1.32653
8.5	1956.82264	2595.79281	1.32653
8.6	2160.70525	2866.25017	1.32653
8.7	2385.85663	3164.92129	1.32653
8.8	2634.49754	3494.75209	1.32653
8.9	2909.08076	3858.99625	1.32653
9.0	3212.31536	4261.24747	1.32653
9.1	3547.19354	4705.47498	1.32653
9.2	3917.02016	5196.06282	1.32653
9.3	4325.44549	5737.85318	1.32653
9.4	4776.50131	6336.19435	1.32653
9.5	5274.64079	6996.99364	1.32653
9.6	5824.78258	7726.77579	1.32653
9.7	6432.35948	8532.74759	1.32653
9.8	7103.37220	9422.86922	1.32653
9.9	7844.44879	10405.93299	1.32653
10.0	8662.91020	11491.65041	1.32653

TABLE 12B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 4/7$ and x from 1.50 to 10.0.

$\alpha = 5/7$

x	$F_{5/7}(x)$	$H_{2/7}(x)$	$T_{5/7}(x)$	x	$F_{5/7}(x)$	$H_{2/7}(x)$	$T_{5/7}(x)$	x	$F_{5/7}(x)$	$H_{2/7}(x)$	$T_{5/7}(x)$
0.0	1.00000	0.0	0.0	0.50	1.08911	1.66313	1.52705	1.00	1.37632	2.83900	2.06275
0.01	1.00004	0.16951	0.16951	0.51	1.09278	1.68529	1.54221	1.01	1.38444	2.86550	2.06980
0.02	1.00014	0.25191	0.25187	0.52	1.09652	1.70744	1.55714	1.02	1.39266	2.89219	2.07673
0.03	1.00032	0.31762	0.31752	0.53	1.10035	1.72957	1.57184	1.03	1.40099	2.91905	2.08356
0.04	1.00056	0.37442	0.37421	0.54	1.10425	1.75170	1.58632	1.04	1.40943	2.94609	2.09027
0.05	1.00088	0.42542	0.42505	0.55	1.10823	1.77382	1.60059	1.05	1.41797	2.97331	2.09688
0.06	1.00126	0.47223	0.47164	0.56	1.11229	1.79596	1.61464	1.06	1.42661	3.00072	2.10339
0.07	1.00172	0.51585	0.51496	0.57	1.11644	1.81810	1.62849	1.07	1.43537	3.02831	2.10978
0.08	1.00224	0.55691	0.55567	0.58	1.12066	1.84026	1.64212	1.08	1.44423	3.05610	2.11608
0.09	1.00284	0.59588	0.59419	0.59	1.12496	1.86244	1.65556	1.09	1.45320	3.08408	2.12227
0.10	1.00350	0.63309	0.63088	0.60	1.12934	1.88464	1.66879	1.10	1.46228	3.11227	2.12836
0.11	1.00424	0.66880	0.66598	0.61	1.13381	1.90687	1.68183	1.11	1.47147	3.14065	2.13436
0.12	1.00505	0.70321	0.69968	0.62	1.13836	1.92914	1.69467	1.12	1.48078	3.16924	2.14025
0.13	1.00592	0.73648	0.73214	0.63	1.14298	1.95144	1.70732	1.13	1.49019	3.19803	2.14605
0.14	1.00687	0.76874	0.76349	0.64	1.14770	1.97379	1.71979	1.14	1.49972	3.22703	2.15175
0.15	1.00789	0.80010	0.79384	0.65	1.15249	1.99619	1.73207	1.15	1.50936	3.25625	2.15737
0.16	1.00898	0.83066	0.82327	0.66	1.15737	2.01864	1.74416	1.16	1.51912	3.28568	2.16288
0.17	1.01014	0.86049	0.85185	0.67	1.16233	2.04114	1.75608	1.17	1.52900	3.31534	2.16831
0.18	1.01137	0.88966	0.87966	0.68	1.16737	2.06371	1.76782	1.18	1.53898	3.34521	2.17365
0.19	1.01267	0.91824	0.90675	0.69	1.17251	2.08634	1.77938	1.19	1.54909	3.37531	2.17890
0.20	1.01404	0.94626	0.93316	0.70	1.17772	2.10903	1.79078	1.20	1.55932	3.40564	2.18406
0.21	1.01548	0.97379	0.95894	0.71	1.18302	2.13180	1.80200	1.21	1.56966	3.43621	2.18914
0.22	1.01700	1.00086	0.98413	0.72	1.18841	2.15465	1.81305	1.22	1.58013	3.46700	2.19413
0.23	1.01859	1.02750	1.00875	0.73	1.19368	2.17757	1.82394	1.23	1.59071	3.49804	2.19904
0.24	1.02024	1.05375	1.03284	0.74	1.19944	2.20057	1.83466	1.24	1.60142	3.52931	2.20386
0.25	1.02197	1.07964	1.05643	0.75	1.20509	2.22367	1.84523	1.25	1.61225	3.56083	2.20861
0.26	1.02378	1.10520	1.07954	0.76	1.21083	2.24685	1.85563	1.26	1.62321	3.59260	2.21328
0.27	1.02565	1.13045	1.10218	0.77	1.21665	2.27013	1.86588	1.27	1.63428	3.62462	2.21786
0.28	1.02760	1.15542	1.12439	0.78	1.22256	2.29350	1.87597	1.28	1.64549	3.65689	2.22237
0.29	1.02962	1.18012	1.14618	0.79	1.22857	2.31697	1.88591	1.29	1.65682	3.68942	2.22681
0.30	1.03171	1.20458	1.16756	0.80	1.23466	2.34055	1.89570	1.30	1.66828	3.72221	2.23117
0.31	1.03387	1.22880	1.18855	0.81	1.24084	2.36424	1.90535	1.31	1.67987	3.75527	2.23545
0.32	1.03611	1.25282	1.20916	0.82	1.24712	2.38803	1.91484	1.32	1.69159	3.78859	2.23966
0.33	1.03842	1.27664	1.22941	0.83	1.25349	2.41194	1.92419	1.33	1.70344	3.82218	2.24380
0.34	1.04080	1.30029	1.24931	0.84	1.25994	2.43597	1.93340	1.34	1.71542	3.85605	2.24787
0.35	1.04326	1.32376	1.26887	0.85	1.26650	2.46012	1.94246	1.35	1.72753	3.89019	2.25187
0.36	1.04579	1.34708	1.28810	0.86	1.27314	2.48439	1.95139	1.36	1.73978	3.92461	2.25580
0.37	1.04840	1.37026	1.30701	0.87	1.27988	2.50879	1.96018	1.37	1.75217	3.95931	2.25967
0.38	1.05107	1.39331	1.32560	0.88	1.28671	2.53332	1.96883	1.38	1.76469	3.99431	2.26347
0.39	1.05383	1.41624	1.34390	0.89	1.29364	2.55799	1.97735	1.39	1.77734	4.02959	2.26720
0.40	1.05666	1.43905	1.36189	0.90	1.30067	2.58279	1.98574	1.40	1.79014	4.06517	2.27087
0.41	1.05956	1.46177	1.37960	0.91	1.30779	2.60773	1.99400	1.41	1.80307	4.10104	2.27447
0.42	1.06254	1.48440	1.39703	0.92	1.31500	2.63281	2.00213	1.42	1.81615	4.13721	2.27801
0.43	1.06559	1.50694	1.41418	0.93	1.32232	2.65804	2.01013	1.43	1.82937	4.17369	2.28149
0.44	1.06872	1.52942	1.43107	0.94	1.32973	2.68342	2.01801	1.44	1.84273	4.21048	2.28491
0.45	1.07193	1.55182	1.44769	0.95	1.33725	2.70895	2.02577	1.45	1.85624	4.24757	2.28827
0.46	1.07521	1.57417	1.46406	0.96	1.34486	2.73464	2.03340	1.46	1.86989	4.28499	2.29158
0.47	1.07857	1.59647	1.48017	0.97	1.35257	2.76048	2.04091	1.47	1.88368	4.32272	2.29482
0.48	1.08200	1.61872	1.49604	0.98	1.36039	2.78649	2.04831	1.48	1.89763	4.36077	2.29801
0.49	1.08552	1.64094	1.51167	0.99	1.36830	2.81266	2.05558	1.49	1.91173	4.39914	2.30114
0.50	1.08911	1.66313	1.52705	1.00	1.37632	2.83900	2.06275	1.50	1.92597	4.43785	2.30422

TABLE 13A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/7$ and x from 0.00 to 1.50.

$\alpha = 5/7$

x	$F_{5/7}(x)$	$H_{2/7}(x)$	$T_{5/7}(x)$
1.50	1.92597	4.43785	2.30422
1.51	1.94037	4.47689	2.30724
1.52	1.95492	4.51627	2.31021
1.53	1.96962	4.55598	2.31313
1.54	1.98448	4.59604	2.31599
1.55	1.99950	4.63645	2.31881
1.56	2.01467	4.67721	2.32157
1.57	2.03001	4.71832	2.32429
1.58	2.04550	4.75979	2.32696
1.59	2.06116	4.80163	2.32958
1.60	2.07698	4.84383	2.33215
1.61	2.09297	4.88640	2.33468
1.62	2.10912	4.92935	2.33716
1.63	2.12544	4.97268	2.33960
1.64	2.14193	5.01639	2.34199
1.65	2.15859	5.06049	2.34435
1.66	2.17543	5.10497	2.34665
1.67	2.19243	5.14986	2.34892
1.68	2.20962	5.19514	2.35115
1.69	2.22698	5.24082	2.35334
1.70	2.24451	5.28692	2.35548
1.71	2.26223	5.33342	2.35759
1.72	2.28013	5.38035	2.35966
1.73	2.29821	5.42769	2.36170
1.74	2.31648	5.47546	2.36369
1.75	2.33494	5.52365	2.36565
1.76	2.35358	5.57228	2.36758
1.77	2.37241	5.62135	2.36947
1.78	2.39143	5.67086	2.37132
1.79	2.41065	5.72082	2.37314
1.80	2.43006	5.77123	2.37493
1.81	2.44967	5.82210	2.37669
1.82	2.46948	5.87343	2.37841
1.83	2.48948	5.92522	2.38010
1.84	2.50969	5.97749	2.38176
1.85	2.53010	6.03023	2.38339
1.86	2.55072	6.08345	2.38499
1.87	2.57154	6.13716	2.38657
1.88	2.59258	6.19135	2.38811
1.89	2.61382	6.24604	2.38962
1.90	2.63528	6.30124	2.39111
1.91	2.65695	6.35693	2.39257
1.92	2.67884	6.41314	2.39400
1.93	2.70095	6.46986	2.39540
1.94	2.72328	6.52710	2.39678
1.95	2.74583	6.58487	2.39813
1.96	2.76861	6.64317	2.39946
1.97	2.79161	6.70200	2.40077
1.98	2.81484	6.76138	2.40205
1.99	2.83831	6.82130	2.40330
2.00	2.86200	6.88178	2.40453

x	$F_{5/7}(x)$	$H_{2/7}(x)$	$T_{5/7}(x)$
2.0	2.86200	6.88178	2.40453
2.1	3.11226	7.51817	2.41566
2.2	3.38830	8.21618	2.42487
2.3	3.69260	8.98218	2.43248
2.4	4.02789	9.82310	2.43877
2.5	4.39721	10.74658	2.44395
2.6	4.80389	11.76102	2.44823
2.7	5.25161	12.87562	2.45175
2.8	5.74443	14.10052	2.45464
2.9	6.28682	15.44688	2.45703
3.0	6.88371	16.92695	2.45898
3.1	7.54055	18.55424	2.46060
3.2	8.26332	20.34362	2.46192
3.3	9.05863	22.31145	2.46301
3.4	9.93375	24.47575	2.46390
3.5	10.89672	26.85638	2.46463
3.6	11.95636	29.47520	2.46523
3.7	13.12242	32.35628	2.46572
3.8	14.40564	35.52616	2.46613
3.9	15.81783	39.01407	2.46646
4.0	17.37204	42.85220	2.46673
4.1	19.08263	47.07602	2.46696
4.2	20.96542	51.72464	2.46714
4.3	23.03787	56.84113	2.46729
4.4	25.31920	62.47294	2.46741
4.5	27.83060	68.67241	2.46751
4.6	30.59541	75.49716	2.46760
4.7	33.63938	83.01073	2.46767
4.8	36.99088	91.28315	2.46772
4.9	40.68116	100.39158	2.46777
5.0	44.74468	110.42108	2.46780
5.1	49.21945	121.46542	2.46783
5.2	54.14731	133.62794	2.46786
5.3	59.57444	147.02256	2.46788
5.4	65.55171	161.77484	2.46790
5.5	72.13521	178.02323	2.46791
5.6	79.38677	195.92032	2.46792
5.7	87.37456	215.63436	2.46793
5.8	96.17372	237.35081	2.46794
5.9	105.86711	261.27416	2.46794
6.0	116.54607	287.62985	2.46795

x	$F_{5/7}(x)$	$H_{2/7}(x)$	$T_{5/7}(x)$
6.0	116.54607	287.62985	2.46795
6.1	128.31133	316.66644	2.46795
6.2	141.27392	348.65799	2.46796
6.3	155.55627	383.90666	2.46796
6.4	171.29339	422.74565	2.46796
6.5	188.63415	465.54233	2.46796
6.6	207.74267	512.70180	2.46797
6.7	228.79997	564.67077	2.46797
6.8	252.00563	621.94183	2.46797
6.9	277.57975	685.05819	2.46797
7.0	305.76505	754.61886	2.46797
7.1	336.82921	831.28444	2.46797
7.2	371.06741	915.78346	2.46797
7.3	408.80519	1008.91936	2.46797
7.4	450.40159	1111.57821	2.46797
7.5	496.25257	1224.73724	2.46797
7.6	546.79485	1349.47425	2.46797
7.7	602.51007	1486.97796	2.46797
7.8	663.92949	1638.55946	2.46797
7.9	731.63904	1805.66482	2.46797
8.0	806.28500	1989.88904	2.46797
8.1	888.58021	2192.99140	2.46797
8.2	979.31095	2416.91242	2.46797
8.3	1079.34451	2663.79257	2.46797
8.4	1189.63759	2935.99288	2.46797
8.5	1311.24544	3236.11779	2.46797
8.6	1445.33217	3567.04018	2.46797
8.7	1593.18185	3931.92918	2.46797
8.8	1756.21102	4334.28075	2.46797
8.9	1935.98231	4777.95140	2.46797
9.0	2134.21954	5267.19550	2.46797
9.1	2352.82441	5806.70635	2.46797
9.2	2593.89483	6401.66157	2.46797
9.3	2859.74524	7057.77317	2.46797
9.4	3152.92902	7781.34273	2.46797
9.5	3476.26309	8579.32242	2.46797
9.6	3832.85530	9459.38226	2.46797
9.7	4226.13439	10429.98434	2.46797
9.8	4659.88325	11500.46471	2.46797
9.9	5138.27555	12681.12386	2.46797
10.0	5665.91613	13983.32643	2.46797

TABLE 13B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/7$ and x from 1.50 to 10.0.

$\alpha = 4/9$

x	$F_{4/9}(x)$	$H_{5/9}(x)$	$T_{4/9}(x)$	x	$F_{4/9}(x)$	$H_{5/9}(x)$	$T_{4/9}(x)$	x	$F_{4/9}(x)$	$H_{5/9}(x)$	$T_{4/9}(x)$
0.0	1.00000	0.0	0.0	0.50	1.14369	0.40145	0.35101	1.0C	1.61287	C.97391	0.60384
0.01	1.00006	0.00500	0.00500	0.51	1.14963	0.41104	0.35754	1.01	1.62626	C.98774	0.60737
0.02	1.00023	0.01079	0.01079	0.52	1.15569	0.42069	0.36401	1.02	1.63982	1.00168	0.61085
0.03	1.00051	0.01693	0.01693	0.53	1.16188	0.43040	0.37043	1.03	1.65356	1.01574	0.61427
0.04	1.00090	0.02332	0.02329	0.54	1.16821	0.44017	0.37679	1.04	1.66749	1.02992	0.61764
0.05	1.00141	0.02988	0.02984	0.55	1.17466	0.45001	0.38310	1.05	1.68159	1.04421	0.62096
0.06	1.00203	0.03660	0.03652	0.56	1.18124	0.45992	0.38935	1.06	1.69588	1.05862	0.62423
0.C7	1.00276	0.04344	0.04332	C.57	1.18795	0.46989	0.39554	1.07	1.71036	1.07315	0.62744
0.08	1.00360	0.05040	0.05022	0.58	1.19480	0.47992	0.40168	1.08	1.72502	1.08781	0.63061
0.09	1.00456	0.05747	0.05720	0.59	1.20178	0.49003	0.40775	1.09	1.73986	1.10259	0.63372
0.10	1.00563	0.06462	0.06426	0.60	1.20889	0.50020	0.41377	1.10	1.75490	1.11749	0.63678
0.11	1.00681	0.07187	0.07138	0.61	1.21613	0.51044	C.41973	1.11	1.77013	1.13252	0.63980
0.12	1.00811	0.07919	0.07855	0.62	1.22351	0.52075	0.42562	1.12	1.78555	1.14768	0.64276
0.13	1.00952	0.08659	0.08577	0.63	1.23103	0.53113	0.43146	1.13	1.80116	1.16297	0.64568
0.14	1.01104	0.09406	0.09303	0.64	1.23868	0.54159	0.43723	1.14	1.81697	1.17839	0.64855
0.15	1.01268	0.10160	0.10033	0.65	1.24647	0.55211	0.44294	1.15	1.83298	1.19395	0.65137
0.16	1.01443	0.10921	0.10766	0.66	1.25440	0.56271	0.44859	1.16	1.84918	1.20964	C.65415
0.17	1.01630	0.11688	0.11501	0.67	1.26247	0.57338	0.45418	1.17	1.86559	1.22546	0.65688
0.18	1.01828	0.12462	0.12238	0.68	1.27067	0.58413	0.45970	1.18	1.88220	1.24142	0.65956
0.19	1.02037	0.13241	0.12977	0.69	1.27902	0.59496	0.46517	1.19	1.89901	1.25752	0.66220
0.20	1.02258	0.14027	0.13717	0.70	1.28751	0.60586	0.47057	1.20	1.91603	1.27377	0.66480
0.21	1.02490	0.14818	0.14458	0.71	1.29614	0.61684	0.47590	1.21	1.93325	1.29015	0.66735
0.22	1.02734	0.15614	0.15199	0.72	1.30491	0.62789	0.48118	1.22	1.95068	1.30668	0.66986
0.23	1.02989	0.16417	0.15940	0.73	1.31383	0.63903	0.48639	1.23	1.96833	1.32335	0.67232
0.24	1.03256	0.17225	0.16682	0.74	1.32290	0.65025	0.49153	1.24	1.98619	1.34018	0.67475
C.25	1.03535	0.18038	0.17422	C.75	1.33211	0.66155	0.49662	1.25	2.00426	1.35715	0.67713
0.26	1.03825	0.18857	0.18162	0.76	1.34146	0.67293	0.50164	1.26	2.02255	1.37427	0.67947
C.27	1.04127	0.19681	0.18901	0.77	1.35097	0.68440	0.50660	1.27	2.04106	1.39154	0.68178
0.28	1.04440	0.20511	0.19639	0.78	1.36062	0.69595	0.51150	1.28	2.05979	1.40897	0.68404
0.29	1.04765	0.21346	0.20375	0.79	1.37042	0.70759	0.51633	1.29	2.07874	1.42656	0.68626
0.30	1.05102	0.22186	0.21109	0.80	1.38038	0.71932	0.52110	1.30	2.09791	1.44430	0.68845
0.31	1.05451	0.23032	0.21841	0.81	1.39048	0.73113	0.52581	1.31	2.11732	1.46220	0.69059
0.32	1.05811	0.23883	0.22571	0.82	1.40074	0.74304	0.53046	1.32	2.13695	1.48027	0.69270
0.33	1.06184	0.24739	0.23299	0.83	1.41116	0.75503	0.53504	1.33	2.15681	1.49850	0.69478
0.34	1.06568	0.25601	0.24023	0.84	1.42173	0.76712	0.53957	1.34	2.17690	1.51689	0.69681
0.35	1.06964	0.26468	0.24745	C.85	1.43245	0.77929	0.54403	1.35	2.19722	1.53545	0.69881
0.36	1.07372	0.27341	0.25463	0.86	1.44333	0.79157	0.54843	1.36	2.21779	1.55418	0.70078
0.37	1.07792	0.28218	0.26179	0.87	1.45437	0.80393	0.55277	1.37	2.23859	1.57308	0.70271
0.38	1.08225	0.29102	0.26890	0.88	1.46557	0.81640	0.55705	1.38	2.25963	1.59215	0.70460
0.39	1.08669	0.29991	0.27598	0.89	1.47693	0.82896	0.56127	1.39	2.28092	1.61140	0.70647
C.40	1.09125	0.30885	0.28303	0.90	1.48846	0.84162	0.56543	1.40	2.30245	1.63082	0.70830
0.41	1.09594	0.31785	0.29003	0.91	1.50014	0.85438	0.56953	1.41	2.32423	1.65042	0.71009
0.42	1.10075	0.32691	0.29699	0.92	1.51199	0.86724	0.57357	1.42	2.34626	1.67020	0.71186
0.43	1.10568	0.33602	0.30391	C.93	1.52401	0.88020	0.57756	1.43	2.36854	1.69017	0.71359
0.44	1.11074	0.34519	0.31078	0.94	1.53619	0.89327	0.58148	1.44	2.39107	1.71032	0.71529
0.45	1.11592	0.35442	0.31761	C.95	1.54854	0.90644	0.58535	1.45	2.41386	1.73065	0.71696
0.46	1.12122	0.36371	C.32439	0.96	1.56107	0.91972	0.58916	1.46	2.43691	1.75118	0.71861
0.47	1.12665	0.37305	0.33112	C.97	1.57376	0.93310	0.59291	1.47	2.46022	1.77189	0.72022
0.48	1.13220	0.38246	0.33780	0.98	1.58662	0.94660	0.59661	1.48	2.48380	1.79280	0.72180
C.49	1.13789	0.39192	0.34443	0.99	1.59966	0.96020	0.60025	1.49	2.50764	1.81391	0.72335
C.50	1.14369	0.40145	0.35101	1.00	1.61287	0.97391	0.60384	1.50	2.53175	1.83521	0.72488

TABLE 14A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 4/9$ and x from 0.00 to 1.50.

$\alpha = 4/9$

x	$F_{4/9}(x)$	$H_{5/9}(x)$	$T_{4/9}(x)$
1.50	2.53175	1.83521	0.72488
1.51	2.55613	1.85671	0.72637
1.52	2.58079	1.87841	0.72784
1.53	2.60572	1.90032	0.72929
1.54	2.63093	1.92243	0.73070
1.55	2.65642	1.94475	0.73209
1.56	2.68219	1.96728	0.73346
1.57	2.70826	1.99002	0.73480
1.58	2.73461	2.01298	0.73611
1.59	2.76125	2.03616	0.73740
1.60	2.78819	2.05955	0.73867
1.61	2.81542	2.08317	0.73991
1.62	2.84296	2.10701	0.74113
1.63	2.87080	2.13108	0.74233
1.64	2.89895	2.15538	0.74351
1.65	2.92740	2.17991	0.74466
1.66	2.95617	2.20468	0.74579
1.67	2.98525	2.22968	0.74690
1.68	3.01465	2.25493	0.74799
1.69	3.04437	2.28041	0.74906
1.70	3.07441	2.30614	0.75011
1.71	3.10479	2.33212	0.75114
1.72	3.13549	2.35835	0.75215
1.73	3.16652	2.38483	0.75314
1.74	3.19790	2.41157	0.75411
1.75	3.22961	2.43856	0.75506
1.76	3.26166	2.46582	0.75600
1.77	3.29407	2.49334	0.75692
1.78	3.32682	2.52112	0.75782
1.79	3.35992	2.54918	0.75870
1.80	3.39339	2.57751	0.75957
1.81	3.42721	2.60611	0.76042
1.82	3.46139	2.63499	0.76125
1.83	3.49595	2.66416	0.76207
1.84	3.53087	2.69360	0.76287
1.85	3.56617	2.72334	0.76366
1.86	3.60184	2.75336	0.76443
1.87	3.63790	2.78368	0.76519
1.88	3.67434	2.81430	0.76593
1.89	3.71117	2.84521	0.76666
1.90	3.74840	2.87643	0.76733
1.91	3.78602	2.90795	0.76808
1.92	3.82404	2.93978	0.76876
1.93	3.86247	2.97193	0.76944
1.94	3.90130	3.00439	0.77010
1.95	3.94055	3.03717	0.77075
1.96	3.98021	3.07027	0.77138
1.97	4.02030	3.10370	0.77201
1.98	4.06081	3.13746	0.77262
1.99	4.10175	3.17155	0.77322
2.00	4.14312	3.20597	0.77381

x	$F_{4/9}(x)$	$H_{5/9}(x)$	$T_{4/9}(x)$
2.0	4.14312	3.20597	0.77381
2.1	4.58162	3.56953	0.77910
2.2	5.06842	3.97083	0.78345
2.3	5.60854	4.41401	0.78702
2.4	6.20754	4.90362	0.78995
2.5	6.87159	5.44468	0.79235
2.6	7.60752	6.04277	0.79432
2.7	8.42290	6.70403	0.79593
2.8	9.32612	7.43525	0.79725
2.9	10.32646	8.24394	0.79833
3.0	11.43418	9.13839	0.79922
3.1	12.66066	10.12780	0.79994
3.2	14.01848	11.22230	0.80054
3.3	15.52156	12.43311	0.80102
3.4	17.18533	13.77266	0.80142
3.5	19.02681	15.25465	0.80175
3.6	21.06487	16.89427	0.80201
3.7	23.32039	18.70830	0.80223
3.8	25.81643	20.71531	0.80241
3.9	28.57854	22.93582	0.80255
4.0	31.63496	25.39254	0.80267
4.1	35.01693	28.11058	0.80277
4.2	38.75901	31.11772	0.80285
4.3	42.89942	34.44467	0.80292
4.4	47.48046	38.12540	0.80297
4.5	52.54887	42.19749	0.80301
4.6	58.15639	46.70249	0.80305
4.7	64.36021	51.68637	0.80308
4.8	71.22362	57.19994	0.80310
4.9	78.81658	63.29943	0.80312
5.0	87.21650	70.04700	0.80314
5.1	96.50895	77.51141	0.80315
5.2	106.78862	85.76871	0.80316
5.3	118.16019	94.90298	0.80317
5.4	130.73944	105.00723	0.80318
5.5	144.65443	116.18432	0.80319
5.6	160.04676	128.54799	0.80319
5.7	177.07305	142.22404	0.80319
5.8	195.90649	157.35158	0.80320
5.9	216.73860	174.08446	0.80320
6.0	239.78122	192.59281	0.80320

x	$F_{4/9}(x)$	$H_{5/9}(x)$	$T_{4/9}(x)$
6.0	239.78122	192.59281	0.80320
6.1	265.26857	213.06478	0.80320
6.2	293.45969	235.70843	0.80321
6.3	324.64105	260.75386	0.80321
6.4	359.12941	288.45549	0.80321
6.5	397.27510	319.09472	0.80321
6.6	439.46550	352.98269	0.80321
6.7	486.12900	390.46350	0.80321
6.8	537.73930	431.91763	0.80321
6.9	594.82027	477.76585	0.80321
7.0	657.95116	528.47343	0.80321
7.1	727.77254	584.55489	0.80321
7.2	804.99274	646.57917	0.80321
7.3	890.39504	715.17539	0.80321
7.4	984.84556	791.03924	0.80321
7.5	1089.30204	874.94000	0.80321
7.6	1204.82353	967.72831	0.80321
7.7	1332.58110	1070.34478	0.80321
7.8	1473.86967	1183.82951	0.80321
7.9	1630.12111	1309.33258	0.80321
8.0	1802.91869	1448.12572	0.80321
8.1	1994.01315	1601.61512	0.80321
8.2	2205.34032	1771.35568	0.80321
8.3	2439.04073	1959.06669	0.80321
8.4	2697.48122	2166.64924	0.80321
8.5	2983.27890	2396.20540	0.80321
8.6	3299.32752	2650.05949	0.80321
8.7	3648.82678	2930.78153	0.80321
8.8	4035.31463	3241.21324	0.80321
8.9	4462.70298	3584.49673	0.80321
9.0	4935.31726	3964.10624	0.80321
9.1	5457.94009	4383.88321	0.80321
9.2	6035.85958	4848.07513	0.80321
9.3	6674.92275	5361.37839	0.80321
9.4	7381.59456	5928.98572	0.80321
9.5	8163.02320	6556.63863	0.80321
9.6	9027.11224	7250.68538	0.80321
9.7	9982.60048	8018.14507	0.80321
9.8	11039.15012	8866.77849	0.80321
9.9	12207.44434	9805.16650	0.80321
10.0	13499.29508	10842.79661	0.80321

TABLE 14B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 4/9$ and x from 1.50 to 10.0.

$\alpha = 5/9$

x	$F_{5/9}(x)$	$H_{4/9}(x)$	$T_{5/9}(x)$	x	$F_{5/9}(x)$	$H_{4/9}(x)$	$T_{5/9}(x)$	x	$F_{5/9}(x)$	$H_{4/9}(x)$	$T_{5/9}(x)$
0.0	1.00000	0.0	0.0	0.50	1.11478	0.68493	0.61441	1.00	1.48736	1.43639	0.96573
0.01	1.00005	0.02027	0.02027	0.51	1.11951	0.69829	0.62375	1.01	1.49795	1.45387	0.97057
0.02	1.00018	0.03753	0.03753	0.52	1.12435	0.71169	0.63298	1.02	1.50867	1.47148	0.97534
0.03	1.00041	0.05383	0.05380	0.53	1.12928	0.72514	0.64212	1.03	1.51954	1.48921	0.98004
0.04	1.00072	0.06952	0.06947	0.54	1.13432	0.73863	0.65116	1.04	1.53054	1.50708	0.98467
0.05	1.00113	0.08478	0.08469	0.55	1.13947	0.75216	0.66010	1.05	1.54169	1.52508	0.98922
0.06	1.00167	0.09972	0.09956	0.56	1.14471	0.76574	0.66894	1.06	1.55298	1.54321	0.99371
0.07	1.00221	0.11439	0.11414	0.57	1.15006	0.77938	0.67768	1.07	1.56441	1.56147	0.99812
0.08	1.00288	0.12884	0.12847	0.58	1.15552	0.79306	0.68632	1.08	1.57599	1.57988	1.00247
0.09	1.00365	0.14310	0.14258	0.59	1.16108	0.80680	0.69487	1.09	1.58771	1.59842	1.00675
0.10	1.00450	0.15720	0.15650	0.60	1.16674	0.82059	0.70331	1.10	1.59958	1.61710	1.01096
0.11	1.00545	0.17116	0.17024	0.61	1.17251	0.83443	0.71166	1.11	1.61159	1.63593	1.01510
0.12	1.00649	0.18500	0.18381	0.62	1.17839	0.84834	0.71991	1.12	1.62376	1.65490	1.01918
0.13	1.00762	0.19873	0.19723	0.63	1.18438	0.86231	0.72807	1.13	1.63607	1.67402	1.02319
0.14	1.00883	0.21236	0.21050	0.64	1.19047	0.87633	0.73612	1.14	1.64854	1.69328	1.02714
0.15	1.01014	0.22591	0.22364	0.65	1.19667	0.89042	0.74409	1.15	1.66116	1.71270	1.03102
0.16	1.01154	0.23937	0.23664	0.66	1.20298	0.90458	0.75195	1.16	1.67394	1.73227	1.03485
0.17	1.01304	0.25277	0.24952	0.67	1.20940	0.91880	0.75972	1.17	1.68686	1.75199	1.03861
0.18	1.01462	0.26610	0.26227	0.68	1.21593	0.93309	0.76739	1.18	1.69995	1.77187	1.04231
0.19	1.01629	0.27938	0.27491	0.69	1.22257	0.94745	0.77497	1.19	1.71319	1.79191	1.04595
0.20	1.01806	0.29261	0.28742	0.70	1.22932	0.96188	0.78245	1.20	1.72659	1.81211	1.04953
0.21	1.01992	0.30580	0.29983	0.71	1.23619	0.97639	0.78984	1.21	1.74016	1.83247	1.05305
0.22	1.02186	0.31895	0.31212	0.72	1.24316	0.99097	0.79713	1.22	1.75388	1.85299	1.05651
0.23	1.02391	0.33206	0.32431	0.73	1.25025	1.00562	0.80434	1.23	1.76777	1.87368	1.05992
0.24	1.02604	0.34514	0.33638	0.74	1.25746	1.02036	0.81145	1.24	1.78182	1.89454	1.06327
0.25	1.02827	0.35820	0.34835	0.75	1.26478	1.03517	0.81846	1.25	1.79603	1.91558	1.06656
0.26	1.03059	0.37123	0.36021	0.76	1.27221	1.05007	0.82539	1.26	1.81041	1.93678	1.06980
0.27	1.03300	0.38425	0.37197	0.77	1.27976	1.06505	0.83222	1.27	1.82497	1.95816	1.07298
0.28	1.03550	0.39725	0.38363	0.78	1.28743	1.08011	0.83897	1.28	1.83969	1.97971	1.07611
0.29	1.03810	0.41024	0.39518	0.79	1.29522	1.09526	0.84562	1.29	1.85458	2.00145	1.07919
0.30	1.04079	0.42322	0.40663	0.80	1.30312	1.11050	0.85218	1.30	1.86964	2.02336	1.08222
0.31	1.04358	0.43619	0.41798	0.81	1.31115	1.12583	0.85866	1.31	1.88488	2.04546	1.08520
0.32	1.04646	0.44916	0.42922	0.82	1.31929	1.14125	0.86505	1.32	1.90029	2.06775	1.08812
0.33	1.04944	0.46213	0.44036	0.83	1.32756	1.15676	0.87135	1.33	1.91589	2.09022	1.09100
0.34	1.05251	0.47511	0.45141	0.84	1.33594	1.17237	0.87756	1.34	1.93165	2.11289	1.09382
0.35	1.05567	0.48809	0.46235	0.85	1.34445	1.18807	0.88369	1.35	1.94760	2.13574	1.09660
0.36	1.05893	0.50107	0.47319	0.86	1.35308	1.20388	0.88973	1.36	1.96374	2.15879	1.09933
0.37	1.06229	0.51407	0.48393	0.87	1.36184	1.21978	0.89569	1.37	1.98005	2.18204	1.10201
0.38	1.06574	0.52708	0.49457	0.88	1.37072	1.23578	0.90156	1.38	1.99655	2.20549	1.10465
0.39	1.06929	0.54010	0.50510	0.89	1.37973	1.25189	0.90735	1.39	2.01323	2.22914	1.10724
0.40	1.07293	0.55314	0.51554	0.90	1.38886	1.26810	0.91305	1.40	2.03011	2.25299	1.10979
0.41	1.07667	0.56620	0.52588	0.91	1.39812	1.28442	0.91868	1.41	2.04717	2.27705	1.11229
0.42	1.08051	0.57928	0.53612	0.92	1.40751	1.30085	0.92422	1.42	2.06442	2.30132	1.11475
0.43	1.08445	0.59238	0.54625	0.93	1.41703	1.31739	0.92968	1.43	2.08187	2.32580	1.11717
0.44	1.08848	0.60551	0.55629	0.94	1.42668	1.33404	0.93507	1.44	2.09951	2.35049	1.11954
0.45	1.09262	0.61867	0.56623	0.95	1.43646	1.35080	0.94037	1.45	2.11735	2.37540	1.12187
0.46	1.09685	0.63185	0.57606	0.96	1.44637	1.36768	0.94559	1.46	2.13538	2.40052	1.12416
0.47	1.10118	0.64507	0.58580	0.97	1.45642	1.38468	0.95074	1.47	2.15362	2.42587	1.12642
0.48	1.10561	0.65832	0.59544	0.98	1.46660	1.40179	0.95581	1.48	2.17205	2.45144	1.12863
0.49	1.11015	0.67161	0.60497	0.99	1.47691	1.41903	0.96081	1.49	2.19069	2.47724	1.13080
0.50	1.11478	0.68493	0.61441	1.00	1.48736	1.43639	0.96573	1.50	2.20954	2.50326	1.13293

TABLE 15A. Lanchester-Clifford-Schläfli Functions $F_{\alpha}(x)$, $H_{1-\alpha}(x)$, and $T_{\alpha}(x)$ for $\alpha = 5/9$ and x from 0.00 to 1.50.

$\alpha = 5/9$

x	$F_{5/9}(x)$	$H_{4/9}(x)$	$T_{5/9}(x)$
1.50	2.20954	2.50326	1.13293
1.51	2.22859	2.52952	1.13503
1.52	2.24785	2.55601	1.13709
1.53	2.26732	2.58273	1.13911
1.54	2.28701	2.60970	1.14110
1.55	2.30691	2.63690	1.14305
1.56	2.32702	2.66435	1.14496
1.57	2.34735	2.69205	1.14684
1.58	2.36791	2.71999	1.14869
1.59	2.38868	2.74819	1.15051
1.60	2.40968	2.77665	1.15229
1.61	2.43091	2.80536	1.15404
1.62	2.45236	2.83433	1.15575
1.63	2.47405	2.86356	1.15744
1.64	2.49596	2.89307	1.15910
1.65	2.51812	2.92284	1.16072
1.66	2.54051	2.95288	1.16232
1.67	2.56313	2.98320	1.16389
1.68	2.58600	3.01379	1.16543
1.69	2.60911	3.04467	1.16694
1.70	2.63247	3.07583	1.16842
1.71	2.65608	3.10728	1.16988
1.72	2.67993	3.13902	1.17130
1.73	2.70404	3.17105	1.17271
1.74	2.72841	3.20338	1.17408
1.75	2.75303	3.23601	1.17544
1.76	2.77791	3.26894	1.17676
1.77	2.80305	3.30217	1.17806
1.78	2.82846	3.33572	1.17934
1.79	2.85413	3.36958	1.18060
1.80	2.88007	3.40375	1.18183
1.81	2.90629	3.43825	1.18304
1.82	2.93278	3.47306	1.18422
1.83	2.95954	3.50821	1.18539
1.84	2.98659	3.54368	1.18653
1.85	3.01392	3.57948	1.18765
1.86	3.04153	3.61562	1.18875
1.87	3.06943	3.65210	1.18983
1.88	3.09762	3.68893	1.19089
1.89	3.12611	3.72610	1.19193
1.90	3.15489	3.76362	1.19295
1.91	3.18397	3.80150	1.19395
1.92	3.21335	3.83973	1.19493
1.93	3.24303	3.87833	1.19590
1.94	3.27302	3.91729	1.19684
1.95	3.30332	3.95662	1.19777
1.96	3.33394	3.99632	1.19868
1.97	3.36487	4.03640	1.19957
1.98	3.39612	4.07686	1.20045
1.99	3.42769	4.11771	1.20131
2.00	3.45958	4.15895	1.20215

x	$F_{5/9}(x)$	$H_{4/9}(x)$	$T_{5/9}(x)$
2.0	3.45958	4.15895	1.20215
2.1	3.79712	4.59359	1.20976
2.2	4.17078	5.07180	1.21603
2.3	4.58419	5.59823	1.22120
2.4	5.04139	6.17801	1.22546
2.5	5.54681	6.81681	1.22896
2.6	6.10538	7.52085	1.23184
2.7	6.72255	8.29700	1.23421
2.8	7.40432	9.15284	1.23615
2.9	8.15736	10.09671	1.23774
3.0	8.98900	11.13782	1.23905
3.1	9.90737	12.28636	1.24012
3.2	10.92143	13.55353	1.24100
3.3	12.04109	14.95173	1.24173
3.4	13.27730	16.49462	1.24232
3.5	14.64214	18.19729	1.24280
3.6	16.14898	20.07640	1.24320
3.7	17.81254	22.15035	1.24353
3.8	19.64913	24.43943	1.24379
3.9	21.67672	26.96607	1.24401
4.0	23.91518	29.75503	1.24419
4.1	26.38646	32.83364	1.24434
4.2	29.11478	36.23209	1.24446
4.3	32.12689	39.98370	1.24456
4.4	35.45236	44.12529	1.24464
4.5	39.12382	48.69750	1.24470
4.6	43.17730	53.74522	1.24476
4.7	47.65262	59.31802	1.24480
4.8	52.59374	65.47063	1.24484
4.9	58.04920	72.26352	1.24487
5.0	64.07262	79.76344	1.24489
5.1	70.72323	88.04413	1.24491
5.2	78.06642	97.18702	1.24493
5.3	86.17442	107.28205	1.24494
5.4	95.12701	118.42853	1.24495
5.5	105.01228	130.73616	1.24496
5.6	115.92754	144.32608	1.24497
5.7	127.98027	159.33211	1.24497
5.8	141.28915	175.90202	1.24498
5.9	155.98528	194.19902	1.24498
6.0	172.21345	214.40339	1.24499

x	$F_{5/9}(x)$	$H_{4/9}(x)$	$T_{5/9}(x)$
6.0	172.21345	214.40339	1.24499
6.1	190.13359	236.71422	1.24499
6.2	209.92230	261.35142	1.24499
6.3	231.77469	288.55787	1.24499
6.4	255.90621	318.60182	1.24499
6.5	282.55485	351.77958	1.24500
6.6	311.98348	388.41841	1.24500
6.7	344.48243	428.87978	1.24500
6.8	380.37238	473.56293	1.24500
6.9	420.00753	522.90885	1.24500
7.0	463.77911	577.40463	1.24500
7.1	512.11927	637.58826	1.24500
7.2	565.50530	704.05402	1.24500
7.3	624.46443	777.45828	1.24500
7.4	689.57900	858.52607	1.24500
7.5	761.49225	948.05822	1.24500
7.6	840.91470	1046.93931	1.24500
7.7	928.63114	1156.14644	1.24500
7.8	1025.50848	1276.75889	1.24500
7.9	1132.50427	1409.96882	1.24500
8.0	1250.67622	1557.09308	1.24500
8.1	1381.19269	1719.58627	1.24500
8.2	1525.34424	1899.05517	1.24500
8.3	1684.55646	2097.27460	1.24500
8.4	1860.40405	2316.20509	1.24500
8.5	2054.62647	2558.01226	1.24500
8.6	2269.14518	2825.08834	1.24500
8.7	2506.08267	3120.07581	1.24500
8.8	2767.78351	3445.89369	1.24500
8.9	3056.83761	3805.76642	1.24500
9.0	3376.10590	4203.25584	1.24500
9.1	3728.74870	4642.29657	1.24500
9.2	4118.25705	5127.23496	1.24500
9.3	4548.48737	5662.87224	1.24500
9.4	5023.69967	6254.51215	1.24500
9.5	5548.59986	6908.01353	1.24500
9.6	6128.38637	7629.84845	1.24500
9.7	6768.80181	8427.16646	1.24500
9.8	7476.18986	9307.86545	1.24500
9.9	8257.55829	10280.67011	1.24500
10.0	9120.64845	11355.21841	1.24500

TABLE 15B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/9$ and x from 1.50 to 10.0.

$\alpha = 3/11$

x	$F_{3/11}(x)$	$H_{8/11}(x)$	$T_{3/11}(x)$	x	$F_{3/11}(x)$	$H_{8/11}(x)$	$T_{3/11}(x)$	x	$F_{3/11}(x)$	$H_{8/11}(x)$	$T_{3/11}(x)$
0.0	1.00000	0.0	0.0	C.50	1.23485	0.18975	0.15367	1.00	2.01006	0.57771	0.28741
0.01	1.00009	0.00062	0.00062	0.51	1.24457	0.19558	0.15715	1.01	2.03235	0.58776	0.28920
0.02	1.00037	0.00170	0.00169	0.52	1.25451	0.20148	0.16060	1.02	2.05494	0.59791	0.29096
0.03	1.00083	0.00306	0.00306	C.53	1.26467	0.20745	0.16404	1.03	2.07784	0.60816	0.29269
C.04	1.00147	0.00465	0.00464	0.54	1.27504	0.21349	0.16744	1.04	2.10105	0.61852	0.29439
C.05	1.00229	0.00643	0.00641	C.55	1.28562	0.21961	0.17082	1.05	2.12457	0.62899	0.29605
0.06	1.00330	0.00838	0.00836	0.56	1.29642	0.22580	0.17417	1.06	2.14841	0.63957	0.29769
0.07	1.00449	0.01049	0.01045	0.57	1.30744	0.23206	0.17749	1.07	2.17257	0.65025	0.29930
0.08	1.00587	0.01274	0.01267	0.58	1.31868	0.23839	0.18078	1.08	2.19704	0.66105	0.30088
0.09	1.00743	0.01513	0.01502	0.59	1.33014	0.24480	0.18404	1.09	2.22184	0.67196	0.30243
0.10	1.00918	0.01764	0.01748	0.60	1.34182	0.25129	0.18727	1.10	2.24696	0.68298	0.30396
0.11	1.01110	0.02027	G.02005	0.61	1.35373	0.25784	0.19047	1.11	2.27242	0.69411	0.30545
0.12	1.01322	0.02301	0.02271	0.62	1.36586	0.26448	0.19363	1.12	2.29820	0.70537	0.30692
0.13	1.01552	0.02586	0.02547	0.63	1.37822	0.27118	0.19676	1.13	2.32433	0.71673	0.30836
C.14	1.01800	0.02882	0.02831	C.64	1.39080	0.27797	0.19986	1.14	2.35079	0.72822	0.30978
0.15	1.02067	0.03187	0.03123	C.65	1.40361	0.28483	0.20292	1.15	2.37759	0.73982	0.31116
0.16	1.02353	0.03503	0.03422	0.66	1.41666	0.29176	0.20595	1.16	2.40473	0.75154	0.31253
0.17	1.02657	0.03827	0.03728	C.67	1.42993	0.29878	0.20894	1.17	2.43222	0.76339	0.31386
0.18	1.02979	0.04161	0.04041	C.68	1.44345	0.30587	0.21190	1.18	2.46007	0.77536	0.31518
C.19	1.03321	0.04504	0.04359	C.69	1.45719	0.31304	C.21482	1.19	2.48826	0.78745	0.31646
C.20	1.03681	0.04856	0.04683	0.7C	1.47117	0.32029	0.21771	1.20	2.51682	0.79966	0.31773
0.21	1.04060	0.05216	0.05013	C.71	1.48540	0.32761	0.22056	1.21	2.54573	0.81201	0.31897
0.22	1.04458	0.05585	0.05346	0.72	1.49986	0.33502	0.22337	1.22	2.57501	0.82448	C.32018
0.23	1.04874	0.05962	0.05685	C.73	1.51456	0.34251	0.22614	1.23	2.60466	0.83708	0.32138
0.24	1.05310	0.06347	0.06027	C.74	1.52951	0.35008	0.22888	1.24	2.63468	0.84981	0.32255
0.25	1.05764	0.06740	0.06372	0.75	1.54470	0.35773	0.23159	1.25	2.66507	0.86267	0.32370
0.26	1.06238	0.07141	0.06721	0.76	1.56015	0.36546	0.23425	1.26	2.69584	0.87567	0.32482
0.27	1.06730	0.07549	0.07073	0.77	1.57584	0.37328	0.23688	1.27	2.72699	0.88880	0.32593
0.28	1.07242	0.07966	0.07428	C.78	1.59178	0.38118	0.23947	1.28	2.75852	0.90206	0.32701
0.29	1.07773	0.08390	0.07785	C.75	1.60797	0.38917	0.24202	1.29	2.79044	0.91547	0.32807
C.30	1.08323	0.08821	0.08144	0.80	1.62442	0.39724	0.24454	1.30	2.82276	0.92901	0.32911
0.31	1.08893	0.09260	0.08504	0.81	1.64112	0.40539	0.24702	1.31	2.85547	0.94270	0.33014
0.32	1.09481	0.09707	C.08866	0.82	1.65809	0.41363	0.24946	1.32	2.88858	0.95652	0.33114
0.33	1.10090	0.10161	0.09229	0.83	1.67531	0.42196	0.25187	1.33	2.92210	0.97049	0.33212
C.34	1.10717	0.10622	0.09594	C.84	1.69280	0.43038	0.25424	1.34	2.95602	0.98460	0.33308
0.35	1.11365	0.11090	0.09959	C.85	1.71055	0.43889	0.25658	1.35	2.99035	0.99887	0.33403
0.36	1.12032	0.11566	0.10324	0.86	1.72857	0.44748	0.25888	1.36	3.02510	1.01327	0.33496
0.37	1.12719	0.12049	0.10689	0.87	1.74686	0.45617	0.26114	1.37	3.06027	1.02783	0.33586
C.38	1.13425	0.12539	C.11055	0.88	1.76541	0.46495	0.26336	1.38	3.09586	1.04254	0.33675
0.39	1.14152	0.13036	0.11420	C.89	1.78424	0.47382	0.26556	1.39	3.13188	1.05741	0.33763
0.40	1.14898	0.13540	0.11785	C.90	1.80335	0.48278	0.26771	1.40	3.16833	1.07242	0.33848
0.41	1.15665	0.14052	0.12149	0.91	1.82273	0.49184	0.26983	1.41	3.20522	1.08760	0.33932
0.42	1.16452	0.14571	0.12512	0.92	1.84240	0.50099	0.27192	1.42	3.24255	1.10293	0.34014
0.43	1.17259	0.15096	0.12874	C.93	1.86234	0.51023	0.27397	1.43	3.28032	1.11842	0.34095
0.44	1.18087	0.15629	0.13235	C.94	1.88257	0.51958	0.27599	1.44	3.31854	1.13407	0.34174
0.45	1.18934	0.16169	0.13595	0.95	1.90309	0.52902	0.27798	1.45	3.35721	1.14989	0.34251
0.46	1.19803	0.16716	0.13953	C.96	1.92390	0.53856	0.27993	1.46	3.39634	1.16587	0.34327
0.47	1.20692	0.17270	0.14309	C.97	1.94499	0.54819	0.28185	1.47	3.43594	1.18202	0.34402
0.48	1.21602	0.17831	0.14664	C.98	1.96639	0.55793	0.28374	1.48	3.47600	1.19833	0.34474
0.45	1.22533	0.18400	0.15016	0.99	1.98807	0.56777	0.28559	1.49	3.51653	1.21482	0.34546
0.50	1.23485	0.18975	0.15367	1.00	2.01006	0.57771	0.28741	1.50	3.55754	1.23148	0.34616

TABLE 16A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/11$ and x from 0.00 to 1.50.

$\alpha = 3/11$

x	$F_{3/11}(x)$	$H_{8/11}(x)$	$T_{3/11}(x)$
1.50	3.55754	1.23146	0.34616
1.51	3.59902	1.24831	0.34685
1.52	3.64100	1.26532	0.34752
1.53	3.68346	1.28250	0.34818
1.54	3.72642	1.29987	0.34882
1.55	3.76988	1.31741	0.34946
1.56	3.81385	1.33514	0.35008
1.57	3.85832	1.35306	0.35069
1.58	3.90331	1.37116	0.35128
1.59	3.94882	1.38945	0.35186
1.60	3.99486	1.40793	0.35244
1.61	4.04143	1.42661	0.35300
1.62	4.08853	1.44548	0.35355
1.63	4.13618	1.46456	0.35408
1.64	4.18437	1.48383	0.35461
1.65	4.23312	1.50330	0.35513
1.66	4.28242	1.52298	0.35563
1.67	4.33229	1.54286	0.35613
1.68	4.38273	1.56295	0.35662
1.69	4.43374	1.58325	0.35709
1.70	4.48533	1.60377	0.35756
1.71	4.53752	1.62450	0.35802
1.72	4.59029	1.64545	0.35846
1.73	4.64367	1.66662	0.35890
1.74	4.69765	1.68801	0.35933
1.75	4.75224	1.70963	0.35975
1.76	4.80745	1.73148	0.36017
1.77	4.86328	1.75355	0.36057
1.78	4.91975	1.77586	0.36097
1.79	4.97685	1.79840	0.36135
1.80	5.03459	1.82118	0.36173
1.81	5.09299	1.84420	0.36211
1.82	5.15204	1.86746	0.36247
1.83	5.21175	1.89097	0.36283
1.84	5.27214	1.91472	0.36318
1.85	5.33320	1.93872	0.36352
1.86	5.39495	1.96298	0.36386
1.87	5.45739	1.98750	0.36418
1.88	5.52052	2.01227	0.36451
1.89	5.58436	2.03730	0.36482
1.90	5.64892	2.06260	0.36513
1.91	5.71419	2.08817	0.36544
1.92	5.78020	2.11400	0.36573
1.93	5.84693	2.14011	0.36602
1.94	5.91441	2.16650	0.36631
1.95	5.98265	2.19316	0.36659
1.96	6.05163	2.22010	0.36686
1.97	6.12139	2.24733	0.36713
1.98	6.19192	2.27485	0.36739
1.99	6.26323	2.30266	0.36765
2.00	6.33533	2.33076	0.36790

x	$F_{3/11}(x)$	$H_{8/11}(x)$	$T_{3/11}(x)$
2.0	6.33533	2.33076	0.36790
2.1	7.10165	2.62868	0.37015
2.2	7.95658	2.95971	0.37198
2.3	8.90980	3.32757	0.37347
2.4	9.97211	3.73641	0.37469
2.5	11.15547	4.19082	0.37567
2.6	12.47321	4.69588	0.37648
2.7	13.94011	5.25726	0.37713
2.8	15.57260	5.88123	0.37767
2.9	17.38893	6.57475	0.37810
3.0	19.40935	7.34555	0.37845
3.1	21.65633	8.20218	0.37874
3.2	24.15483	9.15415	0.37898
3.3	26.93254	10.21201	0.37917
3.4	30.02017	11.38745	0.37933
3.5	33.45181	12.69344	0.37945
3.6	37.26528	14.14437	0.37956
3.7	41.50251	15.75618	0.37964
3.8	46.21003	17.54657	0.37971
3.9	51.43944	19.53517	0.37977
4.0	57.24797	21.74373	0.37982
4.1	63.69909	24.19638	0.37985
4.2	70.86318	26.91988	0.37989
4.3	78.81826	29.94390	0.37991
4.4	87.65088	33.30131	0.37993
4.5	97.45698	37.02860	0.37995
4.6	108.34293	41.16619	0.37996
4.7	120.42666	45.75890	0.37997
4.8	133.83889	50.85642	0.37998
4.9	148.72458	56.51384	0.37999
5.0	165.24436	62.79221	0.38000
5.1	183.57632	69.75921	0.38000
5.2	203.91787	77.48985	0.38001
5.3	226.48778	86.06730	0.38001
5.4	251.52855	95.58370	0.38001
5.5	279.30894	106.14119	0.38001
5.6	310.12681	117.85297	0.38002
5.7	344.31227	130.84449	0.38002
5.8	382.23113	145.25477	0.38002
5.9	424.28878	161.23786	0.38002
6.0	470.93444	178.96450	0.38002

x	$F_{3/11}(x)$	$H_{8/11}(x)$	$T_{3/11}(x)$
6.0	470.93444	178.96450	0.38002
6.1	522.66591	198.62384	0.38002
6.2	580.03475	220.42550	0.38002
6.3	643.65215	244.60175	0.38002
6.4	714.19529	271.40993	0.38002
6.5	792.41445	301.13518	0.38002
6.6	879.14094	334.09340	0.38002
6.7	975.29576	370.63459	0.38002
6.8	1081.89926	411.14653	0.38002
6.9	1200.08186	456.05879	0.38002
7.0	1331.09587	505.84728	0.38002
7.1	1476.32861	561.03923	0.38002
7.2	1637.31692	622.21865	0.38002
7.3	1815.76322	690.03252	0.38002
7.4	2013.55334	765.19749	0.38002
7.5	2232.77622	848.50742	0.38002
7.6	2475.74571	940.84162	0.38002
7.7	2745.02478	1043.17407	0.38002
7.8	3043.45221	1156.58359	0.38002
7.9	3374.17228	1282.26508	0.38002
8.0	3740.66754	1421.54198	0.38002
8.1	4146.79510	1575.88009	0.38002
8.2	4596.82687	1746.90284	0.38002
8.3	5095.49407	1936.40820	0.38002
8.4	5648.03650	2146.38742	0.38002
8.5	6260.25709	2379.04575	0.38002
8.6	6938.58234	2636.82542	0.38002
8.7	7690.12918	2922.43103	0.38002
8.8	8522.77897	3238.85767	0.38002
8.9	9445.25952	3589.42213	0.38002
9.0	10467.23577	3977.79731	0.38002
9.1	11599.41029	4408.05044	0.38002
9.2	12853.63442	4884.68531	0.38002
9.3	14243.03139	5412.68907	0.38002
9.4	15782.13262	5997.58398	0.38002
9.5	17487.02849	6645.48478	0.38002
9.6	19375.53538	7363.16211	0.38002
9.7	21467.38047	8158.11278	0.38002
9.8	23784.40639	9038.63749	0.38002
9.9	26350.79765	10013.92693	0.38002
10.0	29193.33137	11054.15705	0.38002

TABLE 16B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 3/11$ and x from 1.50 to 10.0.

$\alpha = 5/11$

x	$F_{5/11}(x)$	$H_{6/11}(x)$	$T_{5/11}(x)$	x	$F_{5/11}(x)$	$H_{6/11}(x)$	$T_{5/11}(x)$	x	$F_{5/11}(x)$	$H_{6/11}(x)$	$T_{5/11}(x)$
0.0	1.00000	0.0	0.0	0.50	1.14048	0.42061	0.36880	1.00	1.59890	1.00692	0.62976
0.01	1.00006	0.00566	0.00566	0.51	1.14628	0.43048	0.37555	1.01	1.61198	1.02102	0.63340
0.02	1.00022	0.01206	0.01206	0.52	1.15221	0.44042	0.38224	1.02	1.62522	1.03525	0.63699
0.03	1.00050	0.01878	0.01877	0.53	1.15826	0.45042	0.38887	1.03	1.63865	1.04959	0.64052
0.04	1.00088	0.02570	0.02568	0.54	1.16444	0.46048	0.39545	1.04	1.65224	1.06405	0.64400
0.05	1.00138	0.03279	0.03274	0.55	1.17074	0.47060	0.40197	1.05	1.66602	1.07862	0.64743
0.06	1.00198	0.04001	0.03993	0.56	1.17718	0.48079	0.40843	1.06	1.67997	1.09332	0.65080
0.07	1.00270	0.04735	0.04722	0.57	1.18374	0.49104	0.41482	1.07	1.69411	1.10814	0.65412
0.08	1.00352	0.05479	0.05459	0.58	1.19043	0.50136	0.42116	1.08	1.70843	1.12309	0.65738
0.09	1.00446	0.06231	0.06204	0.59	1.19725	0.51175	0.42744	1.09	1.72292	1.13815	0.66059
0.10	1.00550	0.06993	0.06954	0.60	1.20420	0.52220	0.43365	1.10	1.73761	1.15335	0.66376
0.11	1.00666	0.07761	0.07710	0.61	1.21128	0.53272	0.43980	1.11	1.75248	1.16867	0.66687
0.12	1.00793	0.08537	0.08470	0.62	1.21850	0.54331	0.44588	1.12	1.76753	1.18412	0.66993
0.13	1.00931	0.09320	0.09234	0.63	1.22584	0.55397	0.45191	1.13	1.78278	1.19971	0.67294
0.14	1.01080	0.10109	0.10001	0.64	1.23332	0.56470	0.45787	1.14	1.79822	1.21542	0.67590
0.15	1.01240	0.10905	0.10771	0.65	1.24093	0.57550	0.46376	1.15	1.81384	1.23127	0.67882
0.16	1.01411	0.11706	0.11543	0.66	1.24868	0.58637	0.46959	1.16	1.82967	1.24726	0.68169
0.17	1.01593	0.12513	0.12317	0.67	1.25657	0.59732	0.47536	1.17	1.84569	1.26338	0.68450
0.18	1.01787	0.13326	0.13092	0.68	1.26459	0.60834	0.48106	1.18	1.86190	1.27964	0.68728
0.19	1.01992	0.14144	0.13868	0.69	1.27274	0.61944	0.48670	1.19	1.87831	1.29604	0.69000
0.20	1.02208	0.14967	0.14644	0.70	1.28104	0.63062	0.49227	1.20	1.89493	1.31259	0.69268
0.21	1.02435	0.15796	0.15420	0.71	1.28947	0.64187	0.49778	1.21	1.91174	1.32928	0.69532
0.22	1.02673	0.16630	0.16197	0.72	1.29805	0.65320	0.50322	1.22	1.92877	1.34611	0.69791
0.23	1.02923	0.17469	0.16973	0.73	1.30676	0.66461	0.50859	1.23	1.94599	1.36309	0.70046
0.24	1.03184	0.18313	0.17748	0.74	1.31562	0.67610	0.51390	1.24	1.96342	1.38022	0.70297
0.25	1.03456	0.19162	0.18522	0.75	1.32462	0.68767	0.51915	1.25	1.98107	1.39750	0.70543
0.26	1.03740	0.20016	0.19294	0.76	1.33376	0.69933	0.52433	1.26	1.99892	1.41493	0.70785
0.27	1.04035	0.20875	0.20065	0.77	1.34305	0.71107	0.52945	1.27	2.01699	1.43252	0.71023
0.28	1.04341	0.21739	0.20835	0.78	1.35248	0.72290	0.53450	1.28	2.03527	1.45026	0.71257
0.29	1.04659	0.22608	0.21602	0.79	1.36206	0.73481	0.53948	1.29	2.05377	1.46816	0.71486
0.30	1.04988	0.23482	0.22366	0.80	1.37179	0.74680	0.54440	1.30	2.07248	1.48623	0.71712
0.31	1.05329	0.24361	0.23129	0.81	1.38166	0.75889	0.54926	1.31	2.09142	1.50445	0.71934
0.32	1.05682	0.25245	0.23888	0.82	1.39168	0.77107	0.55405	1.32	2.11058	1.52283	0.72152
0.33	1.06046	0.26134	0.24644	0.83	1.40186	0.78333	0.55878	1.33	2.12996	1.54138	0.72367
0.34	1.06421	0.27029	0.25398	0.84	1.41218	0.79569	0.56345	1.34	2.14957	1.56010	0.72577
0.35	1.06809	0.27928	0.26148	0.85	1.42266	0.80814	0.56805	1.35	2.16941	1.57898	0.72784
0.36	1.07208	0.28832	0.26894	0.86	1.43329	0.82069	0.57259	1.36	2.18948	1.59804	0.72987
0.37	1.07618	0.29742	0.27636	0.87	1.44408	0.83333	0.57707	1.37	2.20978	1.61727	0.73187
0.38	1.08041	0.30657	0.28375	0.88	1.45502	0.84607	0.58148	1.38	2.23031	1.63667	0.73383
0.39	1.08475	0.31577	0.29110	0.89	1.46612	0.85891	0.58584	1.39	2.25109	1.65625	0.73576
0.40	1.08922	0.32502	0.29840	0.90	1.47738	0.87184	0.59013	1.40	2.27210	1.67601	0.73765
0.41	1.09380	0.33433	0.30566	0.91	1.48879	0.88487	0.59436	1.41	2.29335	1.69595	0.73951
0.42	1.09850	0.34369	0.31287	0.92	1.50037	0.89801	0.59853	1.42	2.31484	1.71607	0.74133
0.43	1.10332	0.35311	0.32004	0.93	1.51211	0.91125	0.60264	1.43	2.33658	1.73637	0.74312
0.44	1.10826	0.36258	0.32716	0.94	1.52401	0.92459	0.60669	1.44	2.35857	1.75686	0.74489
0.45	1.11333	0.37211	0.33423	0.95	1.53607	0.93804	0.61068	1.45	2.38081	1.77755	0.74661
0.46	1.11851	0.38169	0.34125	0.96	1.54830	0.95160	0.61461	1.46	2.40330	1.79842	0.74831
0.47	1.12382	0.39133	0.34822	0.97	1.56070	0.96526	0.61848	1.47	2.42604	1.81948	0.74998
0.48	1.12925	0.40103	0.35513	0.98	1.57326	0.97904	0.62230	1.48	2.44904	1.84074	0.75162
0.49	1.13480	0.41079	0.36199	0.99	1.58600	0.99292	0.62605	1.49	2.47230	1.86220	0.75322
0.50	1.14048	0.42061	0.36880	1.00	1.59890	1.00692	0.62976	1.50	2.49582	1.88385	0.75480

TABLE 17A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/11$ and x from 0.00 to 1.50.

$\alpha = 5/11$

x	$F_{5/11}(x)$	$H_{6/11}(x)$	$T_{5/11}(x)$
1.50	2.49582	1.88385	0.75480
1.51	2.51961	1.90571	0.75635
1.52	2.54366	1.92777	0.75787
1.53	2.56798	1.95004	0.75937
1.54	2.59257	1.97252	0.76083
1.55	2.61744	1.99520	0.76227
1.56	2.64258	2.01810	0.76369
1.57	2.66800	2.04122	0.76507
1.58	2.69370	2.06455	0.76643
1.59	2.71969	2.08810	0.76777
1.60	2.74597	2.11188	0.76908
1.61	2.77253	2.13588	0.77037
1.62	2.79939	2.16010	0.77163
1.63	2.82654	2.18456	0.77287
1.64	2.85398	2.20925	0.77409
1.65	2.88173	2.23417	C.77529
1.66	2.90979	2.25933	0.77646
1.67	2.93815	2.28473	0.77761
1.68	2.96682	2.31037	0.77874
1.69	2.99580	2.33626	0.77985
1.70	3.02509	2.36239	0.78093
1.71	3.05471	2.38878	0.78200
1.72	3.08464	2.41542	0.78305
1.73	3.11490	2.44231	0.78407
1.74	3.14549	2.46946	0.78508
1.75	3.17641	2.49688	0.78607
1.76	3.20766	2.52455	0.78704
1.77	3.23925	2.55250	0.78799
1.78	3.27118	2.58071	0.78892
1.79	3.30345	2.60920	0.78984
1.8C	3.33607	2.63796	C.79074
1.81	3.36904	2.66700	0.79162
1.82	3.40237	2.69632	0.79248
1.83	3.43605	2.72593	0.79333
1.84	3.47009	2.75582	0.79416
1.85	3.50449	2.78601	0.79498
1.86	3.53927	2.81648	0.79578
1.87	3.57441	2.84726	0.79657
1.88	3.60993	2.87833	0.79734
1.89	3.64582	2.90971	C.79809
1.90	3.68210	2.94139	0.79883
1.91	3.71876	2.97338	0.79956
1.92	3.75582	3.00569	0.80027
1.93	3.79326	3.03831	0.80097
1.94	3.83111	3.07125	0.80166
1.95	3.86935	3.10451	0.80233
1.96	3.90800	3.13810	0.80299
1.97	3.94706	3.17202	0.80364
1.98	3.98653	3.20627	0.80428
1.99	4.02642	3.24086	0.80490
2.00	4.06673	3.27578	0.80551

x	$F_{5/11}(x)$	$H_{6/11}(x)$	$T_{5/11}(x)$
2.0	4.06673	3.27578	0.80551
2.1	4.49390	3.64456	0.81100
2.2	4.96800	4.05149	0.81552
2.3	5.49388	4.50074	0.81923
2.4	6.07694	4.99690	0.82227
2.5	6.72315	5.54504	0.82477
2.6	7.43912	6.15079	0.82682
2.7	8.23218	6.82031	C.82849
2.8	9.11044	7.56048	0.82987
2.9	10.08289	8.37883	0.83100
3.0	11.15945	9.28375	0.83192
3.1	12.35115	10.28447	0.83267
3.2	13.67013	11.39120	0.83329
3.3	15.12988	12.61526	0.83380
3.4	16.74529	13.96912	0.83421
3.5	18.53284	15.46660	0.83455
3.6	20.51075	17.12296	0.83483
3.7	22.69921	18.95511	0.83506
3.8	25.12051	20.98170	0.83524
3.9	27.79932	23.22339	0.83539
4.C	30.76293	25.70300	0.83552
4.1	34.04152	28.44579	0.83562
4.2	37.66846	31.47968	0.83570
4.3	41.68066	34.83555	0.83577
4.4	46.11894	38.54752	0.83583
4.5	51.02846	42.65337	0.83587
4.6	56.45912	47.19484	0.83591
4.7	62.46615	52.21810	0.83594
4.8	69.11059	57.77420	0.83597
4.9	76.45996	63.91960	0.83599
5.0	84.58892	70.71674	0.83600
5.1	93.58004	78.23464	0.83602
5.2	103.52460	86.54965	0.83603
5.3	114.52358	95.74618	0.83604
5.4	126.68861	105.91758	0.83605
5.5	140.14315	117.16706	0.83605
5.6	155.02369	129.60876	0.83606
5.7	171.48119	143.36890	0.83606
5.8	189.68257	158.58702	0.83607
5.9	209.81238	175.41744	0.83607
6.0	232.07472	194.03080	0.83607

x	$F_{5/11}(x)$	$H_{6/11}(x)$	$T_{5/11}(x)$
6.0	232.07472	194.03080	0.83607
6.1	256.69525	214.61577	0.83607
6.2	283.92350	237.38098	0.83607
6.3	314.03538	262.55713	0.83607
6.4	347.33597	290.39927	0.83608
6.5	384.16261	321.18946	0.83608
6.6	424.88830	355.23956	0.83608
6.7	469.92547	392.89439	0.83608
6.8	519.73014	434.53522	0.83608
6.9	574.80653	480.58362	0.83608
7.0	635.71217	531.50574	0.83608
7.1	703.06350	587.81696	0.83608
7.2	777.54210	650.08715	0.83608
7.3	859.90160	718.94640	0.83608
7.4	950.97525	795.09138	0.83608
7.5	1051.68436	879.29237	0.83608
7.6	1163.04758	972.40105	0.83608
7.7	1286.19120	1075.35909	0.83608
7.8	1422.36050	1189.20764	0.83608
7.9	1572.93233	1315.09787	0.83608
8.0	1739.42900	1454.30254	0.83608
8.1	1923.53362	1608.22887	0.83608
8.2	2127.10712	1778.43276	0.83608
8.3	2352.20700	1966.63443	0.83608
8.4	2601.10810	2174.73584	0.83608
8.5	2876.32553	2404.83981	0.83608
8.6	3180.64004	2659.27129	0.83608
8.7	3517.12609	2940.60078	0.83608
8.8	3889.18285	3251.67024	0.83608
8.9	4300.56846	3595.62178	0.83608
9.0	4755.43794	3975.92935	0.83608
9.1	5258.38510	4396.43373	0.83608
9.2	5814.48886	4861.38131	0.83608
9.3	6429.36442	5375.46686	0.83608
9.4	7109.21993	5943.88088	C.83608
9.5	7860.91903	6572.36193	0.83608
9.6	8692.05006	7267.25448	0.83608
9.7	9611.00255	8035.57285	0.83608
9.8	10627.05178	8885.07192	0.83608
9.9	11750.45229	9824.32531	0.83608
10.0	12992.54118	10862.81176	0.83608

TABLE 17B. Lanchester-Clifford-Schläfli Functions $F_{\alpha}(x)$, $H_{1-\alpha}(x)$, and $T_{\alpha}(x)$ for $\alpha = 5/11$ and x from 1.50 to 10.0.

α = 6/11

x	$F_{6/11}(x)$	$H_{5/11}(x)$	$T_{6/11}(x)$	x	$F_{6/11}(x)$	$H_{5/11}(x)$	$T_{6/11}(x)$	x	$F_{6/11}(x)$	$H_{5/11}(x)$	$T_{6/11}(x)$
0.0	1.00000	0.0	0.0	0.50	1.11692	0.65102	0.58287	1.00	1.49664	1.38341	0.92434
0.01	1.00005	0.01781	0.01781	0.51	1.12174	0.66398	0.59192	1.01	1.50743	1.40050	0.92906
0.02	1.00018	0.03344	0.03343	0.52	1.12667	0.67698	0.60087	1.02	1.51837	1.41772	0.93371
0.03	1.00041	0.04835	0.04833	0.53	1.13170	0.69003	0.60973	1.03	1.52945	1.43506	0.93829
0.04	1.00073	0.06281	0.06276	0.54	1.13683	0.70312	0.61849	1.04	1.54067	1.45253	0.94279
0.05	1.00115	0.07695	0.07686	0.55	1.14207	0.71626	0.62716	1.05	1.55203	1.47013	0.94723
0.06	1.00165	0.09084	0.09069	0.56	1.14742	0.72945	0.63573	1.06	1.56354	1.48786	0.95160
0.07	1.00225	0.10452	0.10429	0.57	1.15287	0.74269	0.64421	1.07	1.57520	1.50572	0.95590
0.08	1.00293	0.11804	0.11770	0.58	1.15842	0.75599	0.65260	1.08	1.58700	1.52372	0.96013
0.09	1.00371	0.13142	0.13094	0.59	1.16409	0.76934	0.66089	1.09	1.59895	1.54186	0.96429
0.10	1.00459	0.14468	0.14402	0.60	1.16986	0.78274	0.66909	1.10	1.61106	1.56014	0.96839
0.11	1.00555	0.15783	0.15696	0.61	1.17574	0.79621	0.67720	1.11	1.62331	1.57855	0.97243
0.12	1.00661	0.17089	0.16977	0.62	1.18173	0.80973	0.68521	1.12	1.63571	1.59711	0.97640
0.13	1.00776	0.18387	0.18246	0.63	1.18783	0.82332	0.69313	1.13	1.64827	1.61582	0.98031
0.14	1.00900	0.19678	0.19502	0.64	1.19404	0.83696	0.70095	1.14	1.66099	1.63467	0.98416
0.15	1.01033	0.20962	0.20747	0.65	1.20036	0.85068	0.70869	1.15	1.67386	1.65367	0.98794
0.16	1.01176	0.22240	0.21982	0.66	1.20679	0.86445	0.71633	1.16	1.68688	1.67282	0.99166
0.17	1.01328	0.23514	0.23206	0.67	1.21333	0.87830	0.72388	1.17	1.70007	1.69212	0.99533
0.18	1.01489	0.24783	0.24419	0.68	1.21998	0.89221	0.73133	1.18	1.71341	1.71158	0.99893
0.19	1.01659	0.26048	0.25623	0.69	1.22675	0.90620	0.73870	1.19	1.72692	1.73119	1.00247
0.20	1.01839	0.27309	0.26816	0.70	1.23363	0.92025	0.74597	1.20	1.74059	1.75096	1.00596
0.21	1.02028	0.28568	0.28000	0.71	1.24062	0.93438	0.75316	1.21	1.75442	1.77089	1.00939
0.22	1.02227	0.29824	0.29174	0.72	1.24773	0.94859	0.76025	1.22	1.76842	1.79098	1.01276
0.23	1.02435	0.31078	0.30339	0.73	1.25496	0.96287	0.76725	1.23	1.78258	1.81124	1.01608
0.24	1.02652	0.32330	0.31495	0.74	1.26230	0.97723	0.77417	1.24	1.79691	1.83166	1.01934
0.25	1.02879	0.33580	0.32641	0.75	1.26976	0.99167	0.78099	1.25	1.81141	1.85225	1.02255
0.26	1.03115	0.34830	0.33778	0.76	1.27734	1.00620	0.78773	1.26	1.82608	1.87301	1.02570
0.27	1.03361	0.36078	0.34905	0.77	1.28503	1.02080	0.79438	1.27	1.84092	1.89395	1.02880
0.28	1.03616	0.37326	0.36023	0.78	1.29285	1.03549	0.80094	1.28	1.85594	1.91505	1.03185
0.29	1.03881	0.38574	0.37132	0.79	1.30078	1.05027	0.80741	1.29	1.87113	1.93634	1.03485
0.30	1.04155	0.39821	0.38232	0.80	1.30884	1.06513	0.81380	1.30	1.88650	1.95780	1.03780
0.31	1.04439	0.41069	0.39323	0.81	1.31702	1.08009	0.82010	1.31	1.90204	1.97944	1.04069
0.32	1.04732	0.42317	0.40405	0.82	1.32532	1.09513	0.82632	1.32	1.91777	2.00127	1.04354
0.33	1.05035	0.43565	0.41477	0.83	1.33374	1.11027	0.83245	1.33	1.93367	2.02328	1.04634
0.34	1.05348	0.44815	0.42540	0.84	1.34229	1.12551	0.83850	1.34	1.94976	2.04548	1.04909
0.35	1.05670	0.46066	0.43594	0.85	1.35096	1.14083	0.84446	1.35	1.96603	2.06787	1.05180
0.36	1.06003	0.47318	0.44639	0.86	1.35976	1.15626	0.85034	1.36	1.98249	2.09045	1.05446
0.37	1.06344	0.48572	0.45674	0.87	1.36866	1.17179	0.85614	1.37	1.99913	2.11322	1.05707
0.38	1.06696	0.49827	0.46700	0.88	1.37774	1.18741	0.86186	1.38	2.01597	2.13619	1.05964
0.39	1.07057	0.51085	0.47717	0.89	1.38692	1.20314	0.86749	1.39	2.03299	2.15936	1.06216
0.40	1.07429	0.52345	0.48725	0.90	1.39623	1.21898	0.87305	1.40	2.05021	2.18273	1.06464
0.41	1.07810	0.53607	0.49723	0.91	1.40567	1.23492	0.87853	1.41	2.06762	2.20630	1.06707
0.42	1.08201	0.54871	0.50712	0.92	1.41524	1.25096	0.88392	1.42	2.08522	2.23008	1.06947
0.43	1.08602	0.56139	0.51692	0.93	1.42494	1.26712	0.88924	1.43	2.10302	2.25406	1.07182
0.44	1.09013	0.57409	0.52662	0.94	1.43478	1.28339	0.89448	1.44	2.12102	2.27826	1.07413
0.45	1.09434	0.58682	0.53623	0.95	1.44475	1.29976	0.89965	1.45	2.13923	2.30266	1.07640
0.46	1.09865	0.59959	0.54575	0.96	1.45485	1.31626	0.90474	1.46	2.15763	2.32728	1.07863
0.47	1.10307	0.61239	0.55517	0.97	1.46509	1.33287	0.90975	1.47	2.17624	2.35212	1.08082
0.48	1.10758	0.62523	0.56450	0.98	1.47547	1.34960	0.91469	1.48	2.19505	2.37718	1.08297
0.49	1.11220	0.63811	0.57373	0.99	1.48599	1.36644	0.91955	1.49	2.21408	2.40247	1.08509
0.50	1.11692	0.65102	0.58287	1.00	1.49664	1,38341	0.92434	1.50	2.23331	2.42797	1.08716

TABLE 18A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 6/11$ and x from 0.00 to 1.50.

$\alpha = 6/11$

x	$F_{6/11}(x)$	$H_{5/11}(x)$	$T_{6/11}(x)$
1.50	2.23331	2.42797	1.08716
1.51	2.25275	2.45371	1.08920
1.52	2.27241	2.47967	1.09121
1.53	2.29228	2.50586	1.09317
1.54	2.31237	2.53230	1.09511
1.55	2.33268	2.55896	1.09700
1.56	2.35321	2.58587	1.09887
1.57	2.37397	2.61302	1.10070
1.58	2.39495	2.64042	1.10250
1.59	2.41615	2.66807	1.10426
1.60	2.43759	2.69596	1.10600
1.61	2.45926	2.72411	1.10770
1.62	2.48116	2.75252	1.10937
1.63	2.50330	2.78118	1.11101
1.64	2.52567	2.81011	1.11262
1.65	2.54829	2.83930	1.11420
1.66	2.57114	2.86876	1.11575
1.67	2.59424	2.89849	1.11728
1.68	2.61759	2.92850	1.11878
1.69	2.64119	2.95878	1.12024
1.70	2.66504	2.98934	1.12169
1.71	2.68914	3.02018	1.12310
1.72	2.71350	3.05131	1.12449
1.73	2.73812	3.08273	1.12586
1.74	2.76300	3.11444	1.12720
1.75	2.78814	3.14644	1.12851
1.76	2.81354	3.17874	1.12980
1.77	2.83922	3.21134	1.13107
1.78	2.86517	3.24425	1.13231
1.79	2.89138	3.27747	1.13353
1.80	2.91788	3.31099	1.13473
1.81	2.94465	3.34483	1.13590
1.82	2.97171	3.37899	1.13705
1.83	2.99904	3.41346	1.13818
1.84	3.02667	3.44827	1.13929
1.85	3.05458	3.48340	1.14038
1.86	3.08279	3.51886	1.14145
1.87	3.11128	3.55465	1.14250
1.88	3.14008	3.59078	1.14353
1.89	3.16918	3.62726	1.14454
1.90	3.19858	3.66408	1.14553
1.91	3.22828	3.70125	1.14651
1.92	3.25829	3.73877	1.14746
1.93	3.28862	3.77664	1.14840
1.94	3.31926	3.81488	1.14932
1.55	3.35021	3.85348	1.15022
1.96	3.38149	3.89244	1.15110
1.97	3.41309	3.93178	1.15197
1.98	3.44502	3.97150	1.15282
1.99	3.47728	4.01159	1.15366
2.00	3.50987	4.05206	1.15448

x	$F_{6/11}(x)$	$H_{5/11}(x)$	$T_{6/11}(x)$
2.0	3.50987	4.05206	1.15448
2.1	3.85480	4.47875	1.16186
2.2	4.23674	4.94833	1.16796
2.3	4.65941	5.46539	1.17298
2.4	5.12697	6.03500	1.17711
2.5	5.64397	6.66275	1.18051
2.6	6.21548	7.35478	1.18330
2.7	6.84709	8.11788	1.18559
2.8	7.54500	8.95952	1.18748
2.9	8.31603	9.88796	1.18902
3.0	9.16775	10.91230	1.19029
3.1	10.10851	12.04260	1.19133
3.2	11.14754	13.28993	1.19219
3.3	12.29503	14.66655	1.19288
3.4	13.56224	16.18597	1.19346
3.5	14.96163	17.86311	1.19393
3.6	16.50694	19.71445	1.19431
3.7	18.21335	21.75818	1.19463
3.8	20.09764	24.01440	1.19489
3.9	22.17833	26.50528	1.19510
4.0	24.47588	29.25533	1.19527
4.1	27.01291	32.29161	1.19541
4.2	29.81437	35.64398	1.19553
4.3	32.90785	39.34547	1.19563
4.4	36.32380	43.43250	1.19570
4.5	40.09587	47.94534	1.19577
4.6	44.26122	52.92845	1.19582
4.7	48.86088	58.43092	1.19586
4.8	53.94021	64.50699	1.19590
4.9	59.54927	71.21657	1.19593
5.0	65.74337	78.62581	1.19595
5.1	72.58361	86.80780	1.19597
5.2	80.13746	95.84324	1.19599
5.3	88.47947	105.82130	1.19600
5.4	97.69195	116.84045	1.19601
5.5	107.86585	129.00947	1.19602
5.6	119.10163	142.44850	1.19602
5.7	131.51022	157.29025	1.19603
5.8	145.21419	173.68131	1.19604
5.9	160.34892	191.78361	1.19604
6.0	177.06395	211.77600	1.19604

x	$F_{6/11}(x)$	$H_{5/11}(x)$	$T_{6/11}(x)$
6.0	177.06395	211.77600	1.19604
6.1	195.52444	233.85605	1.19605
6.2	215.91287	258.24199	1.19605
6.3	238.43078	285.17489	1.19605
6.4	263.30080	314.92103	1.19605
6.5	290.76886	347.77456	1.19605
6.6	321.10661	384.06039	1.19605
6.7	354.61615	424.13744	1.19605
6.8	391.62295	468.40220	1.19605
6.9	432.49920	517.29263	1.19605
7.0	477.64739	571.29252	1.19605
7.1	527.51434	630.93633	1.19606
7.2	582.59366	696.81441	1.19606
7.3	643.43061	769.57894	1.19606
7.4	710.62752	849.95034	1.19606
7.5	784.84978	938.72444	1.19606
7.6	866.83243	1036.78041	1.19606
7.7	957.38745	1145.08942	1.19606
7.8	1057.41185	1264.72434	1.19606
7.9	1167.89653	1396.87034	1.19606
8.0	1289.93614	1542.83670	1.19606
8.1	1424.73996	1704.06977	1.19606
8.2	1573.64387	1882.16736	1.19606
8.3	1738.12366	2078.89457	1.19606
8.4	1919.80963	2296.20135	1.19606
8.5	2120.50281	2536.24185	1.19606
8.6	2342.19287	2801.39579	1.19606
8.7	2587.07781	3094.29214	1.19606
8.8	2857.58587	3417.83519	1.19606
8.9	3156.39958	3775.23341	1.19606
9.0	3486.48246	4170.03133	1.19606
9.1	3851.10841	4606.14474	1.19606
9.2	4253.89429	5087.89959	1.19606
9.3	4698.83581	5620.07497	1.19606
9.4	5190.34722	6207.95060	1.19606
9.5	5733.30521	6857.35928	1.19606
9.6	6333.09737	7574.74484	1.19606
9.7	6995.67566	8367.22620	1.19606
9.8	7727.61565	9242.66809	1.19606
9.9	8536.18180	10209.75923	1.19606
10.0	9429.39968	11278.09866	1.19606

TABLE 18B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 6/11$ and x from 1.50 to 10.0.

$\alpha = 8/11$

x	$F_{8/11}(x)$	$H_{3/11}(x)$	$T_{8/11}(x)$
0.0	1.00000	0.0	0.0
0.01	1.00003	0.20379	0.20378
0.02	1.00014	0.29744	0.29740
0.03	1.00031	0.37110	0.37098
0.04	1.00055	0.43421	0.43397
0.05	1.00086	0.49049	0.49007
0.06	1.00124	0.54190	0.54123
0.07	1.00168	0.58958	0.58859
0.08	1.00220	0.63431	0.63292
0.09	1.00279	0.67663	0.67475
0.10	1.00344	0.71692	0.71446
0.11	1.00416	0.75549	0.75236
0.12	1.00496	0.79257	0.78866
0.13	1.00582	0.82834	0.82355
0.14	1.00675	0.86297	0.85719
0.15	1.00775	0.89657	0.88968
0.16	1.00882	0.92926	0.92114
0.17	1.00996	0.96113	0.95165
0.18	1.01116	0.99224	0.98129
0.19	1.01244	1.02268	1.01012
0.20	1.01379	1.05250	1.03819
0.21	1.01521	1.08176	1.06555
0.22	1.01670	1.11049	1.09225
0.23	1.01825	1.13875	1.11833
0.24	1.01988	1.16656	1.14382
0.25	1.02158	1.19397	1.16875
0.26	1.02335	1.22101	1.19314
0.27	1.02519	1.24769	1.21703
0.28	1.02710	1.27406	1.24044
0.29	1.02909	1.30012	1.26338
0.30	1.03114	1.32591	1.28587
0.31	1.03326	1.35145	1.30794
0.32	1.03546	1.37674	1.32959
0.33	1.03773	1.40182	1.35085
0.34	1.04007	1.42669	1.37172
0.35	1.04248	1.45137	1.39222
0.36	1.04497	1.47588	1.41237
0.37	1.04753	1.50023	1.43216
0.38	1.05016	1.52443	1.45162
0.39	1.05286	1.54849	1.47074
0.40	1.05564	1.57243	1.48955
0.41	1.05849	1.59625	1.50805
0.42	1.06142	1.61997	1.52624
0.43	1.06441	1.64360	1.54414
0.44	1.06749	1.66714	1.56174
0.45	1.07064	1.69061	1.57907
0.46	1.07386	1.71400	1.59612
0.47	1.07716	1.73734	1.61290
0.48	1.08053	1.76063	1.62941
0.49	1.08398	1.78387	1.64567
0.50	1.08750	1.80707	1.66167

x	$F_{8/11}(x)$	$H_{3/11}(x)$	$T_{8/11}(x)$
0.50	1.08750	1.80707	1.66167
0.51	1.09111	1.83025	1.67743
0.52	1.09478	1.85340	1.69294
0.53	1.09854	1.87654	1.70821
0.54	1.10237	1.89966	1.72325
0.55	1.10628	1.92278	1.73805
0.56	1.11027	1.94590	1.75263
0.57	1.11434	1.96903	1.76699
0.58	1.11848	1.99216	1.78113
0.59	1.12271	2.01532	1.79506
0.60	1.12701	2.03850	1.80877
0.61	1.13139	2.06171	1.82228
0.62	1.13586	2.08495	1.83558
0.63	1.14040	2.10823	1.84868
0.64	1.14503	2.13155	1.86158
0.65	1.14973	2.15492	1.87428
0.66	1.15452	2.17835	1.88680
0.67	1.15939	2.20182	1.89912
0.68	1.16434	2.22536	1.91126
0.69	1.16938	2.24896	1.92321
0.70	1.17450	2.27264	1.93498
0.71	1.17970	2.29638	1.94658
0.72	1.18499	2.32021	1.95799
0.73	1.19036	2.34411	1.96924
0.74	1.19582	2.36810	1.98031
0.75	1.20137	2.39218	1.99122
0.76	1.20700	2.41635	2.00195
0.77	1.21271	2.44062	2.01253
0.78	1.21852	2.46499	2.02294
0.79	1.22441	2.48946	2.03319
0.80	1.23039	2.51405	2.04329
0.81	1.23646	2.53874	2.05323
0.82	1.24262	2.56355	2.06302
0.83	1.24887	2.58847	2.07266
0.84	1.25521	2.61352	2.08215
0.85	1.26164	2.63870	2.09149
0.86	1.26816	2.66400	2.10069
0.87	1.27477	2.68943	2.10974
0.88	1.28148	2.71500	2.11865
0.89	1.28828	2.74071	2.12743
0.90	1.29517	2.76657	2.13607
0.91	1.30216	2.79256	2.14457
0.92	1.30924	2.81871	2.15294
0.93	1.31642	2.84501	2.16118
0.94	1.32369	2.87146	2.16928
0.95	1.33106	2.89808	2.17726
0.96	1.33853	2.92485	2.18512
0.97	1.34610	2.95180	2.19285
0.98	1.35377	2.97891	2.20046
0.99	1.36153	3.00619	2.20794
1.00	1.36940	3.03364	2.21531

x	$F_{8/11}(x)$	$H_{3/11}(x)$	$T_{8/11}(x)$
1.00	1.36940	3.03364	2.21531
1.01	1.37737	3.06128	2.22256
1.02	1.38544	3.08909	2.22969
1.03	1.39361	3.11709	2.23671
1.04	1.40188	3.14528	2.24361
1.05	1.41026	3.17366	2.25041
1.06	1.41874	3.20223	2.25709
1.07	1.42733	3.23100	2.26367
1.08	1.43602	3.25998	2.27014
1.09	1.44483	3.28915	2.27650
1.10	1.45373	3.31853	2.28276
1.11	1.46275	3.34812	2.28892
1.12	1.47188	3.37793	2.29498
1.13	1.48111	3.40795	2.30094
1.14	1.49046	3.43819	2.30680
1.15	1.49992	3.46865	2.31256
1.16	1.50949	3.49934	2.31823
1.17	1.51917	3.53026	2.32381
1.18	1.52897	3.56141	2.32929
1.19	1.53888	3.59280	2.33468
1.20	1.54891	3.62442	2.33998
1.21	1.55905	3.65629	2.34520
1.22	1.56932	3.68840	2.35032
1.23	1.57970	3.72077	2.35536
1.24	1.59020	3.75338	2.36032
1.25	1.60082	3.78625	2.36519
1.26	1.61156	3.81938	2.36998
1.27	1.62243	3.85277	2.37469
1.28	1.63341	3.88642	2.37933
1.29	1.64453	3.92035	2.38388
1.30	1.65576	3.95454	2.38835
1.31	1.66713	3.98901	2.39275
1.32	1.67862	4.02376	2.39707
1.33	1.69023	4.05880	2.40132
1.34	1.70198	4.09412	2.40550
1.35	1.71386	4.12972	2.40961
1.36	1.72587	4.16562	2.41364
1.37	1.73801	4.20182	2.41761
1.38	1.75028	4.23831	2.42151
1.39	1.76269	4.27511	2.42534
1.40	1.77523	4.31222	2.42910
1.41	1.78791	4.34963	2.43280
1.42	1.80073	4.38736	2.43644
1.43	1.81369	4.42541	2.44001
1.44	1.82678	4.46378	2.44352
1.45	1.84002	4.50247	2.44697
1.46	1.85340	4.54149	2.45036
1.47	1.86692	4.58084	2.45368
1.48	1.88059	4.62053	2.45696
1.49	1.89441	4.66056	2.46017
1.50	1.90837	4.70093	2.46333

TABLE 19A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 8/11$ and x from 0.00 to 1.50.

$\alpha = 8/11$

x	$F_{8/11}(x)$	$H_{3/11}(x)$	$T_{8/11}(x)$
1.50	1.90837	4.70093	2.46333
1.51	1.92248	4.74165	2.46643
1.52	1.93674	4.78272	2.46948
1.53	1.95115	4.82415	2.47247
1.54	1.96571	4.86593	2.47541
1.55	1.98042	4.90808	2.47830
1.56	1.99529	4.95060	2.48114
1.57	2.01032	4.99348	2.48392
1.58	2.02550	5.03674	2.48666
1.59	2.04084	5.08038	2.48935
1.60	2.05635	5.12440	2.49199
1.61	2.07201	5.16880	2.49458
1.62	2.08784	5.21360	2.49713
1.63	2.10383	5.25880	2.49963
1.64	2.11998	5.30439	2.50209
1.65	2.13630	5.35038	2.50450
1.66	2.15280	5.39679	2.50687
1.67	2.16946	5.44360	2.50920
1.68	2.18629	5.49084	2.51149
1.69	2.20329	5.53849	2.51373
1.70	2.22047	5.58657	2.51593
1.71	2.23783	5.63508	2.51810
1.72	2.25536	5.68402	2.52022
1.73	2.27307	5.73340	2.52231
1.74	2.29097	5.78322	2.52436
1.75	2.30904	5.83349	2.52637
1.76	2.32730	5.88421	2.52834
1.77	2.34574	5.93539	2.53028
1.78	2.36437	5.98704	2.53219
1.79	2.38319	6.03914	2.53406
1.80	2.40220	6.09172	2.53589
1.81	2.42140	6.14478	2.53769
1.82	2.44080	6.19831	2.53946
1.83	2.46039	6.25233	2.54120
1.84	2.48018	6.30684	2.54290
1.85	2.50016	6.36185	2.54457
1.86	2.52035	6.41736	2.54622
1.87	2.54074	6.47337	2.54783
1.88	2.56133	6.52989	2.54941
1.89	2.58213	6.58693	2.55096
1.90	2.60314	6.64449	2.55249
1.91	2.62436	6.70258	2.55398
1.92	2.64579	6.76119	2.55545
1.93	2.66743	6.82035	2.55690
1.94	2.68929	6.88004	2.55831
1.95	2.71137	6.94029	2.55970
1.96	2.73366	7.00108	2.56106
1.97	2.75618	7.06244	2.56240
1.98	2.77892	7.12436	2.56371
1.99	2.80189	7.18684	2.56500
2.00	2.82508	7.24991	2.56627

x	$F_{8/11}(x)$	$H_{3/11}(x)$	$T_{8/11}(x)$
2.0	2.82508	7.24991	2.56627
2.1	3.06999	7.91347	2.57769
2.2	3.34005	8.64118	2.58714
2.3	3.63768	9.43961	2.59496
2.4	3.96553	10.31597	2.60141
2.5	4.32655	11.27817	2.60673
2.6	4.72398	12.33490	2.61112
2.7	5.16140	13.49570	2.61474
2.8	5.64274	14.77107	2.61771
2.9	6.17235	16.17255	2.62016
3.0	6.75502	17.71284	2.62218
3.1	7.39603	19.40592	2.62383
3.2	8.10119	21.26717	2.62519
3.3	8.87692	23.31353	2.62631
3.4	9.73028	25.56363	2.62722
3.5	10.66904	28.03801	2.62798
3.6	11.70179	30.75927	2.62860
3.7	12.83796	33.75231	2.62910
3.8	14.08796	37.04456	2.62952
3.9	15.46326	40.66622	2.62986
4.0	16.97650	44.65057	2.63014
4.1	18.64158	49.03427	2.63037
4.2	20.47386	53.85769	2.63056
4.3	22.49022	59.16532	2.63071
4.4	24.70929	65.00619	2.63084
4.5	27.15159	71.43430	2.63094
4.6	29.83973	78.50918	2.63103
4.7	32.79861	86.29638	2.63110
4.8	36.05571	94.86817	2.63116
4.9	39.64127	104.30420	2.63120
5.0	43.58864	114.69220	2.63124
5.1	47.93457	126.12890	2.63127
5.2	52.71956	138.72088	2.63130
5.3	57.98826	152.58561	2.63132
5.4	63.78986	167.85258	2.63134
5.5	70.17859	184.66448	2.63135
5.6	77.21423	203.17861	2.63136
5.7	84.96267	223.56837	2.63137
5.8	93.49653	246.02487	2.63138
5.9	102.89588	270.75878	2.63139
6.0	113.24897	298.00235	2.63139

x	$F_{8/11}(x)$	$H_{3/11}(x)$	$T_{8/11}(x)$
6.0	113.24897	298.00235	2.63139
6.1	124.65310	328.01160	2.63140
6.2	137.21551	361.06877	2.63140
6.3	151.05446	397.48501	2.63140
6.4	166.30031	437.60336	2.63140
6.5	183.09678	481.80202	2.63141
6.6	201.60233	530.49796	2.63141
6.7	221.99168	584.15092	2.63141
6.8	244.45744	643.26779	2.63141
6.9	269.21201	708.40747	2.63141
7.0	296.48960	780.18621	2.63141
7.1	326.54842	859.28354	2.63141
7.2	359.67322	946.44874	2.63141
7.3	396.17800	1042.50804	2.63141
7.4	436.40900	1148.37254	2.63141
7.5	480.74802	1265.04698	2.63141
7.6	529.61612	1393.63930	2.63141
7.7	583.47764	1535.37136	2.63141
7.8	642.84465	1691.59063	2.63141
7.9	708.28186	1863.78312	2.63141
8.0	780.41208	2053.58771	2.63141
8.1	859.92219	2262.81185	2.63141
8.2	947.56974	2493.44896	2.63141
8.3	1044.19024	2747.69760	2.63141
8.4	1150.70518	3027.98264	2.63141
8.5	1268.13095	3336.97859	2.63141
8.6	1397.58856	3677.63533	2.63141
8.7	1540.31451	4053.20654	2.63141
8.8	1697.67262	4467.28105	2.63141
8.9	1871.16724	4923.81741	2.63141
9.0	2062.45773	5427.18208	2.63141
9.1	2273.37443	5982.19147	2.63141
9.2	2505.93638	6594.15848	2.63141
9.3	2762.37073	7268.94369	2.63141
9.4	3045.13429	8013.01197	2.63141
9.5	3356.93721	8833.49486	2.63141
9.6	3700.76916	9738.25943	2.63141
9.7	4079.92823	10735.98430	2.63141
9.8	4498.05276	11836.24347	2.63141
9.9	4959.15653	13049.59883	2.63141
10.0	5467.66752	14387.70229	2.63141

TABLE 19B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 8/11$ and x from 1.50 to 10.0.

$\alpha = 5/13$

x	$F_{5/13}(x)$	$H_{8/13}(x)$	$T_{5/13}(x)$	x	$F_{5/13}(x)$	$H_{8/13}(x)$	$T_{5/13}(x)$	x	$F_{5/13}(x)$	$H_{8/13}(x)$	$T_{5/13}(x)$
0.0	1.00000	0.0	0.0	C.50	1.16620	0.30658	0.26288	1.00	1.71077	0.80479	0.47043
0.01	1.00007	0.00239	0.00239	0.51	1.17307	0.31462	0.26820	1.01	1.72635	0.81711	0.47332
0.02	1.00026	0.00561	0.00561	0.52	1.18009	0.32274	0.27349	1.02	1.74213	C.82953	0.47616
0.03	1.00059	0.00925	0.00924	0.53	1.18726	0.33092	0.27873	1.03	1.75813	0.84207	0.47896
0.04	1.00104	0.01318	0.01317	0.54	1.19458	0.33918	0.28393	1.04	1.77434	0.85472	0.48171
0.05	1.00163	0.01735	0.01732	0.55	1.20205	0.34750	0.28909	1.05	1.79076	0.86748	0.48442
0.06	1.00234	0.02172	0.02167	0.56	1.20967	0.35589	0.29420	1.06	1.80739	0.88036	0.48709
0.C7	1.00319	0.02626	0.02617	0.57	1.21745	0.36435	0.29928	1.07	1.82425	0.89335	0.48971
0.08	1.00416	0.03096	0.03083	C.58	1.22538	0.37289	0.30430	1.08	1.84132	0.90646	0.49229
0.09	1.00527	0.03579	0.03561	0.59	1.23346	0.38149	0.30929	1.09	1.85861	0.91969	0.49483
0.10	1.00651	0.04076	0.04050	0.60	1.24170	0.39017	0.31422	1.10	1.87613	0.93304	0.49732
0.11	1.00787	0.04585	0.04549	0.61	1.25010	0.39892	0.31911	1.11	1.89387	0.94651	0.49978
0.12	1.00937	0.05105	0.05058	0.62	1.25865	0.40774	0.32395	1.12	1.91184	C.96011	0.50219
0.13	1.01100	0.05636	0.05575	0.63	1.26736	0.41664	0.32875	1.13	1.93003	0.97382	0.50456
0.14	1.01276	0.06177	0.06099	C.64	1.27623	0.42561	0.33349	1.14	1.94846	0.98767	0.50690
0.15	1.01465	0.06727	0.06630	C.65	1.28526	0.43466	0.33819	1.15	1.96712	1.00164	0.50919
0.16	1.01668	0.07287	0.07167	0.66	1.29445	0.44378	0.34283	1.16	1.98601	1.01574	0.51145
0.17	1.01883	0.07855	0.07710	0.67	1.30380	0.45297	0.34743	1.17	2.00514	1.02997	0.51366
0.18	1.02112	0.08432	0.08258	0.68	1.31331	0.46225	0.35197	1.18	2.02451	1.04433	0.51584
0.19	1.02354	0.09018	0.08810	0.69	1.32299	0.47160	0.35647	1.19	2.04412	1.05882	0.51798
0.20	1.02609	0.09611	0.09367	C.70	1.33283	0.48103	0.36091	1.20	2.06397	1.07345	C.52009
0.21	1.02878	0.10212	0.09927	0.71	1.34284	0.49054	0.36530	1.21	2.08406	1.08821	0.52216
0.22	1.03160	0.10821	0.10490	C.72	1.35302	0.50014	0.36964	1.22	2.10441	1.10311	0.52419
0.23	1.03455	0.11438	0.11056	0.73	1.36336	0.50981	0.37393	1.23	2.12500	1.11814	0.52619
0.24	1.03764	0.12062	0.11624	0.74	1.37388	0.51956	0.37817	1.24	2.14584	1.13332	0.52815
0.25	1.04085	0.12693	0.12194	0.75	1.38456	0.52940	0.38236	1.25	2.16694	1.14864	0.53008
0.26	1.04421	0.13331	0.12766	0.76	1.39542	0.53932	0.38649	1.26	2.18829	1.16411	0.53197
0.27	1.04770	0.13976	0.13340	0.77	1.40645	0.54932	0.39057	1.27	2.20990	1.17971	0.53383
0.28	1.05132	0.14628	0.13914	0.78	1.41765	0.55941	0.39460	1.28	2.23178	1.19547	0.53566
0.29	1.05508	0.15287	0.14489	C.79	1.42903	0.56958	0.39858	1.29	2.25391	1.21137	0.53745
0.30	1.05898	0.15953	0.15065	0.80	1.44058	0.57984	0.40251	1.30	2.27631	1.22742	0.53922
0.31	1.06301	0.16626	0.15640	0.81	1.45231	0.59019	0.40638	1.31	2.29898	1.24363	0.54095
0.32	1.06718	0.17305	0.16216	0.82	1.46422	0.60063	0.41020	1.32	2.32192	1.25998	0.54265
0.33	1.07148	0.17991	0.16791	C.83	1.47631	0.61116	0.41398	1.33	2.34513	1.27649	0.54432
0.34	1.07593	0.18683	0.17365	0.84	1.48859	0.62177	0.41770	1.34	2.36861	1.29316	0.54596
0.35	1.08051	0.19383	0.17938	0.85	1.50104	0.63248	0.42136	1.35	2.39237	1.30999	0.54757
0.36	1.08523	C.20088	0.18511	0.86	1.51368	0.64329	0.42498	1.36	2.41642	1.32697	0.54915
0.37	1.09009	0.20801	0.19082	0.87	1.52650	0.65418	0.42855	1.37	2.44074	1.34412	0.55070
0.38	1.09509	0.21519	0.19651	0.88	1.53952	0.66517	0.43206	1.38	2.46535	1.36143	0.55223
0.39	1.10023	0.22245	0.20218	0.89	1.55272	0.67625	0.43553	1.39	2.49025	1.37891	0.55372
C.40	1.10551	0.22977	0.20784	0.90	1.56611	0.68744	0.43895	1.40	2.51544	1.39655	0.55519
0.41	1.11093	0.23715	0.21347	0.91	1.57969	0.69872	0.44231	1.41	2.54092	1.41436	0.55663
0.42	1.11650	0.24460	0.21908	0.92	1.59346	0.71009	0.44563	1.42	2.56670	1.43235	0.55805
0.43	1.12220	0.25212	0.22466	0.93	1.60743	0.72157	0.44890	1.43	2.59278	1.45050	0.55944
0.44	1.12805	0.25970	0.23022	0.94	1.62159	0.73315	0.45212	1.44	2.61916	1.46883	0.56080
0.45	1.13405	0.26734	0.23574	0.95	1.63595	0.74483	0.45529	1.45	2.64584	1.48734	0.56214
0.46	1.14019	0.27506	0.24124	0.96	1.65051	0.75661	0.45841	1.46	2.67283	1.50602	0.56346
0.47	1.14647	0.28284	0.24670	0.97	1.66527	0.76850	0.46148	1.47	2.70013	1.52489	0.56475
0.48	1.15290	0.29068	0.25213	0.98	1.68023	0.78049	0.46451	1.48	2.72775	1.54393	0.56601
0.49	1.15948	0.29859	0.25753	C.99	1.69540	0.79259	0.46749	1.49	2.75568	1.56317	0.56725
C.50	1.16620	0.30658	0.26288	1.0C	1.71077	0.80479	0.47043	1.50	2.78392	1.58258	0.56847

TABLE 20A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/13$ and x from 0.00 to 1.50.

$\alpha = 5/13$

x	$F_{5/13}(x)$	$H_{8/13}(x)$	$T_{5/13}(x)$
1.50	2.78392	1.58258	0.56847
1.51	2.81250	1.60219	0.56967
1.52	2.84139	1.62199	0.57084
1.53	2.87062	1.64197	0.57199
1.54	2.90017	1.66216	0.57312
1.55	2.93006	1.68254	0.57423
1.56	2.96029	1.70311	0.57532
1.57	2.99086	1.72389	0.57639
1.58	3.02177	1.74488	0.57743
1.59	3.05304	1.76606	0.57846
1.60	3.08465	1.78746	0.57947
1.61	3.11661	1.80906	0.58046
1.62	3.14894	1.83088	0.58143
1.63	3.18162	1.85291	0.58238
1.64	3.21467	1.87516	0.58331
1.65	3.24809	1.89763	0.58423
1.66	3.28188	1.92032	0.58513
1.67	3.31605	1.94323	0.58601
1.68	3.35059	1.96637	0.58687
1.69	3.38552	1.98973	0.58772
1.70	3.42083	2.01333	0.58855
1.71	3.45654	2.03716	0.58936
1.72	3.49264	2.06123	0.59016
1.73	3.52913	2.08554	0.59095
1.74	3.56603	2.11008	0.59172
1.75	3.60334	2.13487	0.59247
1.76	3.64105	2.15991	0.59321
1.77	3.67918	2.18520	0.59394
1.78	3.71772	2.21074	0.59465
1.79	3.75669	2.23653	0.59535
1.80	3.79608	2.26258	0.59603
1.81	3.83591	2.28889	0.59670
1.82	3.87617	2.31546	0.59736
1.83	3.91686	2.34229	0.59800
1.84	3.95801	2.36940	0.59863
1.85	3.99959	2.39678	0.59925
1.86	4.04163	2.42443	0.59986
1.87	4.08413	2.45235	0.60046
1.88	4.12709	2.48056	0.60104
1.89	4.17052	2.50905	0.60162
1.90	4.21441	2.53783	0.60218
1.91	4.25878	2.56689	0.60273
1.92	4.30363	2.59625	0.60327
1.93	4.34896	2.62590	0.60380
1.94	4.39479	2.65585	0.60432
1.95	4.44110	2.68610	0.60483
1.96	4.48792	2.71666	0.60533
1.97	4.53524	2.74752	0.60582
1.98	4.58307	2.77870	0.60630
1.99	4.63142	2.81019	0.60677
2.00	4.68028	2.84199	0.60723

x	$F_{5/13}(x)$	$H_{8/13}(x)$	$T_{5/13}(x)$
2.0	4.68028	2.84199	0.60723
2.1	5.19867	3.17830	0.61137
2.2	5.77510	3.55030	0.61476
2.3	6.41571	3.96194	0.61754
2.4	7.12731	4.41759	0.61981
2.5	7.91747	4.92206	0.62167
2.6	8.79455	5.48070	0.62319
2.7	9.76786	6.09941	0.62444
2.8	10.84770	6.78474	0.62545
2.9	12.04548	7.54392	0.62629
3.0	13.37387	8.38497	0.62697
3.1	14.84689	9.31675	0.62752
3.2	16.48004	10.34909	0.62798
3.3	18.29055	11.49285	0.62835
3.4	20.29746	12.76006	0.62865
3.5	22.52187	14.16403	0.62890
3.6	24.98714	15.71952	0.62910
3.7	27.71914	17.44284	0.62927
3.8	30.74651	19.35205	0.62941
3.9	34.10098	21.46717	0.62952
4.0	37.81766	23.81032	0.62961
4.1	41.93541	26.40601	0.62968
4.2	46.49729	29.28137	0.62974
4.3	51.55094	32.46644	0.62979
4.4	57.14910	35.99445	0.62983
4.5	63.35016	39.90219	0.62987
4.6	70.21874	44.23040	0.62989
4.7	77.82641	49.02416	0.62992
4.8	86.25233	54.33336	0.62994
4.9	95.58417	60.21324	0.62995
5.0	105.91894	66.72492	0.62996
5.1	117.36404	73.93607	0.62997
5.2	130.03830	81.92156	0.62998
5.3	144.07328	90.76428	0.62999
5.4	159.61456	100.55596	0.62999
5.5	176.82328	111.39811	0.63000
5.6	195.87776	123.40309	0.63000
5.7	216.97536	136.69524	0.63000
5.8	240.33449	151.41217	0.63001
5.9	266.19687	167.70615	0.63001
6.0	294.82997	185.74572	0.63001

x	$F_{5/13}(x)$	$H_{8/13}(x)$	$T_{5/13}(x)$
6.0	294.82997	185.74572	0.63001
6.1	326.52983	205.71737	0.63001
6.2	361.62402	227.82750	0.63001
6.3	400.47505	252.30447	0.63001
6.4	443.48405	279.40103	0.63001
6.5	491.09493	309.39683	0.63001
6.6	543.79888	342.60134	0.63001
6.7	602.13944	379.35700	0.63002
6.8	666.71805	420.04272	0.63002
6.9	738.20021	465.07779	0.63002
7.0	817.32232	514.92615	0.63002
7.1	904.89918	570.10114	0.63002
7.2	1001.83236	631.17076	0.63002
7.3	1109.11941	698.76349	0.63002
7.4	1227.86410	773.57472	0.63002
7.5	1359.28765	856.37385	0.63002
7.6	1504.74128	948.01216	0.63002
7.7	1665.71999	1049.43153	0.63002
7.8	1843.87788	1161.67407	0.63002
7.9	2041.04502	1285.89276	0.63002
8.0	2259.24617	1423.36323	0.63002
8.1	2500.72147	1575.49680	0.63002
8.2	2767.94933	1743.85493	0.63002
8.3	3063.67175	1930.16511	0.63002
8.4	3390.92229	2136.33854	0.63002
8.5	3753.05709	2364.48964	0.63002
8.6	4153.78911	2616.95765	0.63002
8.7	4597.22603	2896.33048	0.63002
8.8	5087.91219	3205.47112	0.63002
8.9	5630.87494	3547.54690	0.63002
9.0	6231.67594	3926.06177	0.63002
9.1	6896.46790	4344.89202	0.63002
9.2	7632.05733	4808.32589	0.63002
9.3	8445.97396	5321.10723	0.63002
9.4	9346.54752	5888.48390	0.63002
9.5	10342.99263	6516.26128	0.63002
9.6	11445.50277	7210.86144	0.63002
9.7	12665.35416	7979.38858	0.63002
9.8	14015.02067	8829.70145	0.63002
9.9	15508.30090	9770.49341	0.63002
10.0	17160.45881	10811.38101	0.63002

TABLE 20B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/13$ and x from 1.50 to 10.0.

α = 8/13

x	$F_{8/13}(x)$	$H_{5/13}(x)$	$T_{8/13}(x)$	x	$F_{8/13}(x)$	$H_{5/13}(x)$	$T_{8/13}(x)$	x	$F_{8/13}(x)$	$H_{5/13}(x)$	$T_{8/13}(x)$
0.00	1.00000	0.0	0.0	C.5C	1.10354	0.93599	0.84817	1.00	1.43871	1.81573	1.26206
0.01	1.00004	0.04415	0.04415	0.51	1.10781	0.95206	0.85941	1.01	1.44821	1.83588	1.26769
0.02	1.00016	0.07526	0.07524	0.52	1.11217	0.96815	0.87051	1.02	1.45784	1.85616	1.27323
0.03	1.00037	0.10281	0.10277	0.53	1.11662	0.98427	0.88147	1.03	1.46759	1.87658	1.27868
0.04	1.00065	0.12829	0.12821	0.54	1.12116	1.00041	0.89230	1.04	1.47747	1.89714	1.28405
0.05	1.00102	0.15234	0.15219	C.55	1.12580	1.01659	0.90300	1.05	1.48747	1.91785	1.28933
0.06	1.00146	0.17531	0.17506	0.56	1.13052	1.03280	0.91356	1.06	1.49760	1.93870	1.29454
0.07	1.00199	0.19743	0.19704	0.57	1.13534	1.04904	0.92399	1.07	1.50786	1.95970	1.29966
0.08	1.00260	0.21884	0.21828	0.58	1.14026	1.06533	0.93429	1.08	1.51824	1.98085	1.30470
0.09	1.00329	0.23967	0.23889	0.59	1.14527	1.08166	0.94446	1.09	1.52875	2.00215	1.30966
0.10	1.00407	0.25999	0.25894	0.60	1.15037	1.09803	0.95450	1.10	1.53940	2.02361	1.31455
0.11	1.00492	0.27988	0.27851	0.61	1.15557	1.11444	0.96441	1.11	1.55018	2.04523	1.31935
0.12	1.00586	0.29938	0.29763	0.62	1.16086	1.13091	0.97420	1.12	1.56109	2.06700	1.32408
0.13	1.00687	0.31953	0.31636	0.63	1.16626	1.14743	0.98386	1.13	1.57213	2.08894	1.32873
0.14	1.00797	0.33738	0.33471	0.64	1.17174	1.16400	0.99339	1.14	1.58331	2.11104	1.33331
0.15	1.00916	0.35596	0.35273	0.65	1.17733	1.18063	1.00281	1.15	1.59462	2.13331	1.33782
0.16	1.01042	0.37428	0.37042	0.66	1.18301	1.19732	1.01210	1.16	1.60607	2.15574	1.34225
0.17	1.01177	0.39239	0.38782	C.67	1.18879	1.21407	1.02126	1.17	1.61765	2.17835	1.34661
0.18	1.01320	0.41028	0.40494	0.68	1.19467	1.23088	1.03031	1.18	1.62938	2.20113	1.35090
0.19	1.01471	0.42799	0.42179	0.69	1.20065	1.24776	1.03924	1.19	1.64125	2.22408	1.35512
0.20	1.01630	0.44553	0.43838	0.70	1.20673	1.26471	1.04805	1.20	1.65325	2.24721	1.35927
0.21	1.01798	0.46291	0.45473	0.71	1.21291	1.28173	1.05674	1.21	1.66540	2.27053	1.36335
0.22	1.01974	0.48014	0.47085	0.72	1.21919	1.29882	1.06531	1.22	1.67769	2.29402	1.36737
0.23	1.02158	0.49725	0.48674	0.73	1.22557	1.31598	1.07377	1.23	1.69013	2.31770	1.37132
0.24	1.02350	0.51423	0.50242	0.74	1.23206	1.33323	1.08211	1.24	1.70271	2.34157	1.37520
0.25	1.02551	0.53110	0.51789	0.75	1.23864	1.35055	1.09034	1.25	1.71544	2.36562	1.37902
0.26	1.02761	0.54787	0.53315	0.76	1.24533	1.36795	1.09846	1.26	1.72832	2.38987	1.38278
0.27	1.02978	0.56455	0.54822	0.77	1.25213	1.38544	1.10647	1.27	1.74134	2.41432	1.38647
0.28	1.03204	0.58114	0.56309	0.78	1.25903	1.40301	1.11436	1.28	1.75452	2.43895	1.39010
0.29	1.03439	0.59765	0.57778	C.79	1.26603	1.42067	1.12215	1.29	1.76785	2.46379	1.39367
0.30	1.03682	0.61409	0.59228	0.80	1.27314	1.43843	1.12982	1.30	1.78133	2.48883	1.39718
0.31	1.03933	0.63046	0.60660	0.81	1.28036	1.45627	1.13739	1.31	1.79496	2.51408	1.40063
0.32	1.04193	0.64678	0.62075	0.82	1.28768	1.47421	1.14485	1.32	1.80875	2.53953	1.40403
C.33	1.04461	0.66304	0.63473	0.83	1.29512	1.49225	1.15221	1.33	1.82270	2.56519	1.40736
0.34	1.04738	0.67926	0.64853	0.84	1.30266	1.51038	1.15946	1.34	1.83680	2.59106	1.41064
0.35	1.05024	0.69543	0.66217	C.85	1.31031	1.52862	1.16661	1.35	1.85106	2.61715	1.41386
0.36	1.05318	0.71157	0.67564	0.86	1.31807	1.54696	1.17365	1.36	1.86549	2.64346	1.41703
0.37	1.05621	0.72768	0.68895	0.87	1.32594	1.56540	1.18060	1.37	1.88007	2.66998	1.42015
0.38	1.05932	0.74376	0.70211	0.88	1.33392	1.58395	1.18744	1.38	1.89482	2.69672	1.42321
0.39	1.06252	0.75981	0.71510	0.89	1.34202	1.60261	1.19418	1.39	1.90974	2.72369	1.42621
0.40	1.06581	0.77585	0.72794	0.90	1.35023	1.62139	1.20083	1.40	1.92482	2.75089	1.42917
0.41	1.06918	0.79187	0.74063	0.91	1.35855	1.64027	1.20737	1.41	1.94007	2.77832	1.43208
0.42	1.07265	0.80788	0.75316	0.92	1.36699	1.65928	1.21382	1.42	1.95548	2.80598	1.43493
0.43	1.07620	0.82388	0.76555	0.93	1.37554	1.67840	1.22018	1.43	1.97107	2.83388	1.43774
0.44	1.07984	0.83988	0.77778	0.94	1.38421	1.69764	1.22643	1.44	1.98683	2.86201	1.44049
0.45	1.08356	0.85588	0.78987	0.95	1.39299	1.71700	1.23260	1.45	2.00276	2.89039	1.44320
0.46	1.08738	0.87188	0.80182	0.96	1.40196	1.73649	1.23867	1.46	2.01887	2.91901	1.44586
C.47	1.09129	0.88789	0.81362	0.97	1.41098	1.75611	1.24466	1.47	2.03515	2.94787	1.44848
0.48	1.09528	0.90391	0.82528	0.98	1.42006	1.77585	1.25055	1.48	2.05161	2.97699	1.45105
0.49	1.09937	0.91994	0.83679	0.99	1.42932	1.79573	1.25635	1.49	2.06825	3.00635	1.45357
0.50	1.10354	0.93599	0.84817	1.00	1.43871	1.81573	1.26206	1.50	2.08507	3.03597	1.45605

TABLE 21A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 8/13$ and x from 0.00 to 1.50.

$\alpha = 8/13$

x	$F_{8/13}(x)$	$H_{5/13}(x)$	$T_{8/13}(x)$
1.50	2.08507	3.03597	1.45605
1.51	2.10208	3.06585	1.45849
1.52	2.11926	3.09599	1.46084
1.53	2.13664	3.12640	1.46323
1.54	2.15420	3.15707	1.46554
1.55	2.17195	3.18801	1.46781
1.56	2.18989	3.21922	1.47004
1.57	2.20802	3.25071	1.47223
1.58	2.22635	3.28248	1.47438
1.59	2.24487	3.31452	1.47649
1.60	2.26359	3.34686	1.47856
1.61	2.28251	3.37948	1.48060
1.62	2.30163	3.41239	1.48260
1.63	2.32095	3.44560	1.48456
1.64	2.34048	3.47910	1.48649
1.65	2.36021	3.51290	1.48839
1.66	2.38015	3.54701	1.49024
1.67	2.40031	3.58143	1.49207
1.68	2.42067	3.61615	1.49386
1.69	2.44125	3.65119	1.49562
1.70	2.46204	3.68655	1.49735
1.71	2.48305	3.72222	1.49905
1.72	2.50429	3.75822	1.50072
1.73	2.52574	3.79455	1.50235
1.74	2.54742	3.83121	1.50396
1.75	2.56932	3.86820	1.50554
1.76	2.59145	3.90553	1.50708
1.77	2.61381	3.94321	1.50860
1.78	2.63641	3.98122	1.51009
1.79	2.65923	4.01959	1.51156
1.80	2.68230	4.05831	1.51300
1.81	2.70560	4.09738	1.51441
1.82	2.72914	4.13681	1.51579
1.83	2.75293	4.17661	1.51715
1.84	2.77696	4.21677	1.51849
1.85	2.80124	4.25731	1.51980
1.86	2.82577	4.29822	1.52108
1.87	2.85055	4.33951	1.52234
1.88	2.87558	4.38118	1.52358
1.89	2.90087	4.42324	1.52480
1.90	2.92642	4.46569	1.52599
1.91	2.95223	4.50853	1.52716
1.92	2.97831	4.55177	1.52831
1.93	3.00465	4.59542	1.52944
1.94	3.03126	4.63947	1.53054
1.95	3.05814	4.68394	1.53163
1.96	3.08530	4.72882	1.53269
1.57	3.11273	4.77412	1.53374
1.98	3.14044	4.81984	1.53376
1.99	3.16843	4.86599	1.53577
2.00	3.19671	4.91258	1.53676

x	$F_{8/13}(x)$	$H_{5/13}(x)$	$T_{8/13}(x)$
2.0	3.19671	4.91258	1.53676
2.1	3.49571	5.40323	1.54567
2.2	3.82624	5.94230	1.55304
2.3	4.19142	6.53491	1.55912
2.4	4.59469	7.18668	1.56413
2.5	5.03987	7.90380	1.56826
2.6	5.53117	8.69307	1.57165
2.7	6.07324	9.56199	1.57445
2.8	6.67122	10.51881	1.57674
2.9	7.33080	11.57263	1.57863
3.0	8.05822	12.73345	1.58018
3.1	8.86041	14.01234	1.58145
3.2	9.74501	15.42147	1.58250
3.3	10.72043	16.97426	1.58336
3.4	11.79598	18.68553	1.58406
3.5	12.98191	20.57160	1.58464
3.6	14.28955	22.65049	1.58511
3.7	15.73139	24.94208	1.58550
3.8	17.32123	27.46827	1.58582
3.9	19.07428	30.25325	1.58608
4.0	21.00732	33.32370	1.58629
4.1	23.13890	36.70904	1.58646
4.2	25.48944	40.44175	1.58661
4.3	28.08152	44.55766	1.58673
4.4	30.94002	49.09631	1.58682
4.5	34.09242	54.10130	1.58690
4.6	37.56904	59.62078	1.58697
4.7	41.40333	65.70786	1.58702
4.8	45.63221	72.42114	1.58706
4.9	50.29641	79.82531	1.58710
5.0	55.44091	87.99175	1.58713
5.1	61.11532	96.99921	1.58715
5.2	67.37439	106.93463	1.58717
5.3	74.27857	117.89393	1.58719
5.4	81.89456	129.98298	1.58720
5.5	90.29595	143.31864	1.58721
5.6	99.56399	158.02985	1.58722
5.7	109.78835	174.25893	1.58723
5.8	121.06799	192.16298	1.58723
5.9	133.51213	211.91536	1.58724
6.0	147.24132	233.70743	1.58724

x	$F_{8/13}(x)$	$H_{5/13}(x)$	$T_{8/13}(x)$
6.0	147.24132	233.70743	1.58724
6.1	162.38864	257.75040	1.58724
6.2	179.10095	284.27738	1.58725
6.3	197.54035	313.54569	1.58725
6.4	217.88578	345.83935	1.58725
6.5	240.33475	381.47183	1.58725
6.6	265.10526	420.78920	1.58725
6.7	292.43796	464.17341	1.58725
6.8	322.59848	512.04609	1.58726
6.9	355.88005	564.87266	1.58726
7.0	392.60634	623.16688	1.58726
7.1	433.13464	687.49587	1.58726
7.2	477.85938	758.48568	1.58726
7.3	527.21594	836.82740	1.58726
7.4	581.68499	923.28393	1.58726
7.5	641.79710	1018.69746	1.58726
7.6	708.13802	1123.99772	1.58726
7.7	781.35438	1240.21108	1.58726
7.8	862.16003	1368.47060	1.58726
7.9	951.34305	1510.02717	1.58726
8.0	1049.77346	1666.26172	1.58726
8.1	1158.41174	1838.69881	1.58726
8.2	1278.31828	2029.02154	1.58726
8.3	1410.66376	2239.08810	1.58726
8.4	1556.74065	2470.94993	1.58726
8.5	1717.97585	2726.87193	1.58726
8.6	1895.94474	3009.35463	1.58726
8.7	2092.38662	3321.15873	1.58726
8.8	2309.22178	3665.33224	1.58726
8.9	2548.57034	4045.24035	1.58726
9.0	2812.77312	4464.59853	1.58726
9.1	3104.41456	4927.50896	1.58726
9.2	3426.34815	5438.50086	1.58726
9.3	3781.72443	6002.57496	1.58726
9.4	4174.02197	6625.25267	1.58726
9.5	4607.08154	7312.63026	1.58726
9.6	5085.14387	8071.43885	1.58726
9.7	5612.89127	8909.11053	1.58726
9.8	6195.49377	9833.85142	1.58726
9.9	6838.65982	10854.72236	1.58726
10.0	7548.69254	11981.72798	1.58726

TABLE 21B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 8/13$ and x from 1.50 to 10.0.

$\alpha = 5/17$

x	$F_{5/17}(x)$	$H_{12/17}(x)$	$T_{5/17}(x)$
0.0	1.00000	0.0	0.0
0.01	1.00009	0.00080	0.00080
0.02	1.00034	0.00213	0.00213
0.03	1.00077	0.00377	0.00377
0.04	1.00136	0.00566	0.00565
0.05	1.00213	0.00776	0.00774
0.06	1.00306	0.01004	0.01001
0.07	1.00417	0.01248	0.01243
0.08	1.00544	0.01507	0.01499
0.09	1.00689	0.01780	0.01768
0.10	1.00851	0.02066	0.02049
0.11	1.01030	0.02364	0.02340
0.12	1.01226	0.02674	0.02642
0.13	1.01439	0.02995	0.02953
0.14	1.01669	0.03327	0.03272
0.15	1.01917	0.03669	0.03600
0.16	1.02181	0.04021	0.03935
0.17	1.02463	0.04382	0.04277
0.18	1.02763	0.04753	0.04625
0.19	1.03079	0.05133	0.04979
0.20	1.03413	0.05521	0.05339
0.21	1.03764	0.05919	0.05704
0.22	1.04133	0.06324	0.06073
0.23	1.04520	0.06738	0.06447
0.24	1.04923	0.07161	0.06825
0.25	1.05345	0.07591	0.07206
0.26	1.05786	0.08029	0.07590
0.27	1.06240	0.08475	0.07977
0.28	1.06715	0.08929	0.08367
0.29	1.07207	0.09390	0.08759
0.30	1.07717	0.09859	0.09152
0.31	1.08245	0.10335	0.09548
0.32	1.08790	0.10819	0.09944
0.33	1.09354	0.11310	0.10342
0.34	1.09936	0.11808	0.10741
0.35	1.10536	0.12314	0.11140
0.36	1.11155	0.12826	0.11539
0.37	1.11791	0.13347	0.11939
0.38	1.12446	0.13874	0.12338
0.39	1.13119	0.14408	0.12737
0.40	1.13811	0.14949	0.13135
0.41	1.14522	0.15498	0.13533
0.42	1.15251	0.16054	0.13929
0.43	1.15999	0.16616	0.14325
0.44	1.16766	0.17186	0.14719
0.45	1.17552	0.17763	0.15111
0.46	1.18356	0.18347	0.15502
0.47	1.19180	0.18938	0.15890
0.48	1.20023	0.19536	0.16277
0.49	1.20886	0.20142	0.16662
0.50	1.21768	0.20754	0.17044

x	$F_{5/17}(x)$	$H_{12/17}(x)$	$T_{5/17}(x)$
0.50	1.21768	0.20754	0.17044
0.51	1.22669	0.21374	0.17424
0.52	1.23590	0.22001	0.17801
0.53	1.24531	0.22634	0.18176
0.54	1.25492	0.23276	0.18548
0.55	1.26472	0.23924	0.18916
0.56	1.27473	0.24580	0.19282
0.57	1.28493	0.25243	0.19645
0.58	1.29535	0.25913	0.20005
0.59	1.30596	0.26591	0.20361
0.60	1.31678	0.27276	0.20714
0.61	1.32781	0.27969	0.21064
0.62	1.33904	0.28669	0.21410
0.63	1.35049	0.29376	0.21752
0.64	1.36214	0.30091	0.22091
0.65	1.37401	0.30814	0.22427
0.66	1.38609	0.31545	0.22758
0.67	1.39838	0.32283	0.23086
0.68	1.41089	0.33029	0.23410
0.69	1.42362	0.33783	0.23730
0.70	1.43657	0.34545	0.24047
0.71	1.44973	0.35315	0.24359
0.72	1.46312	0.36092	0.24668
0.73	1.47674	0.36878	0.24973
0.74	1.49057	0.37672	0.25274
0.75	1.50464	0.38474	0.25570
0.76	1.51893	0.39285	0.25863
0.77	1.53346	0.40104	0.26152
0.78	1.54821	0.40931	0.26438
0.79	1.56320	0.41767	0.26719
0.80	1.57842	0.42611	0.26996
0.81	1.59388	0.43464	0.27269
0.82	1.60958	0.44325	0.27539
0.83	1.62552	0.45196	0.27804
0.84	1.64170	0.46075	0.28065
0.85	1.65812	0.46963	0.28323
0.86	1.67479	0.47860	0.28577
0.87	1.69171	0.48767	0.28827
0.88	1.70888	0.49682	0.29073
0.89	1.72630	0.50607	0.29315
0.90	1.74398	0.51541	0.29554
0.91	1.76191	0.52485	0.29789
0.92	1.78010	0.53438	0.30020
0.93	1.79854	0.54401	0.30247
0.94	1.81725	0.55373	0.30471
0.95	1.83623	0.56355	0.30691
0.96	1.85547	0.57348	0.30907
0.97	1.87498	0.58350	0.31120
0.98	1.89476	0.59362	0.31330
0.99	1.91481	0.60385	0.31536
1.00	1.93514	0.61418	0.31738

x	$F_{5/17}(x)$	$H_{12/17}(x)$	$T_{5/17}(x)$
1.00	1.93514	0.61418	0.31738
1.01	1.95575	0.62461	0.31937
1.02	1.97664	0.63515	0.32133
1.03	1.99781	0.64579	0.32325
1.04	2.01926	0.65654	0.32514
1.05	2.04100	0.66740	0.32700
1.06	2.06303	0.67837	0.32882
1.07	2.08536	0.68945	0.33062
1.08	2.10798	0.70064	0.33238
1.09	2.13090	0.71195	0.33411
1.10	2.15411	0.72337	0.33581
1.11	2.17763	0.73490	0.33748
1.12	2.20146	0.74655	0.33912
1.13	2.22559	0.75832	0.34073
1.14	2.25004	0.77021	0.34231
1.15	2.27480	0.78222	0.34386
1.16	2.29987	0.79435	0.34539
1.17	2.32527	0.80660	0.34688
1.18	2.35099	0.81897	0.34835
1.19	2.37703	0.83148	0.34980
1.20	2.40340	0.84410	0.35121
1.21	2.43010	0.85686	0.35260
1.22	2.45714	0.86974	0.35397
1.23	2.48452	0.88276	0.35530
1.24	2.51223	0.89591	0.35662
1.25	2.54029	0.90919	0.35791
1.26	2.56870	0.92261	0.35917
1.27	2.59745	0.93616	0.36041
1.28	2.62656	0.94985	0.36163
1.29	2.65603	0.96368	0.36283
1.30	2.68586	0.97765	0.36400
1.31	2.71605	0.99176	0.36515
1.32	2.74661	1.00602	0.36628
1.33	2.77754	1.02042	0.36738
1.34	2.80884	1.03497	0.36847
1.35	2.84052	1.04966	0.36953
1.36	2.87258	1.06451	0.37058
1.37	2.90503	1.07951	0.37160
1.38	2.93786	1.09466	0.37260
1.39	2.97109	1.10997	0.37359
1.40	3.00471	1.12543	0.37455
1.41	3.03874	1.14105	0.37550
1.42	3.07317	1.15683	0.37643
1.43	3.10800	1.17278	0.37734
1.44	3.14325	1.18888	0.37823
1.45	3.17891	1.20515	0.37911
1.46	3.21499	1.22159	0.37997
1.47	3.25150	1.23820	0.38081
1.48	3.28843	1.25498	0.38163
1.49	3.32580	1.27193	0.38244
1.50	3.36360	1.28905	0.38324

TABLE 22A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/17$ and x from 0.00 to 1.50.

$\alpha = 5/17$

x	$F_{5/17}(x)$	$H_{12/17}(x)$	$T_{5/17}(x)$
1.50	3.36360	1.28905	0.38324
1.51	3.40185	1.30636	0.38401
1.52	3.44053	1.32383	0.38478
1.53	3.47967	1.34149	0.38552
1.54	3.51927	1.35933	0.38626
1.55	3.55932	1.37736	0.38697
1.56	3.59983	1.39557	0.38768
1.57	3.64081	1.41397	0.38837
1.58	3.68226	1.43256	0.38904
1.59	3.72419	1.45134	0.38970
1.60	3.76661	1.47031	0.39035
1.61	3.80950	1.48948	0.39099
1.62	3.85289	1.50885	0.39161
1.63	3.89678	1.52842	0.39223
1.64	3.94117	1.54819	0.39283
1.65	3.98606	1.56817	0.39341
1.66	4.03146	1.58835	0.39399
1.67	4.07738	1.60874	0.39455
1.68	4.12383	1.62935	0.39511
1.69	4.17079	1.65016	0.39565
1.70	4.21830	1.67120	0.39618
1.71	4.26634	1.69245	0.39670
1.72	4.31492	1.71392	0.39721
1.73	4.36405	1.73562	0.39771
1.74	4.41373	1.75754	0.39820
1.75	4.46398	1.77969	0.39868
1.76	4.51478	1.80207	0.39915
1.77	4.56616	1.82468	0.39961
1.78	4.61812	1.84753	0.40006
1.79	4.67066	1.87061	0.40050
1.80	4.72379	1.89394	0.40094
1.81	4.77751	1.91751	0.40136
1.82	4.83184	1.94132	0.40178
1.83	4.88677	1.96538	0.40219
1.84	4.94231	1.98970	0.40258
1.85	4.99847	2.01427	0.40298
1.86	5.05526	2.03909	0.40336
1.87	5.11268	2.06417	0.40374
1.88	5.17074	2.08952	0.40410
1.89	5.22944	2.11513	0.40447
1.90	5.28880	2.14100	0.40482
1.91	5.34881	2.16715	0.40517
1.92	5.40949	2.19357	0.40550
1.93	5.47084	2.22027	0.40584
1.94	5.53287	2.24725	0.40616
1.55	5.59558	2.27451	0.40648
1.96	5.65899	2.30205	0.40680
1.97	5.72310	2.32988	0.40710
1.98	5.78791	2.35801	0.40740
1.99	5.85344	2.38643	0.40770
2.00	5.91969	2.41514	0.40798

x	$F_{5/17}(x)$	$H_{12/17}(x)$	$T_{5/17}(x)$
2.0	5.91969	2.41514	0.40798
2.1	6.62356	2.71940	0.41057
2.2	7.40830	3.05717	0.41267
2.3	8.28271	3.43221	0.41438
2.4	9.25655	3.84867	0.41578
2.5	10.34068	4.31119	0.41692
2.6	11.54715	4.82490	0.41784
2.7	12.88936	5.39547	0.41860
2.8	14.38218	6.02922	0.41921
2.9	16.04211	6.73315	0.41972
3.0	17.88748	7.51501	0.42013
3.1	19.93859	8.38339	0.42046
3.2	22.21800	9.34785	0.42073
3.3	24.75072	10.41896	0.42096
3.4	27.56449	11.60844	0.42114
3.5	30.69009	12.92930	0.42129
3.6	34.16164	14.39594	0.42141
3.7	38.01697	16.02436	0.42151
3.8	42.29805	17.83227	0.42159
3.9	47.05138	19.83931	0.42165
4.0	52.32855	22.06726	0.42171
4.1	58.16673	24.54025	0.42175
4.2	64.68931	27.28504	0.42179
4.3	71.90656	30.33128	0.42182
4.4	79.91634	33.71185	0.42184
4.5	88.80500	37.46317	0.42186
4.6	98.66820	41.62564	0.42187
4.7	109.61201	46.24399	0.42189
4.8	121.75394	51.36783	0.42190
4.9	135.22424	57.05212	0.42191
5.0	150.16726	63.35776	0.42191
5.1	166.74293	70.35226	0.42192
5.2	185.12852	78.11040	0.42193
5.3	205.52042	86.71506	0.42193
5.4	228.13624	96.25807	0.42193
5.5	253.21712	106.84117	0.42194
5.6	281.03023	118.57709	0.42194
5.7	311.87155	131.59074	0.42194
5.8	346.06903	146.02048	0.42194
5.9	383.98600	162.01963	0.42194
6.0	426.02496	179.75802	0.42194

x	$F_{5/17}(x)$	$H_{12/17}(x)$	$T_{5/17}(x)$
6.0	426.02496	179.75802	0.42194
6.1	472.63180	199.42380	0.42194
6.2	524.30050	221.22540	0.42194
6.3	581.57826	245.39370	0.42194
6.4	645.07120	272.18447	0.42194
6.5	715.45078	301.88102	0.42195
6.6	793.46071	334.79717	0.42195
6.7	879.92479	371.28051	0.42195
6.8	975.75548	411.71604	0.42195
6.9	1081.96340	456.53021	0.42195
7.0	1199.66792	506.19532	0.42195
7.1	1330.10877	561.23449	0.42195
7.2	1474.65900	622.22705	0.42195
7.3	1634.83927	689.81465	0.42195
7.4	1812.33367	764.70789	0.42195
7.5	2009.00727	847.69373	0.42195
7.6	2226.92552	939.64367	0.42195
7.7	2468.37571	1041.52284	0.42195
7.8	2735.89079	1154.40000	0.42195
7.9	3032.27566	1279.45867	0.42195
8.0	3360.63634	1418.00944	0.42195
8.1	3724.41224	1571.50353	0.42195
8.2	4127.41183	1741.54793	0.42195
8.3	4573.85221	1929.92204	0.42195
8.4	5068.40287	2138.59612	0.42195
8.5	5616.23411	2369.75177	0.42195
8.6	6223.07069	2625.80453	0.42195
8.7	6895.25115	2909.42892	0.42195
8.8	7639.79352	3223.58619	0.42195
8.9	8464.46804	3571.55497	0.42195
9.0	9377.87767	3956.96523	0.42195
9.1	10389.54712	4383.83592	0.42195
9.2	11510.02154	4856.61650	0.42195
9.3	12750.97560	5380.23309	0.42195
9.4	14125.33432	5960.13934	0.42195
9.5	15647.40677	6602.37292	0.42195
9.6	17333.03404	7313.61793	0.42195
9.7	19199.75308	8101.27403	0.42195
9.8	21266.97790	8973.53291	0.42195
9.9	23556.20027	9939.46293	0.42195
10.0	26091.21170	11009.10286	0.42195

TABLE 22B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/17$ and x from 1.50 to 10.0.

$\alpha = 12/17$

x	$F_{12/17}(x)$	$H_{5/17}(x)$	$T_{12/17}(x)$	x	$F_{12/17}(x)$	$H_{5/17}(x)$	$T_{12/17}(x)$	x	$F_{12/17}(x)$	$H_{5/17}(x)$	$T_{12/17}(x)$
C.0	1.00000	0.0	0.0	0.50	1.09018	1.57792	1.44740	1.00	1.38093	2.72283	1.97174
0.01	1.00004	0.15064	0.15063	0.51	1.09389	1.59946	1.46218	1.01	1.38915	2.74866	1.97866
C.02	1.00014	0.22649	0.22645	0.52	1.09768	1.62098	1.47674	1.02	1.39748	2.77466	1.98547
0.03	1.00032	0.28752	0.28743	0.53	1.10155	1.64250	1.49108	1.03	1.40592	2.80082	1.99217
0.04	1.00057	0.34058	0.34039	0.54	1.10550	1.66402	1.50521	1.04	1.41446	2.82717	1.99877
0.05	1.00089	0.38842	0.38808	C.55	1.10953	1.68554	1.51914	1.05	1.42310	2.85369	2.00526
0.C6	1.00128	0.43248	0.43193	0.56	1.11364	1.70706	1.53286	1.06	1.43186	2.88039	2.01164
0.C7	1.00174	0.47365	0.47283	0.57	1.11784	1.72860	1.54638	1.C7	1.44073	2.90728	2.01793
0.08	1.00227	0.51250	0.51135	C.58	1.12211	1.75015	1.55970	1.08	1.44970	2.93435	2.02411
0.09	1.00287	0.54945	0.54788	0.59	1.12646	1.77173	1.57282	1.09	1.45879	2.96162	2.03019
0.10	1.00354	0.58480	0.58273	0.6C	1.13090	1.79333	1.58576	1.10	1.46798	2.98907	2.03618
0.11	1.00429	0.61877	0.61613	0.61	1.13542	1.81497	1.59850	1.11	1.47729	3.01672	2.04206
0.12	1.00511	0.65156	0.64825	0.62	1.14002	1.83664	1.61105	1.12	1.48671	3.04457	2.04786
0.13	1.00599	0.68330	0.67923	0.63	1.14471	1.85835	1.62343	1.13	1.49625	3.07263	2.05355
0.14	1.00695	0.71411	0.70918	0.64	1.14948	1.88010	1.63561	1.14	1.50590	3.10088	2.05916
0.15	1.00798	0.74411	0.73822	0.65	1.15433	1.90190	1.64762	1.15	1.51567	3.12935	2.06467
0.16	1.00908	0.77336	0.76640	0.66	1.15927	1.92375	1.65946	1.16	1.52555	3.15802	2.07009
C.17	1.01026	0.80195	0.79381	0.67	1.16429	1.94566	1.67112	1.17	1.53555	3.18691	2.07542
0.18	1.01150	0.82993	C.82049	0.68	1.16940	1.96763	1.68261	1.18	1.54567	3.21602	2.08067
0.19	1.01282	0.85736	0.84651	0.69	1.17459	1.98966	1.69392	1.19	1.55590	3.24534	2.08583
0.20	1.01421	0.88429	0.87190	C.70	1.17987	2.01176	1.70507	1.20	1.56626	3.27489	2.09090
0.21	1.01567	0.91075	0.89670	0.71	1.18523	2.03393	1.71606	1.21	1.57674	3.30467	2.09589
0.22	1.01720	0.93680	0.92095	0.72	1.19069	2.05618	1.72688	1.22	1.58734	3.33467	2.10080
0.23	1.01881	0.96245	0.94468	0.73	1.19623	2.07850	1.73755	1.23	1.59806	3.36490	2.10562
C.24	1.02049	0.98774	0.96791	C.74	1.20186	2.10090	1.74805	1.24	1.60890	3.39537	2.11036
0.25	1.02224	1.01270	0.99067	C.75	1.20757	2.12339	1.75840	1.25	1.61988	3.42608	2.11503
0.26	1.02406	1.03735	1.01298	0.76	1.21338	2.14597	1.76859	1.26	1.63097	3.45703	2.11961
0.27	1.02596	1.06172	1.03485	C.77	1.21928	2.16864	1.77863	1.27	1.64219	3.48822	2.12412
C.28	1.02793	1.08582	1.05632	C.78	1.22526	2.19141	1.78852	1.28	1.65354	3.51966	2.12855
0.29	1.02997	1.10968	1.07739	0.79	1.23134	2.21427	1.79826	1.29	1.66502	3.55135	2.13291
0.30	1.03209	1.13331	1.09808	0.80	1.23751	2.23724	1.80786	1.30	1.67663	3.58329	2.13720
0.31	1.03428	1.15673	1.11840	0.81	1.24377	2.26031	1.81731	1.31	1.68837	3.61549	2.14141
0.32	1.03654	1.17996	1.13837	0.82	1.25012	2.28349	1.82662	1.32	1.70024	3.64795	2.14555
0.33	1.03888	1.20301	1.15799	0.83	1.25657	2.30678	1.83578	1.33	1.71225	3.68068	2.14962
C.34	1.04129	1.22590	1.17729	0.84	1.26310	2.33019	1.84481	1.34	1.72439	3.71367	2.15362
0.35	1.04378	1.24863	1.19626	0.85	1.26974	2.35372	1.85370	1.35	1.73666	3.74693	2.15755
0.36	1.04634	1.27121	1.21492	0.86	1.27646	2.37736	1.86246	1.36	1.74907	3.78046	2.16141
0.37	1.04897	1.29367	1.23327	C.87	1.28329	2.40113	1.87108	1.37	1.76161	3.81427	2.16521
0.38	1.05169	1.31601	1.25133	0.88	1.29021	2.42503	1.87957	1.38	1.77430	3.84835	2.16895
0.39	1.05447	1.33823	1.26910	C.89	1.29722	2.44906	1.88793	1.39	1.78712	3.88272	2.17261
C.4C	1.05733	1.36036	1.28660	C.90	1.30433	2.47322	1.89616	1.40	1.80008	3.91738	2.17622
0.41	1.06027	1.38240	1.30381	0.91	1.31154	2.49752	1.90426	1.41	1.81319	3.95233	2.17976
0.42	1.06329	1.40435	1.32076	C.92	1.31885	2.52195	1.91224	1.42	1.82644	3.98756	2.18325
0.43	1.06638	1.42623	1.33745	0.93	1.32626	2.54653	1.92009	1.43	1.83983	4.02310	2.18667
0.44	1.06955	1.44804	1.35389	0.94	1.33376	2.57126	1.92782	1.44	1.85337	4.05893	2.19003
C.45	1.07279	1.46979	1.37007	0.95	1.34137	2.59613	1.93543	1.45	1.86705	4.09507	2.19333
0.46	1.07611	1.49150	1.38600	0.96	1.34908	2.62116	1.94293	1.46	1.88089	4.13152	2.19658
0.47	1.07951	1.51315	1.40170	0.97	1.35689	2.64634	1.95030	1.47	1.89487	4.16827	2.19977
0.48	1.08299	1.53477	1.41716	0.98	1.36480	2.67167	1.95756	1.48	1.90900	4.20534	2.20290
0.49	1.08654	1.55636	1.43239	C.99	1.37281	2.69717	1.96470	1.49	1.92328	4.24272	2.20598
0.5C	1.09018	1.57792	1.44740	1.00	1.38093	2.72283	1.97174	1.5C	1.93771	4.28042	2.20901

TABLE 23A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 12/17$ and x from 0.00 to 1.50.

$\alpha = 12/17$

x	$F_{12/17}(x)$	$H_{5/17}(x)$	$T_{12/17}(x)$
1.50	1.93771	4.28042	2.20901
1.51	1.95230	4.31845	2.21198
1.52	1.96705	4.35681	2.21490
1.53	1.98195	4.39550	2.21777
1.54	1.99701	4.43452	2.22058
1.55	2.01222	4.47388	2.22335
1.56	2.02760	4.51359	2.22607
1.57	2.04314	4.55363	2.22874
1.58	2.05885	4.59403	2.23136
1.59	2.07471	4.63479	2.23394
1.60	2.09075	4.67590	2.23647
1.61	2.10695	4.71737	2.23896
1.62	2.12332	4.75921	2.24140
1.63	2.13986	4.80142	2.24379
1.64	2.15658	4.84399	2.24615
1.65	2.17346	4.88695	2.24846
1.66	2.19053	4.93029	2.25073
1.67	2.20777	4.97401	2.25296
1.68	2.22518	5.01812	2.25515
1.69	2.24278	5.06263	2.25730
1.70	2.26056	5.10753	2.25941
1.71	2.27852	5.15283	2.26149
1.72	2.29666	5.19854	2.26352
1.73	2.31499	5.24466	2.26552
1.74	2.33351	5.29120	2.26748
1.75	2.35222	5.33815	2.26941
1.76	2.37112	5.38552	2.27130
1.77	2.39021	5.43333	2.27316
1.78	2.40949	5.48156	2.27499
1.79	2.42897	5.53023	2.27678
1.8C	2.44865	5.57934	2.27853
1.81	2.46853	5.62890	2.28026
1.82	2.48861	5.67890	2.28195
1.83	2.50890	5.72936	2.28362
1.84	2.52939	5.78028	2.28525
1.85	2.55008	5.83166	2.28685
1.86	2.57099	5.88351	2.28843
1.87	2.59210	5.93584	2.28997
1.68	2.61343	5.98864	2.29149
1.89	2.63497	6.04192	2.29297
1.90	2.65673	6.09569	2.29443
1.91	2.67871	6.14996	2.29587
1.92	2.70090	6.20472	2.29728
1.93	2.72332	6.25998	2.29866
1.94	2.74597	6.31575	2.30091
1.95	2.76883	6.37204	2.30134
1.96	2.79193	6.42884	2.30265
1.57	2.81526	6.48616	2.30393
1.98	2.83882	6.54402	2.30519
1.99	2.86262	6.60240	2.30642
2.00	2.88665	6.66133	2.30763

x	$F_{12/17}(x)$	$H_{5/17}(x)$	$T_{12/17}(x)$
2.0	2.88665	6.66133	2.30763
2.1	3.14048	7.28143	2.31857
2.2	3.42051	7.96167	2.32762
2.3	3.72927	8.70824	2.33510
2.4	4.06954	9.52794	2.34128
2.5	4.44441	10.42826	2.34638
2.6	4.85728	11.41739	2.35057
2.7	5.31189	12.50435	2.35403
2.8	5.81238	13.69907	2.35686
2.9	6.36332	15.01245	2.35922
3.0	6.96973	16.45652	2.36114
3.1	7.63715	18.04448	2.36272
3.2	8.37170	19.79090	2.36402
3.3	9.18012	21.71181	2.36509
3.4	10.06982	23.82485	2.36597
3.5	11.04898	26.14948	2.36669
3.6	12.12664	28.70711	2.36728
3.7	13.31272	31.52133	2.36776
3.8	14.61817	34.61815	2.36816
3.9	16.05508	38.02620	2.36848
4.0	17.63674	41.77705	2.36875
4.1	19.37781	45.90547	2.36897
4.2	21.29446	50.44979	2.36915
4.3	23.40450	55.45224	2.36930
4.4	25,72756	60.95936	2.36942
4.5	28.28528	67.02246	2.36952
4.6	31.10150	73.69808	2.36960
4.7	34.20252	81.04853	2.36967
4.8	37.61732	89.14249	2.36972
4.9	41.37783	98.05570	2.36976
5.0	45.51926	107.87160	2.36980
5.1	50.08045	118.68220	2.36983
5.2	55.10417	130.58892	2.36986
5.3	60.63760	143.70358	2.36988
5.4	66.73275	158.14943	2.36989
5.5	73.44695	174.06236	2.36991
5.6	80.84343	191.59221	2.36992
5.7	88.99187	210.90415	2.36993
5.8	97.96913	232.18032	2.36993
5.9	107.85993	255.62152	2.36994
6.0	118.75771	281.44917	2.36994

x	$F_{12/17}(x)$	$H_{5/17}(x)$	$T_{12/17}(x)$
6.0	118.75771	281.44917	2.36994
6.1	130.76546	309.90742	2.36995
6.2	143.99679	341.26548	2.36995
6.3	158.57695	375.82019	2.36995
6.4	174.64407	413.89892	2.36996
6.5	192.35045	455.86264	2.36996
6.6	211.86407	502.10943	2.36996
6.7	233.37016	553.07830	2.36996
6.8	257.07300	609.25337	2.36996
6.9	283.19787	671.16858	2.36996
7.0	311.99324	739.41276	2.36996
7.1	343.73312	814.63533	2.36996
7.2	378.71974	897.55255	2.36997
7.3	417.28643	988.95440	2.36997
7.4	459.80081	1089.71216	2.36997
7.5	506.66840	1200.78687	2.36997
7.6	558.33644	1323.23849	2.36997
7.7	615.29828	1458.23620	2.36997
7.8	678.09805	1607.06964	2.36997
7.9	747.33599	1771.16132	2.36997
8.0	823.67418	1952.08037	2.36997
8.1	907.84297	2151.55767	2.36997
8.2	1000.64800	2371.50257	2.36997
8.3	1102.97798	2614.02128	2.36997
8.4	1215.81329	2881.43727	2.36997
8.5	1340.23543	3176.31367	2.36997
8.6	1477.43749	3501.47806	2.36997
8.7	1628.73567	3860.04979	2.36997
8.8	1795.58200	4255.47013	2.36997
8.9	1979.57841	4691.53557	2.36997
9.0	2182.49218	5172.43456	2.36997
9.1	2406.27310	5702.78798	2.36997
9.2	2653.07228	6287.69393	2.36997
9.3	2925.26302	6932.77704	2.36997
9.4	3225.46378	7644.24298	2.36997
9.5	3556.56354	8428.93852	2.36997
9.6	3921.74978	9294.41791	2.36997
9.7	4324.53941	10249.01609	2.36997
9.8	4768.81281	11301.92943	2.36997
9.9	5258.85148	12463.30496	2.36997
10.0	5799.37957	13744.33875	2.36997

TABLE 23B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 12/17$ and x from 1.50 to 10.0.

α = 5/21

x	$F_{5/21}(x)$	$H_{16/21}(x)$	$T_{5/21}(x)$	x	$F_{5/21}(x)$	$H_{16/21}(x)$	$T_{5/21}(x)$	x	$F_{5/21}(x)$	$H_{16/21}(x)$	$T_{5/21}(x)$
0.0	1.00000	0.0	0.0	0.50	1.26919	0.16443	0.12956	1.00	2.16003	0.52421	0.24268
0.01	1.00011	0.00041	0.00041	0.51	1.28035	0.16971	0.13255	1.01	2.18569	0.53366	0.24416
0.02	1.00042	0.00118	0.00118	0.52	1.29175	0.17506	0.13552	1.02	2.21170	0.54322	0.24561
0.03	1.00095	0.00218	0.00218	0.53	1.30340	0.18048	0.13847	1.03	2.23807	0.55288	0.24703
0.04	1.00168	0.00338	0.00338	0.54	1.31529	0.18597	0.14139	1.04	2.26480	0.56265	0.24843
0.05	1.00263	0.00475	0.00474	0.55	1.32744	0.19153	0.14429	1.05	2.29188	0.57252	0.24980
0.06	1.00378	0.00628	0.00625	0.56	1.33983	0.19717	0.14716	1.06	2.31934	0.58250	0.25115
0.07	1.00515	0.00794	0.00790	0.57	1.35247	0.20288	0.15001	1.07	2.34716	0.59259	0.25247
0.08	1.00672	0.00973	0.00967	0.58	1.36537	0.20867	0.15283	1.08	2.37535	0.60278	0.25377
0.09	1.00851	0.01165	0.01155	0.59	1.37852	0.21452	0.15562	1.09	2.40392	0.61309	0.25504
0.10	1.01051	0.01368	0.01354	0.60	1.39192	0.22045	0.15838	1.10	2.43287	0.62350	0.25628
0.11	1.01272	0.01583	0.01563	0.61	1.40559	0.22646	0.16111	1.11	2.46220	0.63403	0.25751
0.12	1.01514	0.01808	0.01781	0.62	1.41951	0.23254	0.16381	1.12	2.49191	0.64468	0.25871
0.13	1.01778	0.02043	0.02007	0.63	1.43369	0.23869	0.16649	1.13	2.52201	0.65543	0.25988
0.14	1.02062	0.02288	0.02242	0.64	1.44814	0.24492	0.16913	1.14	2.55251	0.66630	0.26104
0.15	1.02368	0.02543	0.02484	0.65	1.46285	0.25122	0.17174	1.15	2.58340	0.67729	0.26217
0.16	1.02695	0.02807	0.02733	0.66	1.47782	0.25761	0.17431	1.16	2.61470	0.68840	0.26328
0.17	1.03043	0.03080	0.02989	0.67	1.49307	0.26406	0.17686	1.17	2.64639	0.69963	0.26437
0.18	1.03413	0.03362	0.03251	0.68	1.50858	0.27060	0.17937	1.18	2.67850	0.71098	0.26544
0.19	1.03804	0.03652	0.03518	0.69	1.52436	0.27721	0.18185	1.19	2.71101	0.72244	0.26649
0.20	1.04217	0.03951	0.03722	0.70	1.54042	0.28390	0.18430	1.20	2.74394	0.73404	0.26751
0.21	1.04651	0.04259	0.04070	0.71	1.55675	0.29067	0.18672	1.21	2.77729	0.74575	0.26852
0.22	1.05107	0.04574	0.04352	0.72	1.57336	0.29752	0.18910	1.22	2.81106	0.75759	0.26950
0.23	1.05584	0.04898	0.04639	0.73	1.59025	0.30445	0.19145	1.23	2.84526	0.76956	0.27047
0.24	1.06083	0.05230	0.04930	0.74	1.60742	0.31146	0.19376	1.24	2.87989	0.78166	0.27142
0.25	1.06604	0.05569	0.05224	0.75	1.62488	0.31855	0.19605	1.25	2.91496	0.79389	0.27235
0.26	1.07147	0.05917	0.05522	0.76	1.64262	0.32572	0.19830	1.26	2.95046	0.80624	0.27326
0.27	1.07711	0.06272	0.05823	0.77	1.66064	0.33298	0.20051	1.27	2.98641	0.81873	0.27415
0.28	1.08297	0.06634	0.06126	0.78	1.67896	0.34032	0.20269	1.28	3.02281	0.83136	0.27503
0.29	1.08906	0.07004	0.06431	0.79	1.69757	0.34774	0.20484	1.29	3.05966	0.84411	0.27589
0.30	1.09536	0.07382	0.06739	0.80	1.71647	0.35524	0.20696	1.30	3.09696	0.85701	0.27673
0.31	1.10189	0.07767	0.07048	0.81	1.73567	0.36283	0.20905	1.31	3.13473	0.87004	0.27755
0.32	1.10864	0.08159	0.07359	0.82	1.75516	0.37051	0.21110	1.32	3.17296	0.88321	0.27836
0.33	1.11561	0.08558	0.07671	0.83	1.77496	0.37827	0.21311	1.33	3.21166	0.89653	0.27915
0.34	1.12280	0.08965	0.07985	0.84	1.79506	0.38612	0.21510	1.34	3.25083	0.90998	0.27992
0.35	1.13022	0.09379	0.08298	0.85	1.81547	0.39406	0.21706	1.35	3.29049	0.92358	0.28068
0.36	1.13787	0.09800	0.08613	0.86	1.83619	0.40208	0.21898	1.36	3.33063	0.93733	0.28143
0.37	1.14574	0.10229	0.08927	0.87	1.85721	0.41020	0.22087	1.37	3.37126	0.95122	0.28216
0.38	1.15384	0.10664	0.09242	0.88	1.87855	0.41840	0.22273	1.38	3.41238	0.96526	0.28287
0.39	1.16217	0.11107	0.09557	0.89	1.90021	0.42670	0.22455	1.39	3.45400	0.97945	0.28357
0.40	1.17073	0.11556	0.09871	0.90	1.92218	0.43509	0.22635	1.40	3.49612	0.99379	0.28426
0.41	1.17952	0.12013	0.10185	0.91	1.94448	0.44357	0.22812	1.41	3.53875	1.00829	0.28493
0.42	1.18854	0.12477	0.10498	0.92	1.96710	0.45214	0.22985	1.42	3.58189	1.02294	0.28559
0.43	1.19779	0.12948	0.10810	0.93	1.99004	0.46081	0.23156	1.43	3.62555	1.03774	0.28623
0.44	1.20728	0.13426	0.11121	0.94	2.01332	0.46958	0.23323	1.44	3.66974	1.05271	0.28686
0.45	1.21700	0.13911	0.11431	0.95	2.03692	0.47843	0.23488	1.45	3.71445	1.06783	0.28748
0.46	1.22696	0.14403	0.11739	0.96	2.06086	0.48739	0.23650	1.46	3.75970	1.08312	0.28809
0.47	1.23716	0.14903	0.12046	0.97	2.08514	0.49645	0.23809	1.47	3.80549	1.09857	0.28868
0.48	1.24760	0.15409	0.12351	0.98	2.10976	0.50560	0.23965	1.48	3.85182	1.11419	0.28926
0.49	1.25827	0.15922	0.12654	0.99	2.13472	0.51485	0.24118	1.49	3.89870	1.12997	0.28983
0.50	1.26919	0.16443	0.12956	1.00	2.16003	0.52421	0.24268	1.50	3.94614	1.14592	0.29039

TABLE 24A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/21$ and x from 0.00 to 1.50.

$\alpha = 5/21$

x	$F_{5/21}(x)$	$H_{16/21}(x)$	$T_{5/21}(x)$
1.50	3.94614	1.14592	0.29039
1.51	3.99414	1.16204	0.29094
1.52	4.04270	1.17834	0.29147
1.53	4.09184	1.19480	0.29200
1.54	4.14156	1.21145	0.29251
1.55	4.19186	1.22827	0.29301
1.56	4.24275	1.24528	0.29351
1.57	4.29424	1.26246	0.29399
1.58	4.34633	1.27983	0.29446
1.59	4.39903	1.29738	0.29493
1.60	4.45234	1.31513	0.29538
1.61	4.50627	1.33306	0.29582
1.62	4.56083	1.35118	0.29626
1.63	4.61603	1.36950	0.29668
1.64	4.67186	1.38801	0.29710
1.65	4.72834	1.40673	0.29751
1.66	4.78548	1.42564	0.29791
1.67	4.84327	1.44476	0.29830
1.68	4.90173	1.46408	0.29869
1.69	4.96086	1.48360	0.29906
1.70	5.02068	1.50334	0.29943
1.71	5.08118	1.52329	0.29979
1.72	5.14238	1.54345	0.30014
1.73	5.20427	1.56383	0.30049
1.74	5.26688	1.58442	0.30083
1.75	5.33020	1.60524	0.30116
1.76	5.39425	1.62628	0.30148
1.77	5.45903	1.64755	0.30180
1.78	5.52454	1.66904	0.30211
1.79	5.59081	1.69077	0.30242
1.80	5.65782	1.71272	0.30272
1.81	5.72560	1.73492	0.30301
1.82	5.79415	1.75735	0.30330
1.83	5.86348	1.78002	0.30358
1.84	5.93359	1.80293	0.30385
1.85	6.00450	1.82609	0.30412
1.86	6.07620	1.84950	0.30438
1.87	6.14872	1.87316	0.30464
1.88	6.22206	1.89708	0.30490
1.89	6.29623	1.92125	0.30514
1.90	6.37123	1.94568	0.30539
1.91	6.44708	1.97037	0.30562
1.92	6.52378	1.99533	0.30585
1.93	6.60135	2.02056	0.30608
1.94	6.67978	2.04605	0.30631
1.95	6.75910	2.07182	0.30652
1.96	6.83931	2.09787	0.30674
1.97	6.92041	2.12420	0.30695
1.98	7.00243	2.15081	0.30715
1.99	7.08536	2.17771	0.30735
2.00	7.16923	2.20489	0.30755

x	$F_{5/21}(x)$	$H_{16/21}(x)$	$T_{5/21}(x)$
2.0	7.16923	2.20489	0.30755
2.1	8.06109	2.49333	0.30930
2.2	9.05716	2.81433	0.31073
2.3	10.16895	3.17156	0.31189
2.4	11.40929	3.56912	0.31283
2.5	12.79243	4.01157	0.31359
2.6	14.33422	4.50395	0.31421
2.7	16.05230	5.05188	0.31471
2.8	17.96624	5.66160	0.31512
2.9	20.09781	6.34003	0.31546
3.0	22.47120	7.09484	0.31573
3.1	25.11324	7.93457	0.31595
3.2	28.05377	8.86870	0.31613
3.3	31.32590	9.90773	0.31628
3.4	34.96638	11.06332	0.31640
3.5	39.01602	12.34844	0.31650
3.6	43.52012	13.77744	0.31658
3.7	48.52897	15.36627	0.31664
3.8	54.09836	17.13264	0.31669
3.9	60.29020	19.09617	0.31674
4.0	67.17322	21.27865	0.31677
4.1	74.82365	23.70426	0.31680
4.2	83.32607	26.39981	0.31683
4.3	92.77435	29.39504	0.31684
4.4	103.27258	32.72297	0.31686
4.5	114.93627	36.42021	0.31687
4.6	127.89351	40.52735	0.31688
4.7	142.28642	45.08944	0.31689
4.8	158.27260	50.15644	0.31690
4.9	176.02686	55.78376	0.31690
5.0	195.74306	62.03283	0.31691
5.1	217.63620	68.97181	0.31691
5.2	241.94470	76.67625	0.31692
5.3	268.93293	85.22995	0.31692
5.4	298.89406	94.72582	0.31692
5.5	332.15314	105.26690	0.31692
5.6	369.07059	116.96739	0.31692
5.7	410.04600	129.95395	0.31693
5.8	455.52239	144.36700	0.31693
5.9	505.99091	160.36218	0.31693
6.0	561.99606	178.11208	0.31693

x	$F_{5/21}(x)$	$H_{16/21}(x)$	$T_{5/21}(x)$
6.0	561.99606	178.11208	0.31693
6.1	624.14143	197.80798	0.31693
6.2	693.09612	219.66195	0.31693
6.3	769.60184	243.90906	0.31693
6.4	854.48071	270.80986	0.31693
6.5	948.64398	300.65317	0.31693
6.6	1053.10168	333.75908	0.31693
6.7	1168.97324	370.48239	0.31693
6.8	1297.49938	411.21630	0.31693
6.9	1440.05512	456.39662	0.31693
7.0	1598.16435	506.50631	0.31693
7.1	1773.51585	562.08059	0.31693
7.2	1967.98111	623.71260	0.31693
7.3	2183.63403	692.05961	0.31693
7.4	2422.77275	767.84999	0.31693
7.5	2687.94382	851.89081	0.31693
7.6	2981.96898	945.07636	0.31693
7.7	3307.97487	1048.39758	0.31693
7.8	3669.42579	1162.95240	0.31693
7.9	4070.16016	1289.95734	0.31693
8.0	4514.43079	1430.76024	0.31693
8.1	5006.94950	1586.85443	0.31693
8.2	5552.93656	1759.89436	0.31693
8.3	6158.17538	1951.71297	0.31693
8.4	6829.07318	2164.34092	0.31693
8.5	7572.72610	2400.02780	0.31693
8.6	8397.00349	2661.26576	0.31693
8.7	9310.61029	2950.81557	0.31693
8.8	10323.19814	3271.73548	0.31693
8.9	11445.45635	3627.41326	0.31693
9.0	12689.22565	4021.60160	0.31693
9.1	14067.62200	4458.45735	0.31693
9.2	15595.17360	4942.58494	0.31693
9.3	17287.97268	5479.08448	0.31693
9.4	19163.84354	6073.60503	0.31693
9.5	21242.52857	6732.40357	0.31693
9.6	23545.89436	7462.41028	0.31693
9.7	26098.15971	8271.30082	0.31693
9.8	28926.14825	9167.57644	0.31693
9.9	32059.56811	10160.65253	0.31693
10.0	35531.32147	11260.95681	0.31693

TABLE 24B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 5/21$ and x from 1.50 to 10.0.

x	$F_{16/21}(x)$	$H_{5/21}(x)$	$T_{16/21}(x)$	x	$F_{16/21}(x)$	$H_{5/21}(x)$	$T_{16/21}(x)$	x	$F_{16/21}(x)$	$H_{5/21}(x)$	$T_{16/21}(x)$
0.0	1.00000	0.0	0.0	C.5C	1.08350	2.28156	2.10575	1.00	1.35212	3.66387	2.70972
0.01	1.00003	0.33692	0.33691	C.51	1.08693	2.30779	2.12322	1.01	1.35970	3.69503	2.71752
0.02	1.00013	0.46871	0.46865	0.52	1.09044	2.33397	2.14039	1.02	1.36738	3.72639	2.72520
0.03	1.00030	0.56859	0.56842	0.53	1.09402	2.36011	2.15728	1.03	1.37516	3.75797	2.73275
0.04	1.00053	0.65216	0.65182	0.54	1.09768	2.38624	2.17389	1.04	1.38304	3.78976	2.74017
0.05	1.00082	0.72541	0.72481	0.55	1.10141	2.41234	2.19024	1.05	1.39101	3.82177	2.74747
0.06	1.00118	0.79138	0.79045	0.56	1.10521	2.43844	2.20632	1.06	1.39909	3.85400	2.75466
0.C7	1.00161	0.85188	0.85051	C.57	1.10909	2.46455	2.22213	1.07	1.40726	3.88646	2.76172
0.08	1.00210	0.90808	0.90618	0.58	1.11304	2.49065	2.23770	1.08	1.41555	3.91914	2.76867
0.09	1.00266	0.96080	0.95825	0.59	1.11707	2.51677	2.25301	1.09	1.42391	3.95206	2.77551
0.10	1.00328	1.01062	1.00731	0.60	1.12117	2.54291	2.26808	1.10	1.43238	3.98522	2.78223
0.11	1.00397	1.05799	1.05380	C.61	1.12535	2.56908	2.28291	1.11	1.44096	4.01861	2.78884
0.12	1.00473	1.10326	1.09807	C.62	1.12961	2.59528	2.29750	1.12	1.44965	4.05225	2.79534
0.13	1.00555	1.14670	1.14037	0.63	1.13394	2.62151	2.31185	1.13	1.45843	4.08614	2.80173
0.14	1.00644	1.18854	1.18093	0.64	1.13835	2.64779	2.32598	1.14	1.46732	4.12028	2.80802
0.15	1.00739	1.22895	1.21993	0.65	1.14284	2.67412	2.33989	1.15	1.47632	4.15467	2.81420
0.16	1.00842	1.26810	1.25752	0.66	1.14741	2.70051	2.35357	1.16	1.48543	4.18932	2.82028
0.17	1.00950	1.30611	1.29382	C.67	1.15205	2.72695	2.36704	1.17	1.49464	4.22423	2.82626
0.18	1.01066	1.34309	1.32893	0.68	1.15677	2.75346	2.38030	1.18	1.50395	4.25941	2.83214
C.19	1.01188	1.37915	1.36296	C.69	1.16157	2.78004	2.39334	1.19	1.51338	4.29486	2.83792
0.20	1.01316	1.41436	1.39599	C.70	1.16645	2.80670	2.40618	1.20	1.52292	4.33058	2.84360
0.21	1.01452	1.44880	1.42807	C.71	1.17141	2.83344	2.41882	1.21	1.53257	4.36658	2.84919
0.22	1.01594	1.48253	1.45928	0.72	1.17645	2.86026	2.43126	1.22	1.54233	4.40285	2.85468
0.23	1.01742	1.51562	1.48967	0.73	1.18158	2.88718	2.44350	1.23	1.55220	4.43941	2.86008
0.24	1.01898	1.54811	1.51928	C.74	1.18678	2.91419	2.45554	1.24	1.56218	4.47626	2.86539
0.25	1.02060	1.58005	1.54816	0.75	1.19206	2.94130	2.46740	1.25	1.57228	4.51340	2.87061
C.26	1.02229	1.61149	1.57636	0.76	1.19743	2.96851	2.47907	1.26	1.58249	4.55084	2.87574
0.27	1.02404	1.64246	1.60389	C.77	1.20288	2.99583	2.49056	1.27	1.59282	4.58857	2.88078
C.28	1.02587	1.67300	1.63081	C.78	1.20841	3.02327	2.50186	1.28	1.60326	4.62660	2.88574
0.29	1.02776	1.70313	1.65713	C.79	1,21402	3.05082	2.51299	1.29	1.61383	4.66495	2.89061
0.30	1.02972	1.73290	1.68288	C.80	1.21972	3.07850	2.52394	1.30	1.62451	4.70360	2.89540
0.31	1.03175	1.76232	1.70809	0.81	1.22550	3.10630	2.53471	1.31	1.63531	4.74257	2.90011
0.32	1.03384	1.79142	1.73278	C.82	1.23137	3.13423	2.54532	1.32	1.64622	4.78185	2.90474
0.33	1.03601	1.82023	1.75696	0.83	1.23733	3.16230	2.55576	1.33	1.65726	4.82146	2.90929
0.34	1.03824	1.84876	1.78067	0.84	1.24336	3.19051	2.56603	1.34	1.66843	4.86139	2.91376
C.35	1.04055	1.87705	1.80391	0.85	1.24949	3.21886	2.57614	1.35	1.67971	4.90165	2.91815
0.36	1.04292	1.90509	1.82670	0.86	1.25570	3.24735	2.58608	1.36	1.69112	4.94224	2.92246
0.37	1.04536	1.93293	1.84906	0.87	1.26200	3.27600	2.59587	1.37	1.70266	4.98318	2.92671
C.38	1.04787	1.96056	1.87100	0.88	1.26839	3.30480	2.60550	1.38	1.71432	5.02445	2.93088
0.39	1.05045	1.98801	1.89253	0.89	1,27487	3.33376	2.61498	1.39	1.72610	5.06607	2.93497
0.4C	1.05310	2.01529	1.91368	0.90	1.28143	3.36288	2.62431	1.4C	1.73802	5.10803	2.93900
0.41	1.05582	2.04242	1.93444	0.91	1.28809	3.39217	2.63349	1.41	1.75006	5.15035	2.94295
0.42	1.05861	2.06940	1.95483	0.92	1.29483	3.42162	2.64252	1.42	1.76224	5.19303	2.94684
0.43	1.06147	2.09626	1.97486	0.93	1.30167	3.45126	2.65141	1.43	1.77454	5.23607	2.95066
0.44	1.06440	2.12299	1.99454	0.94	1.30860	3.48107	2.66015	1.44	1.78698	5.27947	2.95441
0.45	1.06741	2.14963	2.01388	0.95	1.31562	3.51106	2.66875	1.45	1.79955	5.32325	2.95810
0.46	1.07048	2.17617	2.03289	C.96	1.32273	3.54123	2.67722	1.46	1.81225	5.36739	2.96172
0.47	1.07363	2.20262	2.05157	C.97	1.32994	3.57160	2.68554	1.47	1.82509	5.41192	2.96528
0.48	1.07684	2.22900	2.06994	0.98	1.33724	3.60216	2.69374	1.48	1.83807	5.45683	2.96878
0.45	1.08013	2.25532	2.08800	0.99	1.34463	3.63291	2.70180	1.49	1.85119	5.50212	2.97221
0.50	1.08350	2.28158	2.10575	1.00	1.35212	3.66387	2.70972	1.5C	1.86444	5.54780	2.97559

TABLE 25A. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 16/21$ and x from 0.00 to 1.50.

$\alpha = 16/21$

x	$F_{16/21}(x)$	$H_{5/21}(x)$	$T_{16/21}(x)$
1.50	1.86444	5.54780	2.97559
1.51	1.87783	5.59388	2.97890
1.52	1.89137	5.64035	2.98216
1.53	1.90504	5.68723	2.98536
1.54	1.91886	5.73452	2.98850
1.55	1.93283	5.78222	2.99159
1.56	1.94694	5.83033	2.99462
1.57	1.96119	5.87887	2.99760
1.58	1.97560	5.92783	3.00052
1.59	1.99016	5.97722	3.00339
1.60	2.00486	6.02705	3.00622
1.61	2.01572	6.07731	3.00899
1.62	2.03473	6.12802	3.01171
1.63	2.04990	6.17917	3.01438
1.64	2.06522	6.23078	3.01701
1.65	2.08070	6.28285	3.01959
1.66	2.09634	6.33538	3.02212
1.67	2.11214	6.38837	3.02460
1.68	2.12809	6.44184	3.02704
1.69	2.14422	6.49578	3.02944
1.70	2.16050	6.55021	3.03180
1.71	2.17696	6.60512	3.03411
1.72	2.19358	6.66052	3.03638
1.73	2.21036	6.71642	3.03861
1.74	2.22732	6.77283	3.04079
1.75	2.24445	6.82974	3.04294
1.76	2.26175	6.88716	3.04505
1.77	2.27923	6.94509	3.04712
1.78	2.29688	7.00355	3.04916
1.79	2.31471	7.06254	3.05115
1.80	2.33272	7.12206	3.05311
1.81	2.35091	7.18212	3.05504
1.82	2.36928	7.24272	3.05693
1.83	2.38784	7.30387	3.05878
1.84	2.40658	7.36558	3.06060
1.85	2.42551	7.42784	3.06239
1.86	2.44462	7.49068	3.06414
1.87	2.46393	7.55408	3.06587
1.88	2.48343	7.61806	3.06756
1.89	2.50312	7.68262	3.06922
1.90	2.52301	7.74777	3.07084
1.91	2.54310	7.81352	3.07244
1.92	2.56338	7.87986	3.07401
1.93	2.58387	7.94682	3.07555
1.94	2.60455	8.01438	3.07706
1.95	2.62545	8.08256	3.07855
1.96	2.64654	8.15137	3.08000
1.97	2.66785	8.22081	3.08143
1.98	2.68937	8.29088	3.08284
1.99	2.71109	8.36160	3.08421
2.00	2.73304	8.43296	3.08557

x	$F_{16/21}(x)$	$H_{5/21}(x)$	$T_{16/21}(x)$
2.0	2.73304	8.43296	3.08557
2.1	2.96463	9.18375	3.09777
2.2	3.21983	10.00683	3.10787
2.3	3.50087	10.90952	3.11623
2.4	3.81023	11.89985	3.12313
2.5	4.15063	12.98661	3.12883
2.6	4.52509	14.17947	3.13352
2.7	4.93692	15.48905	3.13739
2.8	5.38977	16.92700	3.14058
2.9	5.88768	18.50614	3.14320
3.0	6.43507	20.24059	3.14536
3.1	7.03684	22.14584	3.14713
3.2	7.69836	24.23896	3.14859
3.3	8.42557	26.53873	3.14979
3.4	9.22499	29.06581	3.15077
3.5	10.10381	31.84294	3.15158
3.6	11.06995	34.89515	3.15224
3.7	12.13214	38.25000	3.15278
3.8	13.29996	41.93784	3.15323
3.9	14.58400	45.99205	3.15360
4.0	15.99589	50.44942	3.15390
4.1	17.54848	55.35044	3.15414
4.2	19.25588	60.73971	3.15435
4.3	21.13364	66.66633	3.15451
4.4	23.19890	73.18439	3.15465
4.5	25.47054	80.35344	3.15476
4.6	27.96934	88.23910	3.15485
4.7	30.71819	96.91362	3.15493
4.8	33.74231	106.45659	3.15499
4.9	37.06950	116.95567	3.15504
5.0	40.73034	128.50745	3.15508
5.1	44.75855	141.21830	3.15511
5.2	49.19129	155.20544	3.15514
5.3	54.06945	170.59797	3.15516
5.4	59.43814	187.53817	3.15518
5.5	65.34702	206.18274	3.15520
5.6	71.85081	226.70439	3.15521
5.7	79.00982	249.29339	3.15522
5.8	86.89050	274.15939	3.15523
5.9	95.56606	301.53341	3.15524
6.0	105.11717	331.67003	3.15524

x	$F_{16/21}(x)$	$H_{5/21}(x)$	$T_{16/21}(x)$
6.0	105.11717	331.67003	3.15524
6.1	115.63276	364.84977	3.15525
6.2	127.21079	401.38180	3.15525
6.3	139.95925	441.60680	3.15525
6.4	153.99713	485.90024	3.15526
6.5	169.45557	534.67593	3.15526
6.6	186.47913	588.38993	3.15526
6.7	205.22710	647.54492	3.15526
6.8	225.87507	712.69492	3.15526
6.9	248.61659	784.45058	3.15526
7.0	273.66498	863.48502	3.15526
7.1	301.25537	950.54017	3.15526
7.2	331.64698	1046.43388	3.15526
7.3	365.12552	1152.06769	3.15526
7.4	402.00597	1268.43541	3.15527
7.5	442.63554	1396.63260	3.15527
7.6	487.39701	1537.86701	3.15527
7.7	536.71235	1693.47011	3.15527
7.8	591.04679	1864.90980	3.15527
7.9	650.91321	2053.80437	3.15527
8.0	716.87709	2261.93803	3.15527
8.1	789.56187	2491.27791	3.15527
8.2	869.65491	2743.99286	3.15527
8.3	957.91412	3022.47422	3.15527
8.4	1055.17512	3329.35863	3.15527
8.5	1162.35930	3667.55333	3.15527
8.6	1280.48263	4040.26395	3.15527
8.7	1410.66536	4451.02519	3.15527
8.8	1554.14278	4903.73471	3.15527
8.9	1712.27703	5402.69045	3.15527
9.0	1886.57019	5952.63186	3.15527
9.1	2078.67866	6558.78532	3.15527
9.2	2290.42904	7226.91425	3.15527
9.3	2523.83568	7963.37445	3.15527
9.4	2781.12001	8775.17510	3.15527
9.5	3064.73183	9670.04603	3.15527
9.6	3377.37290	10656.51197	3.15527
9.7	3722.02284	11743.97446	3.15527
9.8	4101.96782	12942.80217	3.15527
9.9	4520.83209	14264.43063	3.15527
10.0	4982.61287	15721.47212	3.15527

TABLE 25B. Lanchester-Clifford-Schläfli Functions $F_\alpha(x)$, $H_{1-\alpha}(x)$, and $T_\alpha(x)$ for $\alpha = 16/21$ and x from 1.50 to 10.0.